



# BCM<sup>®</sup> Bus Converter BCM380y475x800A31

# c 🕰 us 🖾 😂 CE

# Fixed Ratio DC-DC Converter

#### **Features**

- Up to 800 W continuous output power
- 1250 W/in<sup>3</sup> power density
- 97.7% peak efficiency
- 4242 Vdc isolation
- Parallel operation for multi-kW arrays
- OV, OC, UV, short circuit and thermal protection
- 6123 through-hole ChiP package
  - 2.494" x 0.898" x 0.286"
     (63.34 mm x 22.80 mm x 7.26 mm)
- PMBus<sup>™</sup> management interface\*

### **Typical Applications**

- 380 DC Power Distribution
- High End Computing Systems
- Automated Test Equipment
- Industrial Systems
- High Density Power Supplies
- Communications Systems
- Transportation

Produc	t Ratings
$V_{IN} = 380 V (260 - 410 V)$	Pout = up to 800 W
V <sub>OUT</sub> = 47.5 V (32.5 – 51.3 V) (NO LOAD)	K = 1/8

### **Product Description**

The VI Chip® Bus Converter (BCM) is a high efficiency Sine Amplitude Converter (SAC), operating from a 260 to 410 VDC primary bus to deliver an isolated ratiometric output from 32.5 to 51.3 VDC.

The BCM380y475x800A31 offers low noise, fast transient response, and industry leading efficiency and power density. In addition, it provides an AC impedance beyond the bandwidth of most downstream regulators, allowing input capacitance normally located at the input of a POL regulator to be located at the input of the BCM module. With a K factor of 1/8, that capacitance value can be reduced by a factor of 64x, resulting in savings of board area, material and total system cost.

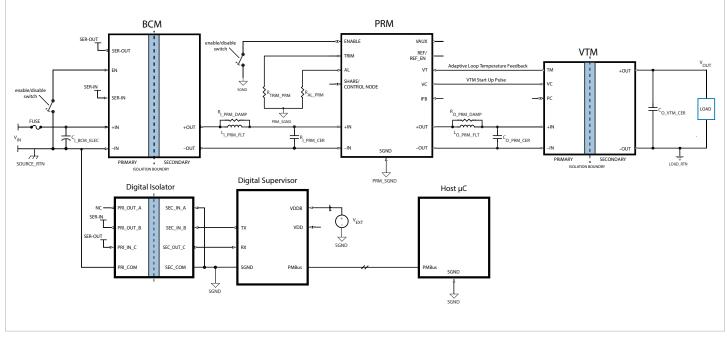
The BCM380y475x800A31, combined with the D44TL1A0 Digital Supervisor and I13TL1A0 Digital Isolator, provide a secondary referenced PMBus™ compatible telemetry and control interface. This interface provides access to the BCM's internal controller configuration, fault monitoring, and other telemetry functions.

Leveraging the thermal and density benefits of Vicor's ChiP packaging technology, the BCM module offers flexible thermal management options with very low top and bottom side thermal impedances. Thermally-adept ChiP-based power components, enable customers to achieve low cost power system solutions with previously unattainable system size, weight and efficiency attributes, quickly and predictably.

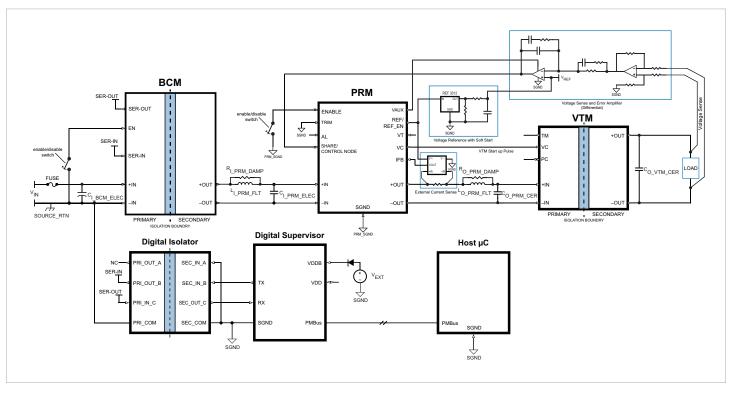
\*When used with D44TL1A0 and I13TL1A0 chipset



# **Typical Application**



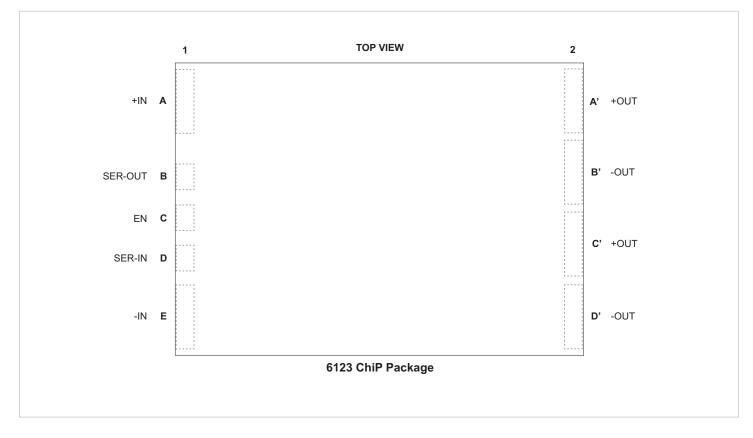
BCM380y475x800A31 + PRM + VTM, Adaptive Loop Configuration



BCM380y475x800A31 + PRM + VTM, Remote Sense Configuration



# **Pin Configuration**



# **Pin Descriptions**

Pin Number	Signal Name	Туре	Function		
A1	+IN	INPUT POWER	Positive input power terminal		
B1	B1 SER-OUT OUTPUT		UART transmit pin; Primary side referenced signals		
C1 EN INPUT		INPUT	Enables and disables power supply; Primary side referenced signals		
D1	SER-IN	INPUT	UART receive pin; Primary side referenced signals		
E1	-IN	INPUT POWER RETURN	Negative input power terminal		
A'2, C'2	A'2, C'2 +OUT		Positive output power terminal		
B'2, D'2	-OUT	OUTPUT POWER RETURN	Negative output power terminal		



### **Part Ordering Information**

Device	Input Voltage Range	Package Type	Output Voltage x 10	Temperature Grade	Output Power	Revision	Package Size	Version
BCM	380	У	475	х	800	А	3	1
BCM = BCM	380 = 260 to 410 V	P = ChiP Through Hole	475 = 47.5 V	T = -40 to 125°C M = -55 to 125°C	800 = 800 W	А	3 = 6123	1

All products shipped in JEDEC standard high profile (0.400" thick) trays (JEDEC Publication 95, Design Guide 4.10).

