# LNK353/354 <br> LinkSwitch-HF Family <br> Enhanced, Energy Efficient, Low Power Off-Line Switcher IC 



## Product Highlights

## Features Optimized for Lowest System Cost

- Fully integrated auto-restart for short-circuit and open loop protection
- Self-biased supply - saves transformer auxiliary winding and associated bias supply components
- Tight tolerances and negligible temperature variation on key parameters eases design and lowers cost
- High maximum switching frequency allows very low flux density transformer designs, practically eliminating audible noise
- Frequency jittering greatly reduces EMI
- Packages with large creepage to high voltage pin
- Lowest component count switcher solution


## Much Better Performance over Linear/RCC

- Lower system cost than RCC, discrete PWM and other integrated solutions
- Universal input range allows worldwide operation
- Simple ON/OFF control - no loop compensation needed
- No bias winding - simpler, lower cost transformer
- High frequency switching - smaller and lower cost transformer
- Very low component count - higher reliability and single side printed circuit board
- High bandwidth provides fast turn on with no overshoot and excellent transient load response
- Current limit operation rejects line frequency ripple
- Built-in current limit and hysteretic thermal shutdown protection


## EcoSmart ${ }^{\text {® }}$ - Extremely Energy Efficient

- No-load consumption $<300 \mathrm{~mW}$ without bias winding at 265 VAC input
- Meets California Energy Commission (CEC), Energy Star, and EU requirements


## Applications

- Chargers for cell/cordless phones, PDAs, digital cameras, MP3/portable audio devices, shavers etc.
- Standby and auxiliary supplies


## Description

LinkSwitch-HF integrates a 700 V power MOSFET, oscillator, simple ON/OFF control scheme, a high voltage switched current


Figure 1. Typical Standby Application.

| OUTPUT POWER TABLE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| PRODUCT ${ }^{(3)}$ | 230 VAC $\pm 15 \%$ |  | 85-265 VAC |  |
|  | Adapter ${ }^{(1)}$ | Open Frame ${ }^{(2)}$ | Adapter ${ }^{(1)}$ | Open Frame ${ }^{(2)}$ |
| LNK353 P or G | 3 W | 4 W | $2.5 \mathrm{~W}^{(4)}$ | 3 W |
| LNK354 P or G | 3.5 W | 5 W | $3 \mathrm{~W}^{(4)}$ | 4.5 W |

Table 1. Notes: 1. Typical continuous power in a non-ventilated enclosed adapter measured at $50^{\circ} \mathrm{C}$ ambient. 2. Maximum practical continuous power in an open frame design with adequate heat sinking, measured at $50{ }^{\circ} \mathrm{C}$ ambient. 3. Packages: P: DIP-8B, G: SMD-8B. For lead-free package options, see Part Ordering Information. 4. For designs without a Y capacitor, the available power may be lower (see Key Applications Considerations).
source, frequency jittering, cycle-by-cycle current limit, and thermal shutdown circuitry onto a monolithic IC. The start-up and operating power are derived directly from the DRAIN pin, eliminating the need for a bias winding and associated circuitry. The 200 kHz maximum switching frequency allows very low flux transformer designs, practically eliminating audible noise with the simple ON/OFF control scheme using standard varnished transformer construction. Efficient operation at this high switching frequency is achieved due to the optimized switching characteristics and small capacitances of the integrated power MOSFET. The fully integrated auto-restart circuit safely limits output power during fault conditions such as output short circuit or open loop, reducing component count and secondary feedback circuitry cost. The internal oscillator frequency is jittered to significantly reduce both the quasi-peak and average EMI, minimizing filtering cost.


Figure 2. Functional Block Diagram.

## Pin Functional Description

## DRAIN (D) Pin:

Power MOSFET drain connection. Provides internal operating current for both start-up and steady-state operation.

## BYPASS (BP) Pin:

Connection point for a $0.1 \mu \mathrm{~F}$ external bypass capacitor for the internally generated 5.8 V supply.