### **Standard Models**

Part Number	V <sub>IN</sub>	Package Type	V <sub>OUT</sub>	Temperature	Power	Package Size
BCM380 <b>P</b> 475 <b>T</b> 800A31	260 to 410 V	ChiP Through Hole	47.5 V 32.5 to 51.3 V	-40°C to 125°C	800 W	6123
BCM380 <b>P</b> 475 <b>M</b> 800A31	260 to 410 V	ChiP Through Hole	47.5 V 32.5 to 51.3 V	-55°C to 125°C	800 W	6123

#### **Absolute Maximum Ratings**

The absolute maximum ratings below are stress ratings only. Operation at or beyond these maximum ratings can cause permanent damage to the device.

Parameter	Comments	Min	Мах	Unit
+IN to -IN		-1	480	V
$V_{IN}$ slew rate (operational)			1000	V/ms
Isolation voltage, input to output	Dielectric test applied to 100% production units		4242	V
+OUT to -OUT		-1	60	V
SER-OUT to -IN		-0.3	4.6	V
EN to –IN		-0.3	5.5	V
SER-IN to -IN		-0.3	4.6	V



### **Electrical Specifications**

Specifications apply over all line and load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of  $-40^{\circ}C \le T_{INTERNAL} \le 125^{\circ}C$  (T-Grade); All other specifications are at  $T_{INTERNAL} = 25^{\circ}C$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Тур	Мах	Unit	
		Powertrain					
Input voltage range, continuous	V <sub>IN_DC</sub>		260		410	V	
		Full current or power supported, 50 ms max,					
Input voltage range, transient	Vin_trans	10% duty cycle max	260		410	V	
		$V_{IN}$ voltage where $\mu C$ is initialized,					
$V_{IN} \mu Controller Active$	$V_{\mu C\_ACTIVE}$	(ie VAUX = Low, powertrain inactive)			120	V	
		Disabled, EN Low, $V_{IN} = 380 \text{ V}$		2			
Quiescent current	Ι <sub>Q</sub>	$T_{\text{INTERNAL}} \leq 100^{\circ}\text{C}$			4	mA	
		$V_{IN} = 380 \text{ V},  \text{T}_{INTERNAL} = 25^{\circ}\text{C}$		8.9	12		
		$V_{\rm IN} = 380 \text{ V}$	5	0.5	16	-	
No load power dissipation	P <sub>NL</sub>	$V_{IN} = 260 \text{ V}$ to 410 V, $T_{INTERNAL} = 25^{\circ}\text{C}$	2		15	W	
		$V_{IN} = 260 \text{ V to } 110 \text{ V}, \text{ INTERINAL} = 25 \text{ C}$ $V_{IN} = 260 \text{ V to } 410 \text{ V}$			20	-	
		$V_{IN} = 410 \text{ V}, \text{ C}_{OUT} = 100 \mu\text{F},$					
Inrush current peak	I <sub>INR_P</sub>	$R_{LOAD} = 25\%$ of full load current		6		A	
		T <sub>INTERNAL</sub> ≤ 100°C			12		
DC input current	lin_dc	At $P_{OUT}$ = 800 W, $T_{INTERNAL} \le 100^{\circ}C$			2.25	А	
Transformation ratio	К	$K = V_{OUT}/V_{IN}$ , at no load		1/8		V/V	
Output power (continuous)	P <sub>OUT_DC</sub>				800	W	
Output power (pulsed)	P <sub>OUT_PULSE</sub>	10 ms pulse, 25% Duty cycle, $P_{TOTAL} = 50\%$ rated $P_{OUT_DC}$			1000	W	
Output current (continuous)	I <sub>OUT_DC</sub>				16.9	Α	
Output current (pulsed)	I <sub>OUT_PULSE</sub>	10 ms pulse, 25% Duty cycle, $I_{TOTAL} = 50\%$ rated $I_{OUT_DC}$			21	А	
		V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 16.9 A	96.5	97.4			
Efficiency (ambient)	$\eta_{AMB}$	V <sub>IN</sub> = 260 V to 410 V, I <sub>OUT</sub> = 16.9 A	95.3			%	
		V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 8.45 A	96.5	97.5		-	
Efficiency (hot)	$\eta_{HOT}$	V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 16.9 A, T <sub>INTERNAL</sub> = 100°C	96.3	97.1		%	
Efficiency (over load range)	$\eta_{20\%}$	3 A < I <sub>OUT</sub> < 16.9 A, T <sub>INTERNAL</sub> ≤ 100°C	92			%	
	R <sub>OUT_COLD</sub>	V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 16.9 A, T <sub>INTERNAL</sub> = -40°C	10	19	33		
Output resistance	R <sub>OUT_AMB</sub>	V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 16.9 A	12	35	58	mΩ	
	R <sub>OUT_HOT</sub>	V <sub>IN</sub> = 380 V, I <sub>OUT</sub> = 16.9 A, T <sub>INTERNAL</sub> = 100°C	24	43	60		
Switching frequency	F <sub>SW</sub>	Frequency of the Output Voltage Ripple = $2x F_{SW}$	1.12	1.18	1.24	MHz	
		C <sub>OUT</sub> = 0 F, I <sub>OUT</sub> = 16.9 A, V <sub>IN</sub> = 380 V,		250			
Output voltage ripple	Vout_pp	20 MHz BW		250		mV	
	_	T <sub>INTERNAL</sub> ≤ 100°C			350	-	
Input inductance (parasitic)		Frequency 2.5 MHz (double switching frequency),		6.7		nH	
	L <sub>IN_PAR</sub>	Simulated lead model		0.7			
Output inductance (parasitic)	Lout_par	Frequency 2.5 MHz (double switching frequency),		1.3		nH	
,		Simulated lead model					
Input Series inductance (internal)	L <sub>IN_INT</sub>	Reduces the need for input decoupling inductance in BCM arrays		0.56		μH	
	<u> </u>	Effective value at 380 V <sub>IN</sub>		0.25			
Effective Input capacitance (internal)	CIN_INT	LITECTIVE VALUE AT DOD AIN		0.25		μF	



### **Electrical Specifications (Cont.)**

Specifications apply over all line and load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of  $-40^{\circ}C \le T_{INTERNAL} \le 125^{\circ}C$  (T-Grade); All other specifications are at  $T_{INTERNAL} = 25^{\circ}C$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Тур	Мах	Unit
		Powertrain (Cont.)				
Effective Output capacitance (internal)	C <sub>OUT_INT</sub>	Effective value at 47.5 V <sub>OUT</sub>		12.8		μF
Effective Output capacitance (external)	COUT_EXT	Excessive capacitance may drive module into SC protection	0		100	μF
Array Maximum external output capacitance	C <sub>OUT_AEXT</sub>	$C_{OUT\_AEXT}$ Max = N * 0.5* $C_{OUT\_EXT}$ Max				
		Powertrain Protection				
Auto Restart Time	t <sub>auto_restart</sub>	Startup into a persistent fault condition. Non-Latching fault detection given $V_{IN} > V_{IN\_UVLO+}$ , Module will ignore attempts to re-enable during time off	292.5		357.5	ms
Input overvoltage lockout threshold	VIN_OVLO+		430	440	450	V
Input overvoltage recovery threshold	VIN_OVLO-		420	430	440	V
Input overvoltage lockout hysteresis	Vin_ovlo_hyst			10		V
Overvoltage lockout response time	t <sub>ovlo</sub>			10		μs
Soft-Start time	t <sub>soft-start</sub>	From powertrain active Fast Current limit protection disabled during Soft-Start		1		ms
Output overcurrent trip threshold	I <sub>OCP</sub>		18	23.7	40	А
Overcurrent Response Time Constant	t <sub>OCP</sub>	Effective internal RC filter		3.6		ms
Short circuit protection trip threshold	I <sub>SCP</sub>		30			А
Short circuit protection response time	t <sub>SCP</sub>			1		μs
Overtemperature shutdown threshold	t <sub>OTP</sub>	Temperature sensor located inside controller IC	125			°C
		Powertrain Supervisory Limits				
Input overvoltage lockout threshold	V <sub>IN_OVLO+</sub>		420	434.5	450	V
Input overvoltage recovery threshold	V <sub>IN_OVLO-</sub>		405	424	440	V
Input overvoltage lockout hysteresis	V <sub>IN_OVLO_HYST</sub>			10.5		V
Overvoltage lockout response time	t <sub>ovlo</sub>			100		μs
Input undervoltage lockout threshold	V <sub>IN_UVLO-</sub>		200	226	250	V
Input undervoltage recovery threshold	V <sub>IN_UVLO+</sub>		225	244	259	V
Input undervoltage lockout hysteresis	V <sub>IN_UVLO_HYST</sub>			15		V
Undervoltage lockout response time	t <sub>UVLO</sub>			100		μs
Undervoltage startup delay	t <sub>UVLO+_DELAY</sub>	From $V_{IN} = V_{IN\_UVLO+}$ to powertrain active, EN floating, (i.e One time Startup delay from application of $V_{IN}$ to $V_{OUT}$ )		20		ms
Output Overcurrent Trip Threshold	I <sub>OCP</sub>		20	22	24	А
Overcurrent Response Time Constant	t <sub>OCP</sub>			3.6		ms
Overtemperature shutdown threshold	t <sub>OTP</sub>	Temperature sensor located inside controller IC	125			°C
Undertemperature shutdown threshold	t <sub>UTP</sub>	Temperature sensor located inside controller IC			-45	°C
Undertemperature restart time	t <sub>UTP_RESTART</sub>	Startup into a persistent fault condition. Non-Latching fault detection given $V_{IN} > V_{IN\_UVLO+}$		3		S



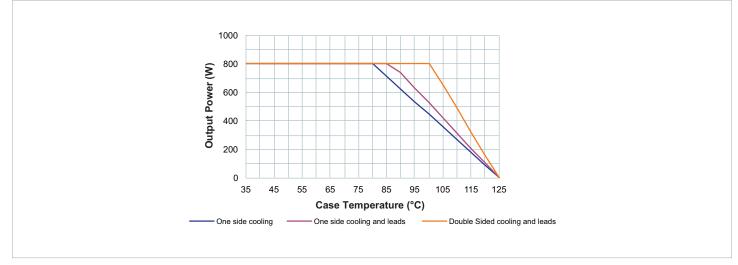


Figure 1 — Specified thermal operating area

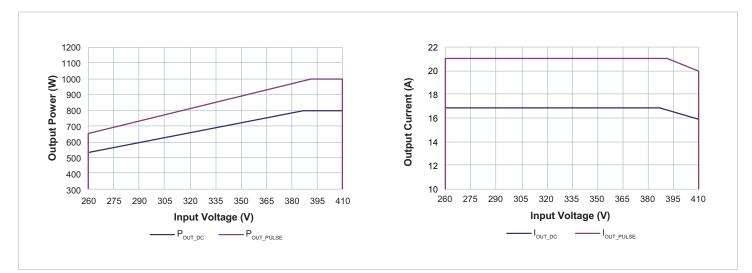


Figure 2 — Specified electrical operating area using rated R<sub>OUT\_HOT</sub>

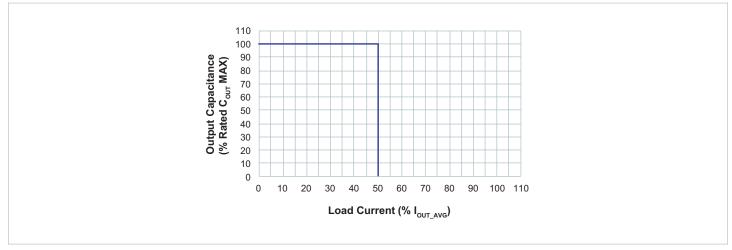


Figure 3 — Specified Primary start-up into load current and external capacitance



#### **Reported Characteristics**

Specifications apply over all line, load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of  $-40^{\circ}C \le T_{INTERNAL} \le 125^{\circ}C$  (T-Grade); All other specifications are at  $T_{INTERNAL} = 25^{\circ}C$  unless otherwise noted.