## FEEDBACK (FB) Pin:

During normal operation, switching of the power MOSFET is controlled by this pin. MOSFET switching is terminated when a current greater than $49 \mu \mathrm{~A}$ is delivered into this pin.

## SOURCE (S) Pin:

This pin is the power MOSFET source connection. It is also the ground reference for the BYPASS and FEEDBACK pins.


Figure 3. Pin Configuration.

## LinkSwitch-HF Functional Description

LinkSwitch-HF combines a high voltage power MOSFET switch with a power supply controller in one device. Unlike conventional PWM (pulse width modulator) controllers, LinkSwitch-HF uses a simple ON/OFF control to regulate the output voltage. The LinkSwitch-HF controller consists of an oscillator, feedback (sense and logic) circuit, 5.8 V regulator, BYPASS pin under-voltage circuit, over-temperature protection, frequency jittering, current limit circuit, leading edge blanking and a 700 V power MOSFET. The LinkSwitch-HF incorporates additional circuitry for auto-restart.

## Oscillator

The typical oscillator frequency is internally set to an average of 200 kHz . Two signals are generated from the oscillator: the maximum duty cycle signal $\left(\mathrm{DC}_{\mathrm{MAX}}\right)$ and the clock signal that indicates the beginning of each cycle.

The LinkSwitch-HF oscillator incorporates circuitry that introduces a small amount of frequency jitter, typically 16 kHz peak-to-peak, to minimize EMI emission. The modulation rate of the frequency jitter is set to 1.5 kHz to optimize EMI reduction for both average and quasi-peak emissions. The frequency jitter should be measured with the oscilloscope triggered at the falling edge of the DRAIN waveform. The waveform in Figure 4 illustrates the frequency jitter of the LinkSwitch-HF.

## Feedback Input Circuit

The feedback input circuit at the FB pin consists of a low impedance source follower output set at 1.65 V . When the current delivered into this pin exceeds $49 \mu \mathrm{~A}$, a low logic level (disable) is generated at the output of the feedback circuit. This output is sampled at the beginning of each cycle on the rising edge of the clock signal. If high, the power MOSFET is turned on for that cycle (enabled), otherwise the power MOSFET remains off (disabled). Since the sampling is done only at the beginning of each cycle, subsequent changes in the FB pin voltage or current during the remainder of the cycle are ignored.

### 5.8 V Regulator and 6.3 V Shunt Voltage Clamp

The 5.8 V regulator charges the bypass capacitor connected to the BYPASS pin to 5.8 V by drawing a current from the voltage on the DRAIN, whenever the MOSFET is off. The BYPASS pin is the internal supply voltage node for the LinkSwitch-HF. When the MOSFET is on, the LinkSwitch-HF runs off of the energy stored in the bypass capacitor. Extremely low power consumption of the internal circuitry allows the LinkSwitch-HF to operate continuously from the current drawn from the DRAIN pin. Abypass capacitor value of $0.1 \mu$ Fis sufficient for both high frequency decoupling and energy storage.

In addition, there is a 6.3 V shunt regulator clamping the BYPASS pin at 6.3 V when current is provided to the BYPASS
pin through an external resistor. This facilitates powering of LinkSwitch-HF externally through a bias winding to decrease the no-load consumption to less than 50 mW .

## BYPASS Pin Under-Voltage

The BYPASS pin under-voltage circuitry disables the power MOSFET when the BYPASS pin voltage drops below 4.85 V . Once the BYPASS pin voltage drops below 4.85 V , it must rise back to 5.8 V to enable (turn-on) the power MOSFET.

## Over-Temperature Protection

The thermal shutdown circuitry senses the die temperature. The threshold is set at $142^{\circ} \mathrm{C}$ typical with a $75^{\circ} \mathrm{C}$ hysteresis. When the die temperature rises above this threshold $\left(142^{\circ} \mathrm{C}\right)$ the power MOSFET is disabled and remains disabled until the die temperature falls by $75^{\circ} \mathrm{C}$, at which point it is re-enabled.