	Monitored Telemetry									
• The BCM communication version is not intended to be used without a Digital Supervisor.										
ATTRIBUTE	DIGITAL SUPERVISOR PMBus™ READ COMMAND	ACCURACY (RATED RANGE)	FUNCTIONAL REPORTING RANGE	UPDATE RATE	REPORTED UNITS					
Input voltage	(88h) READ_VIN	± 5%(LL - HL)	130 V to 450 V	100 µs	V <sub>ACTUAL</sub> = V <sub>REPORTED</sub> x 10 <sup>-1</sup>					
Input current	(89h) READ_IIN	± 20%(10 - 20% of FL) ± 5%(20 - 133% of FL)	- 0.42 A to 2.9 A	100 µs	$I_{ACTUAL} = I_{REPORTED} \times 10^{-3}$					
Output voltage <sup>[1]</sup>	(8Bh) READ_VOUT	± 5%(LL - HL)	16.25 V to 56.25 V	100 µs	$V_{ACTUAL} = V_{REPORTED} \times 10^{-1}$					
Output current	(8Ch) READ_IOUT	± 20%(10 - 20% of FL) ± 5%(20 - 133% of FL)	- 3.5 A to 22.5 A	100 µs	$I_{ACTUAL}L = I_{REPORTED} \times 10^{-2}$					
Output resistance	(D4h) READ_ROUT	± 5%(50 - 100% of FL) at NL ± 10%(50 - 100% of FL)(LL - HL)	2 m $\Omega$ to 50 m $\Omega$	100 ms	$R_{ACTUAL} = R_{REPORTED} \times 10^{-5}$					
Temperature <sup>[2]</sup>	(8Dh) READ_TEMPERATURE_1	± 7°C(Full Range)	- 55°C to 130°C	100 ms	T <sub>ACTUAL</sub> = T <sub>REPORTED</sub>					

 $^{[1]}$  Default READ Output Voltage returned when unit is disabled = -300 V.  $^{[2]}$  Default READ Temperature returned when unit is disabled = -273°C.

#### Variable Parameter

• Factory setting of all below Thresholds and Warning limits are 100% of listed protection values.

• Variables can be written only when module is disabled either EN pulled low or  $V_{IN} < V_{IN UVLO-}$ .

• Module must remain in a disabled mode for 3 ms after any changes to the below variables allowing ample time to commit changes to EEPROM.

ATTRIBUTE	DIGITAL SUPERVISOR PMBus <sup>™</sup> COMMAND <sup>[3]</sup>	CONDITIONS / NOTES	ACCURACY (RATED RANGE)	FUNCTIONAL REPORTING	DEFAULT VALUE
	Philos Command			RANGE	VALUE
Input / Output Overvoltage Protection Limit	(55h) VIN_OV_FAULT_LIMIT	$V_{\text{IN}\_\text{OVLO-}}$ is automatically 3% lower than this set point	± 5%(LL - HL)	130 V to 435 V	100%
Input / Output Overvoltage Warning Limit	(57h) VIN_OV_WARN_LIMIT		± 5%(LL - HL)	130 V to 435 V	100%
Input / Output Undervoltage Protection Limit	(D7h) DISABLE_FAULTS	Can only be disabled to a preset default value	± 5%(LL - HL)	130 V or 260 V	100%
Input Overcurrent Protection Limit	(5Bh) IIN_OC_FAULT_LIMIT		± 20%(10 - 20% of FL) ± 5%(20 - 133% of FL)	0.21 to 0.42 A 0.42 to 2.810 A	100%
Input Overcurrent Warning Limit	(5Dh) IIN_OC_WARN_LIMIT		± 20%(10 - 20% of FL) ± 5%(20 - 133% of FL)	0.21 to 0.42 A 0.42 to 2.810 A	100%
Overtemperature Protection Limit	(4Fh) OT_FAULT_LIMIT		± 7°C(Full Range)	0 to 125°C	100%
Overtemperature Warning Limit	(51h) OT_WARN_LIMIT		± 7°C(Full Range)	0 to 125°C	100%
Turn on Delay	(60h) TON_DELAY	Additional time delay to the Undervoltage Startup Delay	± 50 μs	0 to 100 ms	0 ms

<sup>[3]</sup> Refer to Digital Supervisor datasheet for complete list of supported commands.



#### **Signal Characteristics**

Specifications apply over all line, load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of  $-40^{\circ}C \le T_{INTERNAL} = 125^{\circ}C$  (T-Grade); All other specifications are at  $T_{INTERNAL} = 25^{\circ}C$  unless otherwise noted.

#### UART SER-IN / SER-OUT Pins

• Universal Asynchronous Receiver/Transmitter (UART) pins.

- The BCM communication version is not intended to be used without a Digital Supervisor.
- Isolated I<sup>2</sup>C communication and telemetry is available when using Vicor Digital Isolator and Vicor Digital Supervisor. Please see specific product data sheet for more details.
- $\bullet$  UART SER-IN pin is internally pulled high using a 1.5 k $\Omega$  to 3.3 V.

SIGNAL TYPE	STATE	ATTRIBUTE	SYMBOL	CONDITIONS / NOTES	MIN	ТҮР	MAX	UNIT
GENERAL I/O		Baud Rate	BR <sub>UART</sub>	Rate		750		Kbit/s
		SER-IN Pin						
		SER-IN Input Voltage Range	$V_{\text{SER-IN}\_\text{IH}}$		2.3			V
		SER in input voltage hange	V <sub>SER-IN_IL</sub>				1	V
DIGITAL		SER-IN rise time	t <sub>ser-IN_RISE</sub>	10% to 90%		400		ns
INPUT		SER-IN fall time	t <sub>SER-IN_FALL</sub>	10% to 90%		25		ns
	Regular	SER-IN R <sub>PULLUP</sub>	R <sub>SER-IN_PLP</sub>	Pull up to 3.3 V		1.5		kΩ
		SER-IN External Capacitance	C <sub>SER-IN_EXT</sub>				400	pF
	Operation	SER-OUT Pin						
		SER-OUT Output Voltage	V <sub>SER-OUT_OH</sub>	$0 \text{ mA} \ge I_{OH} \ge -4 \text{ mA}$	2.8			V
DIGITAL		Range	V <sub>SER-OUT_OL</sub>	$0 \text{ mA} \le I_{OL} \le 4 \text{ mA}$			0.5	V
OUTPUT		SER-OUT rise time	t <sub>ser-out_rise</sub>	10% to 90%		55		ns
		SER-OUT fall time	t <sub>ser-out_fall</sub>	10% to 90%		45		ns
		SER-OUT source current	I <sub>SER-OUT</sub>	V <sub>SER-OUT</sub> = 2.8 V			6	mA
		SER-OUT output impedance	Z <sub>SER-OUT</sub>			120		Ω

#### Enable / Disable Control

• The EN pin is a standard analog I/O configured as an input to an internal  $\mu$ C.

• It is internally pulled high to 3.3 V.

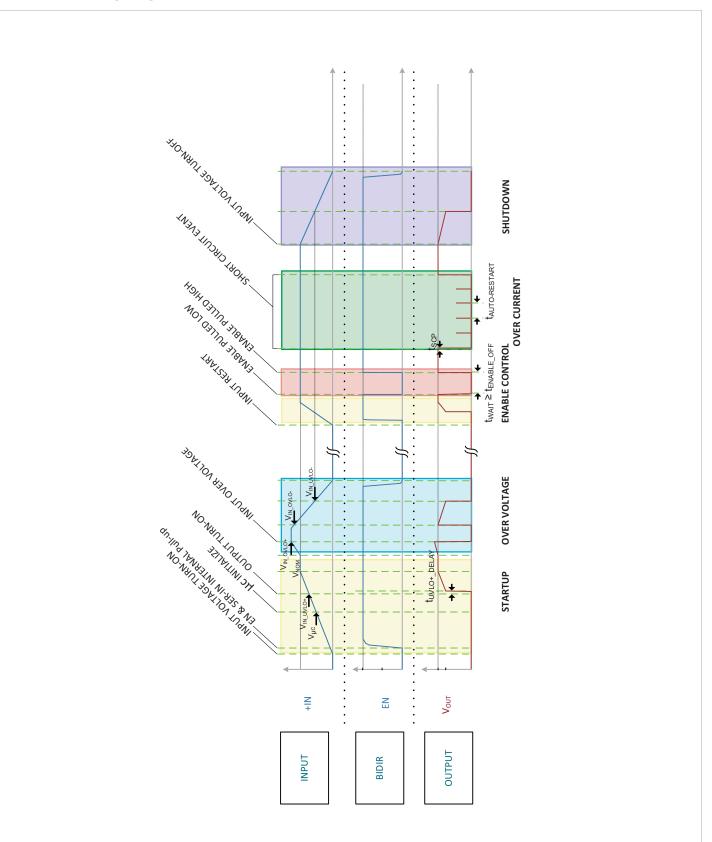
• When held low the BCM internal bias will be disabled and the powertrain will be inactive.

- In an array of BCMs, EN pins should be interconnected to synchronize startup and permit startup into full load conditions.
- Enable / disable command will have no effect if the EN pin is disabled.

		ATTRIBUTE	SYMBOL	CONDITIONS / NOTES	MIN	ТҮР	MAX	UNIT
	Startup	EN to Powertrain active time	t <sub>en_start</sub>	$\label{eq:VIN} \begin{split} V_{\text{IN}} &> V_{\text{IN}_{\text{UVLO+}}},\\ \text{EN held low both conditions satisfied}\\ \text{for }t &> t_{\text{UVLO+}_{\text{DELAY}}} \end{split}$		250		μs
ANALOG INPUT		EN Voltage Threshold	V <sub>ENABLE</sub>		2.3			V
	Regular Operation	EN Resistance (Internal)	R <sub>EN_INT</sub>	Internal pull up resistor		1.5		kΩ
		EN Disable Threshold	V <sub>EN_DISABLE_TH</sub>				1	V



#### **BCM Module Timing diagram**

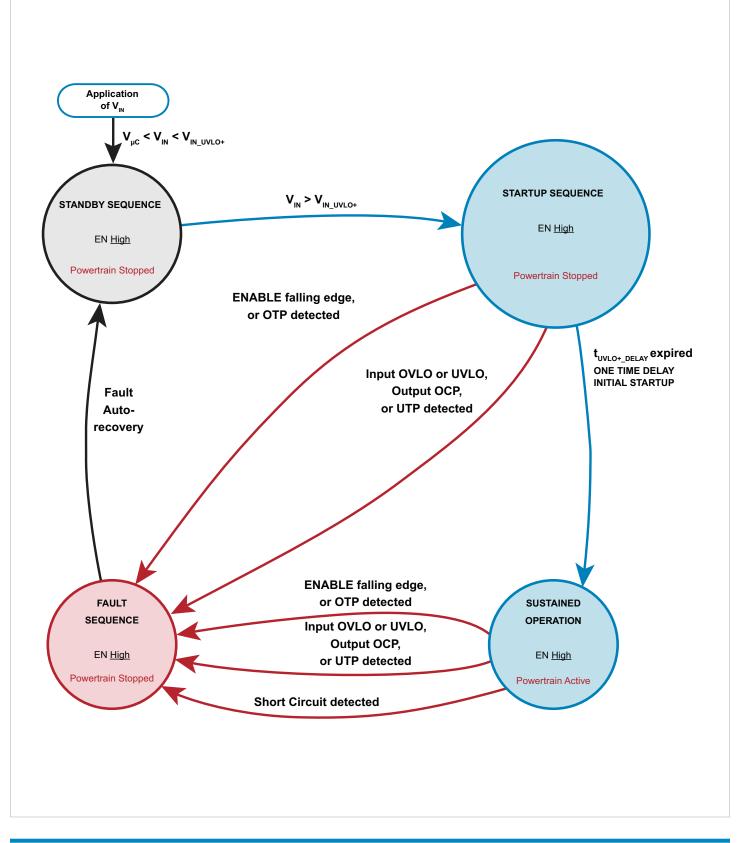


BCM<sup>®</sup> Bus Converter Page 10 of 23



#### **High Level Functional State Diagram**

Conditions that cause state transitions are shown along arrows. Sub-sequence activities listed inside the state bubbles.





#### **Application Characteristics**

Product is mounted and temperature controlled via top side cold plate, unless otherwise noted. See associated figures for general trend data.