## Current Limit

The current limit circuit senses the current in the power MOSFET. When this current exceeds the internal threshold ( $\mathrm{I}_{\text {LIMIT }}$ ), the power MOSFET is turned off for the remainder of that cycle. The leading edge blanking circuit inhibits the current limit comparator for a short time ( $\mathrm{t}_{\mathrm{LEB}}$ ) after the power MOSFET is turned on. This leading edge blanking time has been set so that current spikes caused by capacitance and rectifier reverse recovery time will not cause premature termination of the switching pulse.

## Auto-Restart

In the event of a fault condition such as output overload, output short circuit, or an open loop condition, LinkSwitch-HF enters into auto-restart operation. An internal counter clocked by the oscillator gets reset every time the FB pin is pulled high. If the FB pin is not pulled high for 30 ms , the power MOSFET switching is disabled for 650 ms . The auto-restart alternately enables and disables the switching of the power MOSFET until the fault condition is removed.


Figure 4. Frequency Jitter.
Time ( $\mu \mathrm{s}$ )


Figure 5. Universal Input, 5.7 V, 400 mA , Constant Voltage, Constant Current Battery Charger Using LinkSwitch-HF.

## Applications Example

## A 2.4 W CC/CV Charger Adapter

The circuit shown in Figure 5 is a typical implementation of a $5.7 \mathrm{~V}, 400 \mathrm{~mA}$, constant voltage, constant current (CV/CC) battery charger.

The input bridge formed by diodes D1-D4, rectifies the AC input voltage. The rectified AC is then filtered by the bulk storage capacitors C1 and C2. Resistor RF1 is a flameproof, fusible, wire wound type and functions as a fuse, inrush current limiter and, together with the $\pi$ filter formed by $\mathrm{C} 1, \mathrm{C} 2$ and L 1 , differential mode noise attenuator.

This simple EMI filtering, together with the frequency jittering of LinkSwitch-HF (U1), a small value Y1 capacitor (CY1), and shield windings within T 1 , and a secondary-side RC snubber (R5, C5), allows the design to meet both conducted and radiated EMI limits. The low value of CY1 is important to meet the requirement of low line frequency leakage current, in this case $<10 \mu \mathrm{~A}$.

The rectified and filtered input voltage is applied to the primary winding of T1. The other side of the transformer primary is driven by the integrated MOSFET in U1. Diode D5, C3, R1 and R3 form the primary clamp network. This limits the peak drain voltage due to leakage inductance. Resistor R3 allows the use of a slow, low cost rectifier diode by limiting the reverse current through D5 when U1 turns on. The selection of a slow diode improves efficiency and conducted EMI.

Output rectification is provided by Schottky diode D6. The low forward voltage provides high efficiency across the operating range and the low ESR capacitor C6 minimizes output voltage ripple.

In constant voltage (CV) mode, the output voltage is set by the Zener diode VR1 and the emitter-base voltage of PNP transistor Q 1 . The $\mathrm{V}_{\mathrm{BE}}$ of Q 1 divided by the value of R7 sets the bias current through VR1 ( $\sim 2.7 \mathrm{~mA})$. When the output voltage exceeds the threshold voltage determined by Q1 and VR1, Q1 is turned on and current flows through the LED of U2. As the LED current increases, the current fed into the FEEDBACK pin increases, disabling further switching cycles of U1. At very light loads, almost all switching cycles will be disabled, giving a low effective switching frequency and providing low no-load consumption.

During load transients, R6 and R8 ensure that the ratings of Q1 are not exceeded while R4 prevents C 4 from being discharged.

Resistors R9 and R10 form the constant current (CC) sense circuit. Above approximately 400 mA , the voltage across the sense resistor exceeds the optocoupler diode forward conduction voltage of approximately 1 V . The current through the LED is therefore determined by the output current and CC control dominates over the CV feedback loop. CC control is maintained even under output short circuit conditions.

## Key Application Considerations

## LinkSwitch-HF Design Considerations

## Output Power Table

Data sheet maximum output power table (Table 1) represents the maximum practical continuous output power level that can be obtained under the following assumed conditions:

1. The minimum DC input voltage is 90 V or higher for 85 VAC input, or 240 V or higher for 230 VAC input or 115 VAC with a voltage doubler. The value of the input capacitance should be large enough to meet these criteria for AC input designs.
2. Secondary output of 5.5 V with a Schottky rectifier diode.
3. Assumed efficiency of $70 \%$.
4. Operating frequency of $\mathrm{f}_{\mathrm{OSC}(\min )}$ and $\mathrm{I}_{\mathrm{LIMIT}(\min )}$.
5. Voltage only output (no secondary side constant current circuit).
6. Continuous mode operation $\left(0.6 \leq \mathrm{K}_{\mathrm{P}} \leq 1\right)$.
7. The part is board mounted with SOURCE pins soldered to a sufficient area of copper to keep the SOURCE pin temperature at or below $100^{\circ} \mathrm{C}$.
8. Ambient temperature of $50^{\circ} \mathrm{C}$ for open frame designs and an internal enclosure temperature of $60^{\circ} \mathrm{C}$ for adapter designs.

Below a value of $1, \mathrm{~K}_{\mathrm{p}}$ is the ratio of ripple to peak primary current. Above a value of $1, \mathrm{~K}_{\mathrm{p}}$ is the ratio of primary MOSFET off time to the secondary diode conduction time.

Operating at a lower effective switching frequency can simplify meeting conducted and radiated EMI limits, especially for designs where the safety Y capacitor must be eliminated. By using a lower effective full load frequency, the calculated value of the primary inductance is higher than required for power delivery. However, the maximum power capability at this lower operating frequency will be lower than the values shown in Table 1.

## Audible Noise

The cycle skipping mode of operation used in LinkSwitch-HF can generate audio frequency components in the transformer. To limit this audible noise generation, the transformer should be designed such that the peak core flux density is below 1250 Gauss ( 125 mT ). Following this guideline and using the standard transformer production technique of dip varnishing practically eliminates audible noise. Higher flux densities are possible however, careful evaluation of the audible noise performance should be made using production transformer samples before approving the design.

Ceramic capacitors that use dielectrics such as Z5U , when used in clamp circuits, may also generate audio noise. If this is the case, try replacing them with a capacitor having a different dielectric, for example a polyester film type.

## LinkSwitch-HF Layout Considerations

See Figure 6 for a recommended circuit board layout for LinkSwitch-HF.

## Single Point Grounding

Use a single point ground connection from the input filter capacitor to the area of copper connected to the SOURCE pins.

## Bypass Capacitor ( $\mathrm{C}_{\mathrm{BP}}$ )

The BYPASS pin capacitor should be located as near as possible to the BYPASS and SOURCE pins.

## Primary Loop Area

The area of the primary loop that connects the input filter capacitor, transformer primary and LinkSwitch-HF together should be kept as small as possible.

## Primary Clamp Circuit

A clamp is used to limit peak voltage on the DRAIN pin at turn off. This can be achieved by using an RCD clamp (as shown in Figure 5) or a Zener ( $\sim 200 \mathrm{~V}$ ) and diode clamp across the primary winding. In all cases, to minimize EMI, care should be taken to minimize the circuit path from the clamp components to the transformer and LinkSwitch-HF.

## Thermal Considerations

The copper area underneath the LinkSwitch-HF acts not only as a single point ground, but also as a heatsink. As this area is connected to the quiet source node, this area should be maximized for good heatsinking of LinkSwitch-HF. The same applies to the cathode of the output diode.