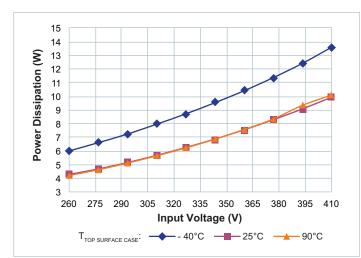
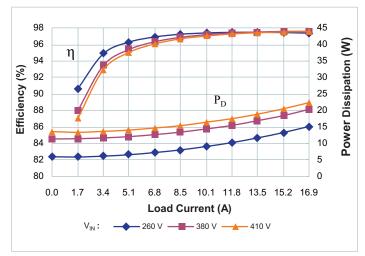
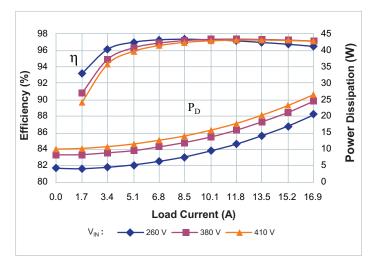


Figure 4 — No load power dissipation vs. V<sub>IN</sub>



**Figure 6** — Efficiency and power dissipation at  $T_{CASE} = -40^{\circ}C$ 



**Figure 8** — Efficiency and power dissipation at  $T_{CASE} = 90^{\circ}C$ 

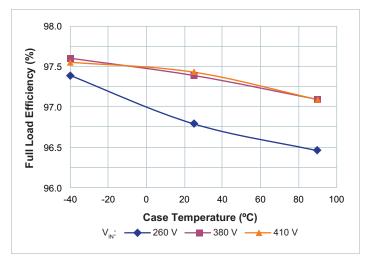
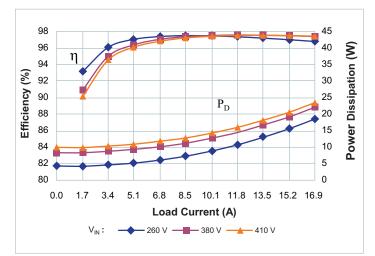


Figure 5 — Full load efficiency vs. temperature; V<sub>IN</sub>



**Figure 7** — Efficiency and power dissipation at  $T_{CASE} = 25^{\circ}C$ 

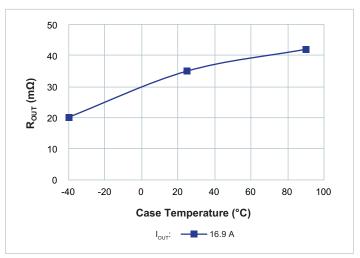
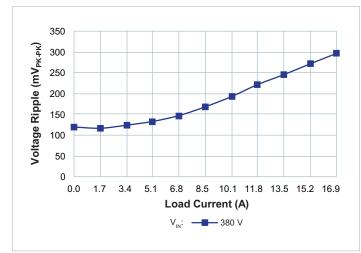
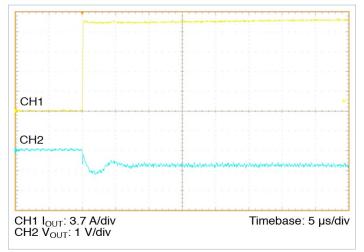


Figure 9 — R<sub>OUT</sub> vs. temperature; Nominal V<sub>IN</sub>





**Figure 10** — V<sub>RIPPLE</sub> vs. I<sub>OUT</sub>; No external C<sub>OUT</sub>. Board mounted module, scope setting : 20 MHz analog BW



**Figure 12** — 0 A– 16.9 A transient response:  $C_{IN} = 270 \ \mu$ F, no external  $C_{OUT}$ 

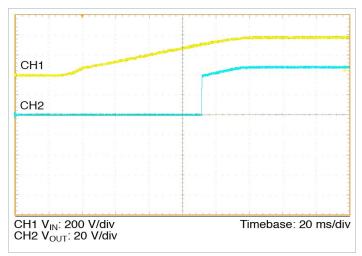
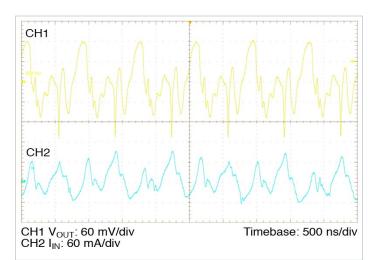
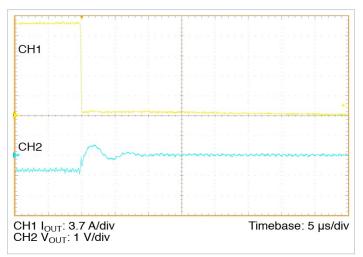


Figure 14 — Start up from application of  $V_{IN}$  = 380 V, 50%  $I_{OUT}$ , 100%  $C_{OUT}$ 



**Figure 11** — Full load ripple, 270 μF C<sub>IN</sub>; No external C<sub>OUT.</sub> Board mounted module, scope setting : 20 MHz analog BW



**Figure 13** — 16.9 A – 0 A transient response:  $C_{IN} = 270 \ \mu$ F, no external  $C_{OUT}$ 

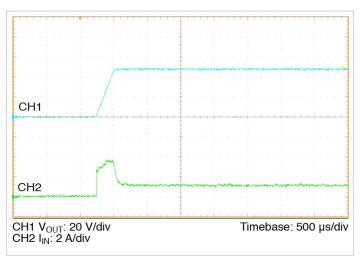


Figure 15 — Start up from application of EN with pre-applied  $V_{IN} = 380 V$ , 50%  $I_{OUT}$ , 100%  $C_{OUT}$ 



#### **General Characteristics**

Specifications apply over all line, load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of  $-40^{\circ}C \le T_{INTERNAL} \le 125^{\circ}C$  (T-Grade); All other specifications are at  $T_{INTERNAL} = 25^{\circ}C$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Тур	Max	Unit	
		Mechanical					
Length	L		62.96 / [2.479]	63.34 / [2.494]	63.72 / [2.509]	mm / [in	
Width	W		22.67 / [0.893]	22.80/[0.898]	22.93 / [0.903]	mm / [in	
Height	Н		7.21 / [0.284]	7.26 / [0.286]	7.31 / [0.288]	mm / [in	
Volume	Vol	Without heatsink		10.48 / [0.640]		cm <sup>3</sup> /[in <sup>3</sup>	
Weight	W			41/[1.45]		g / [oz]	
		Nickel	0.51		2.03		
Lead finish		Palladium	0.02		0.15	μm	
		Gold	0.003		0.051		
		Thermal					
Operating temperature	т	BCM380P475T800A31 (T-Grade)	-40		125	°C	
Operating temperature	T <sub>INTERNAL</sub>	BCM380P475M800A31 (M-Grade)	-55		125	°C	
Thermal resistance top side	філт-тор	Estimated thermal resistance to maximum temperature internal component from isothermal top		1.64		°C/W	
Thermal resistance leads	$\phi_{\text{INT-LEADS}}$	Estimated thermal resistance to maximum temperature internal component from isothermal leads		8.51		°C/W	
Thermal resistance bottom side	філт-воттом	Estimated thermal resistance to maximum temperature internal component from isothermal bottom		2.55		°C/W	
Thermal capacity				34		Ws /°C	
		Assembly					
C	-	BCM380P475T800A31 (T-Grade)	-55		125	°C	
Storage Temperature	T <sub>ST</sub>	BCM380P475M800A31 (M-Grade)	-65		125	°C	
	565	Human Body Model,			1		
	ESD <sub>HBM</sub>	"ESDA / JEDEC JDS-001-2012" Class I-C (1kV to < 2 kV)					
ESD Withstand		Charge Device Model,					
	ESD <sub>CDM</sub>	"JESD 22-C101-E" Class II (200V to < 500V)					