## Y-Capacitor

The placement of the Y-capacitor should be directly from the primary input filter capacitor positive terminal to the common/return terminal of the transformer secondary. Such a placement will route high magnitude common mode surge currents away from the LinkSwitch-HF device. Note that if an input $\pi(\mathrm{C}, \mathrm{L}, \mathrm{C})$ EMI filter is used, then the inductor in the filter should be placed between the negative terminals of the input filter capacitors.

## Optocoupler

Place the optocoupler physically close to the LinkSwitch-HF to minimize the primary side trace lengths. Keep the high current, high voltage drain and clamp traces away from the optocoupler to prevent noise pick up.

## Output Diode

For best performance, the area of the loop connecting the secondary winding, the output diode and the output filter capacitor should be minimized. In addition, sufficient copper area should be provided at the anode and cathode terminals

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of the diode for heatsinking. A larger area is preferred at the quiet cathode terminal. A large anode area can increase high frequency radiated EMI.

## Quick Design Checklist

As with any power supply design, all LinkSwitch-HF designs should be verified on the bench to make sure that component specifications are not exceeded under worst-case conditions. The following minimum set of tests is strongly recommended:

1. Maximum drain voltage - Verify that $\mathrm{V}_{\mathrm{DS}}$ does not exceed 675 V at the highest input voltage and peak (overload) output power.
2. Maximum drain current-At maximum ambient temperature, maximum input voltage and peak output (overload) power, verify drain current waveforms for any signs of transformer saturation and excessive leading edge current spikes at startup. Repeat under steady state conditions and verify that
the leading edge current spike event is below $\mathrm{I}_{\text {LIMIT(MIN) }}$ at the end of the $t_{\text {LEB(MIN) }}$. Under all conditions, the maximum drain current should be below the specified absolute maximum ratings.
3. Thermal Check - At specified maximum output power, minimum input voltage and maximum ambient temperature, verify that the temperature specifications are not exceeded for LinkSwitch-HF, transformer, output diode, and output capacitors. Enough thermal margin should be allowed for part-to-part variation of the $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ of LinkSwitch-HF as specified in the data sheet. Under low line, maximum power, a maximum LinkSwitch-HF SOURCE pin temperature of $100^{\circ} \mathrm{C}$ is recommended to allow for these variations.

## Design Tools

Up-to-date information on design tools can be found at the Power Integrations website: www.powerint.com.


Figure 6. Recommended Printed Circuit Layout for LinkSwitch-HF in a Flyback Converter Configuration.


| THERMAL IMPEDANCE |  |
| :---: | :---: |
| Thermal Impedance: P or G Package: $\begin{aligned} & \left(\theta_{\mathrm{JA}}\right) . \ldots . . . . . . . . . . . . . . . . . . . ~ \\ & 70^{\circ} \mathrm{C} / \mathrm{W}^{(2)} ; 60^{\circ} \mathrm{C} / \mathrm{W}^{(3)} \\ & \left(\theta_{\mathrm{JC}}\right)^{(1)} \ldots \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ~ \\ & 11^{\circ} \mathrm{C} / \mathrm{W} \end{aligned}$ | Notes: <br> 1. Measured on pin 2 (SOURCE) close to plastic interface. <br> 2. Soldered to 0.36 sq . in. $\left(232 \mathrm{~mm}^{2}\right), 2 \mathrm{oz}$. $\left(610 \mathrm{~g} / \mathrm{m}^{2}\right)$ copper clad. <br> 3. Soldered to 1 sq . in. $\left(645 \mathrm{~mm}^{2}\right), 2 \mathrm{oz}$. $\left(610 \mathrm{~g} / \mathrm{m}^{2}\right)$ copper clad. |



| Parameter | Symbol | Conditions <br> SOURCE $=0 \mathrm{~V} ; \mathrm{T}_{\mathrm{J}}=-40$ to $125^{\circ} \mathrm{C}$ <br> See Figure 7 <br> (Unless Otherwise Specified) |  | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CONTROL FUNCTIONS (cont) |  |  |  |  |  |  |  |
| BYPASS Pin Supply Current | $I_{\text {BPSC }}$ | See Note D |  | 68 |  |  | $\mu \mathrm{A}$ |
| CIRCUIT PROTECTION |  |  |  |  |  |  |  |
| Current Limit | $\begin{gathered} \mathrm{I}_{\text {LIMT }} \\ (\text { See } \\ \text { Note E) } \end{gathered}$ | $\begin{gathered} \mathrm{di} / \mathrm{dt}=90 \mathrm{~mA} / \mu \mathrm{s} \\ \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ | LNK353 | 172 | 185 | 198 | mA |
|  |  | $\begin{gathered} \mathrm{di} / \mathrm{dt}=400 \mathrm{~mA} / \mathrm{\mu s} \\ \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ |  | 215 | 245 | 274 |  |
|  |  | $\begin{gathered} \mathrm{di} / \mathrm{dt}=115 \mathrm{~mA} / \mu \mathrm{s} \\ \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ | LNK354 | 233 | 250 | 268 |  |
|  |  | $\begin{gathered} \mathrm{di} / \mathrm{dt}=500 \mathrm{~mA} / \mu \mathrm{s} \\ \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ |  | 264 | 300 | 336 |  |
| Minimum On Time | $\mathrm{t}_{\text {on(min) }}$ |  | LNK353 | 390 | 470 | 610 | ns |
|  |  |  | LNK354 | 280 | 360 | 500 |  |
| Leading Edge Blanking Time | $t_{\text {Leb }}$ | $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ <br> See Note F |  | 170 | 215 |  | ns |
| Thermal Shutdown Temperature | $\mathrm{T}_{\text {sD }}$ |  |  | 135 | 142 | 150 | ${ }^{\circ} \mathrm{C}$ |
| Thermal Shutdown Hysteresis | $\mathrm{T}_{\text {SHD }}$ | See Note G |  |  | 75 |  | ${ }^{\circ} \mathrm{C}$ |
| OUTPUT |  |  |  |  |  |  |  |
| ON-State Resistance | $\mathrm{R}_{\text {DS(ON) }}$ | $\begin{gathered} \mathrm{LNK} 353 \\ \mathrm{I}_{\mathrm{D}}=25 \mathrm{~mA} \end{gathered}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 34 | 40 | $\Omega$ |
|  |  |  | $\mathrm{T}_{\mathrm{J}}=100{ }^{\circ} \mathrm{C}$ |  | 54 | 63 |  |
|  |  | $\begin{gathered} \text { LNK354 } \\ \mathrm{I}_{\mathrm{D}}=25 \mathrm{~mA} \end{gathered}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 24 | 28 |  |
|  |  |  | $\mathrm{T}_{\mathrm{J}}=100^{\circ} \mathrm{C}$ |  | 38 | 45 |  |
| OFF-State Drain Leakage Current | $\mathrm{I}_{\text {DSs }}$ | $\begin{gathered} \mathrm{V}_{\mathrm{BP}}=6.2 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}} \geq 2 \mathrm{~V}, \\ \mathrm{~V}_{\mathrm{DS}}=560 \mathrm{~V}, \\ \mathrm{~T}_{\mathrm{J}}=125^{\circ} \mathrm{C} \end{gathered}$ |  |  |  | 50 | $\mu \mathrm{A}$ |
| Breakdown Voltage | $B V_{\text {DSs }}$ | $\begin{gathered} \mathrm{V}_{\mathrm{BP}}=6.2 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}} \geq 2 \mathrm{~V}, \\ \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C} \end{gathered}$ |  | 700 |  |  | V |
| Rise Time | $\mathrm{t}_{\mathrm{R}}$ | Measured in a Typical Flyback Converter Application |  |  | 50 |  | ns |
| Fall Time | $\mathrm{t}_{\mathrm{F}}$ |  |  |  | 50 |  | ns |