### **General Characteristics (Cont.)**

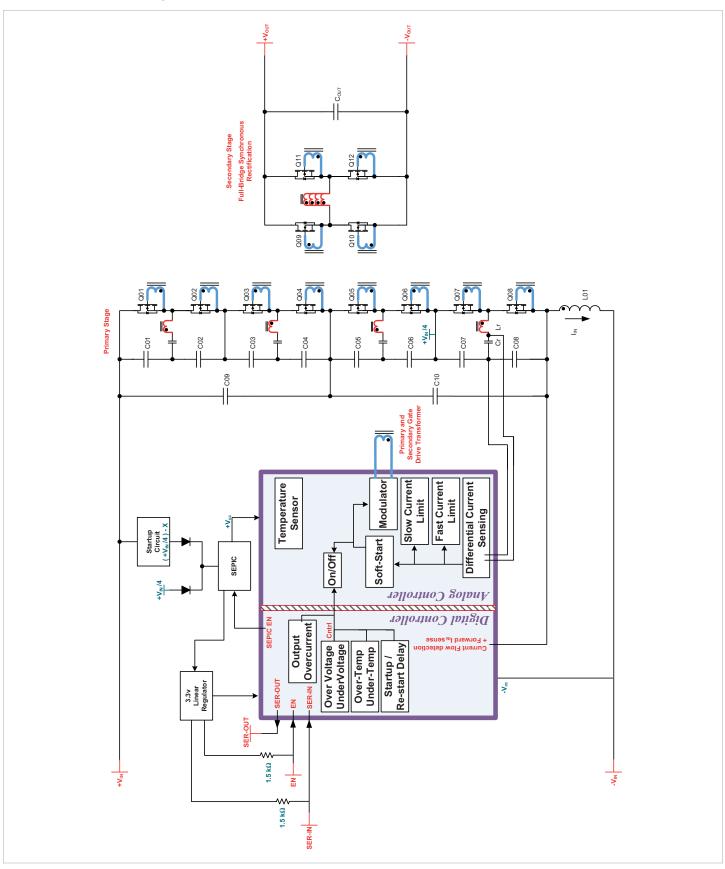
Specifications apply over all line, load conditions, unless otherwise noted; **Boldface** specifications apply over the temperature range of -40°C  $\leq$  T<sub>INTERNAL</sub> = 125°C (T-Grade); All other specifications are at T<sub>INTERNAL</sub> = 25°C unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Тур	Max	Unit
		Soldering <sup>[1]</sup>				
Peak temperature Top case					135	°C
		Safety				
Isolation voltage		IN to OUT	4,242			Vdc
	V <sub>HIPOT</sub>	IN to CASE	2,121			
		OUT to CASE	2,121			
Isolation capacitance	C <sub>IN_OUT</sub>	Unpowered unit	620	780	940	pF
Isolation resistance	R <sub>IN_OUT</sub>	At 500 Vdc	10			MΩ
MTBF		MIL-HDBK-217Plus Parts Count - 25°C Ground Benign, Stationary, Indoors / Computer		2.18		MHrs
		Telcordia Issue 2 - Method I Case III; 25°C Ground Benign, Controlled		7.85		MHrs
Agency approvals / standards		cTUVus				
		cURus				
		CE Marked for Low Voltage Directive and RoHS Recast Directive, as applicable				

<sup>[1]</sup> Product is not intended for reflow solder attach.

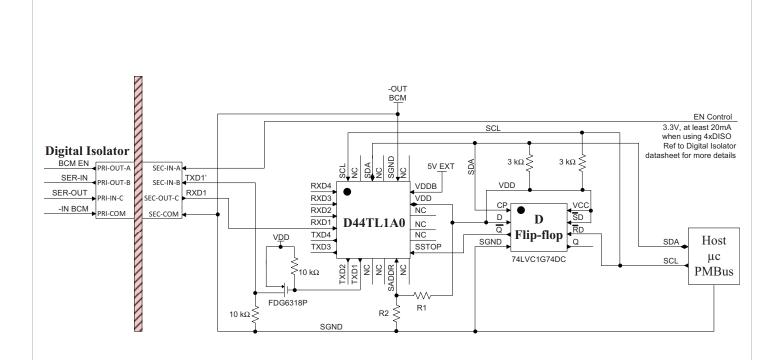


#### **BCM Module Block Diagram**





#### System Diagram



The BCM380y475x800A31 bus converter provides accurate telemetry monitoring and reporting, threshold and warning limits adjustment, in addition to corresponding status flags.

The BCM internal  $\mu$ C is referenced to primary ground. The Digital Isolator allows UART communication interface with the host Digital Supervisor at typical speed of 750 KHz across the isolation barrier. One of the advantages of the Digital Isolator is its low power consumption. Each transmission channel is able to draw its internal bias circuitry directly from the input signal being transmitted to the output with minimal to no signal distortion.

The Digital Supervisor provides the host system  $\mu$ C with access to an array of up to 4 BCMs. This array is constantly polled for status by the Digital Supervisor. Direct communication to individual BCM is enabled by a page command. For example, the page (0x00) prior to a telemetry inquiry points to the Digital Supervisor data and pages (0x01 – 0x04) prior to a telemetry inquiry points to the array of BCMs connected data. The Digital Supervisor constantly polls the BCM data through the UART interface.

The Digital Supervisor enables the PMBus<sup>TM</sup> compatible host interface with an operating bus speed of up to 400 kHz. The Digital Supervisor follows the PMBus command structure and specification.

Please refer to the Digital Supervisor data sheet for more details.