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| Parameter | Symbol | Conditions <br> SOURCE $=0 \mathrm{~V} ; \mathrm{T}_{j}=-40$ to $125^{\circ} \mathrm{C}$ <br> See Figure 7 <br> (Unless Otherwise Specified) | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OUTPUT (cont) |  |  |  |  |  |  |
| DRAIN Supply Voltage |  |  | 50 |  |  | V |
| Output Enable Delay | $\mathrm{t}_{\text {EN }}$ | See Figure 9 |  |  | 10 | $\mu \mathrm{s}$ |
| Output Disable Setup Time | $\mathrm{t}_{\text {DST }}$ |  |  | 0.5 |  | $\mu \mathrm{s}$ |
| Auto-Restart ON-Time | $\mathrm{t}_{\text {AR }}$ | $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ <br> See Note H |  | 31 |  | ms |
| Auto-Restart Duty Cycle | $D C_{\text {AR }}$ |  |  | 5 |  | \% |

## NOTES:

A. Total current consumption is the sum of $I_{S 1}$ and $I_{D S S}$ when FEEDBACK pin voltage is $\geq 2 \mathrm{~V}$ (MOSFET not switching) and the sum of $\mathrm{I}_{\mathrm{S} 2}$ and $\mathrm{I}_{\mathrm{DSS}}$ when FEEDBACK pin is shorted to SOURCE (MOSFET switching).

B Since the output MOSFET is switching, it is difficult to isolate the switching current from the supply current at the DRAIN. An alternative is to measure the BYPASS pin current at 6 V .
C. See Typical Performance Characteristics section Figure 14 for BYPASS pin start-up charging waveform.
D. This current is only intended to supply an optional optocoupler connected between the BYPASS and FEEDBACK pins and not any other external circuitry.
E. For current limit at other di/dt values, refer to Figure 13.
F. This parameter is guaranteed by design.
G. This parameter is derived from characterization.
H. Auto-restart on time has the same temperature characteristics as the oscillator (inversely proportional to frequency).


Figure 7. LinkSwitch-HF General Test Circuit.


Figure 8. LinkSwitch-HF Duty Cycle Measurement.


Figure 9. LinkSwitch-HF Output Enable Timing.

## Typical Performance Characteristics



Figure 10. Breakdown vs. Temperature.


Figure 12. Current Limit vs. Temperature at Normalized di/dt.


Figure 14. BYPASS Pin Start-up Waveform.


Figure 11. Frequency vs. Temperature.


Figure 13. Current Limit vs. di/dt.


Figure 15. Output Characteristics.

## Typical Performance Characteristics (cont.)



Figure 16. $C_{\text {oss }}$ vs. Drain Voltage.

## PART ORDERING INFORMATION

| LinkSwitch Product Family |  |
| :---: | :--- |
| HF Series Number |  |
| Package Identifier |  |
| G | Plastic Surface Mount DIP |
| P | Plastic DIP |
| Lead Finish |  |
| Blank | Standard (Sn Pb) |
| N | Pure Matte Tin (Pb-Free) |
| Tape \& Reel and Other Options |  |
| Blank | Standard Configurations |
| TL | Tape \& Reel, 1 k pcs minimum, G Package only |



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Notes

Notes

| Revision | Notes | Date |
| :---: | :--- | :---: |
| D | 1) Released Final Data Sheet. | $10 / 04$ |
| E | 1) Added lead-free ordering information. | $12 / 04$ |
| F | 1) Minor error corrections. | $2 / 05$ |

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# OCEAN CHIPS <br> Океан Электроники <br> Поставка электронных компонентов 

Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;
- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR». JONHON
«JONHON» (основан в 1970 г.)
Разъемы специального, военного и аэрокосмического назначения:
(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)
«FORSTAR» (основан в 1998 г.)
ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:
(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).


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