#### Sine Amplitude Converter™ Point of Load Conversion

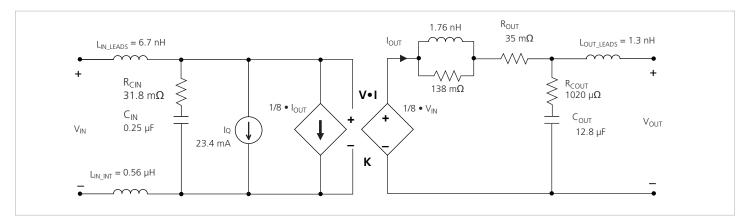


Figure 16 — BCM module AC model

The Sine Amplitude Converter (SAC<sup>™</sup>) uses a high frequency resonant tank to move energy from input to output. (The resonant tank is formed by Cr and leakage inductance Lr in the power transformer windings as shown in the BCM module Block Diagram). The resonant LC tank, operated at high frequency, is amplitude modulated as a function of input voltage and output current. A small amount of capacitance embedded in the input and output stages of the module is sufficient for full functionality and is key to achieving high power density.

The BCM380y475x800A31 SAC can be simplified into the preceeding model.

At no load:

$$V_{OUT} = V_{IN} \bullet K \tag{1}$$

K represents the "turns ratio" of the SAC. Rearranging Eq (1):

$$K = \frac{V_{OUT}}{V_{IN}} \tag{2}$$

In the presence of load, V<sub>OUT</sub> is represented by:

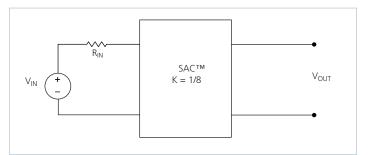
$$V_{OUT} = V_{IN} \bullet K - I_{OUT} \bullet R_{OUT} \tag{3}$$

and I<sub>OUT</sub> is represented by:

$$I_{OUT} = \frac{I_{IN} - I_Q}{K} \tag{4}$$

 $R_{OUT}$  represents the impedance of the SAC, and is a function of the  $R_{DSON}$  of the input and output MOSFETs and the winding resistance of the power transformer.  $I_Q$  represents the quiescent current of the SAC control, gate drive circuitry, and core losses.

The use of DC voltage transformation provides additional interesting attributes. Assuming that  $R_{OUT} = 0 \ \Omega$  and  $I_Q = 0 \ A$ , Eq. (3) now becomes Eq. (1) and is essentially load independent, resistor R is now placed in series with  $V_{IN}$ .



**Figure 17** — *K* = 1/8 Sine Amplitude Converter with series input resistor

The relationship between  $V_{IN}$  and  $V_{OUT}$  becomes:

$$V_{OUT} = (V_{IN} - I_{IN} \bullet R_{IN}) \bullet K$$
<sup>(5)</sup>

Substituting the simplified version of Eq. (4)  $(I_Q \text{ is assumed} = 0 \text{ A})$  into Eq. (5) yields:

$$V_{OUT} = V_{IN} \bullet K - I_{OUT} \bullet R_{IN} \bullet K^2 \tag{6}$$



This is similar in form to Eq. (3), where  $R_{OUT}$  is used to represent the characteristic impedance of the SAC<sup>TM</sup>. However, in this case a real R on the input side of the SAC is effectively scaled by  $K^2$  with respect to the output.

Assuming that  $R=1~\Omega,$  the effective R as seen from the secondary side is 15.6 m $\Omega,$  with K=1/8 .

A similar exercise should be performed with the addition of a capacitor or shunt impedance at the input to the SAC. A switch in series with  $V_{IN}$  is added to the circuit. This is depicted in Figure 18.

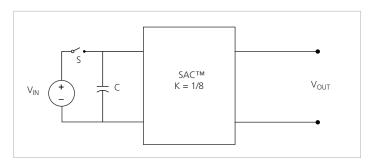


Figure 18 — Sine Amplitude Converter with input capacitor

A change in  $V_{IN}$  with the switch closed would result in a change in capacitor current according to the following equation:

$$I_C(t) = C \frac{dV_{IN}}{dt} \tag{7}$$

Assume that with the capacitor charged to  $V_{IN}$ , the switch is opened and the capacitor is discharged through the idealized SAC. In this case,

$$I_C = I_{OUT} \bullet K \tag{8}$$

substituting Eq. (1) and (8) into Eq. (7) reveals:

$$I_{OUT} = \frac{C}{K^2} \cdot \frac{dV_{OUT}}{dt}$$
(9)

The equation in terms of the output has yielded a  $K^2$  scaling factor for *C*, specified in the denominator of the equation.

A K factor less than unity results in an effectively larger capacitance on the output when expressed in terms of the input. With a K = 1/8 as shown in Figure 18, C=1  $\mu$ F would appear as C=64  $\mu$ F when viewed from the output.

Low impedance is a key requirement for powering a high-current, lowvoltage load efficiently. A switching regulation stage should have minimal impedance while simultaneously providing appropriate filtering for any switched current. The use of a SAC between the regulation stage and the point of load provides a dual benefit of scaling down series impedance leading back to the source and scaling up shunt capacitance or energy storage as a function of its K factor squared. However, the benefits are not useful if the series impedance of the SAC is too high. The impedance of the SAC must be low, i.e. well beyond the crossover frequency of the system.

A solution for keeping the impedance of the SAC low involves switching at a high frequency. This enables small magnetic components because magnetizing currents remain low. Small magnetics mean small path lengths for turns. Use of low loss core material at high frequencies also reduces core losses.

The two main terms of power loss in the BCM module are:

- No load power dissipation (P<sub>NL</sub>): defined as the power used to power up the module with an enabled powertrain at no load.
- Resistive loss (R<sub>OUT</sub>): refers to the power loss across the BCM<sup>®</sup> module modeled as pure resistive impedance.

$$P_{DISSIPATED} = P_{NL} + P_{R_{OUT}} \tag{10}$$

Therefore,

$$P_{OUT} = P_{IN} - P_{DISSIPATED} = P_{IN} - P_{NL} - P_{R_{OUT}}$$
(11)

The above relations can be combined to calculate the overall module efficiency:

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{P_{IN} - P_{NL} - P_{R_{OUT}}}{P_{IN}}$$
(12)

$$= \frac{V_{IN} \bullet I_{IN} - P_{NL} - (I_{OUT})^2 \bullet R_{OUT}}{V_{IN} \bullet I_{IN}}$$

$$= I - \left(\frac{P_{NL} + (I_{OUT})^2 \cdot R_{OUT}}{V_{IN} \cdot I_{IN}}\right)$$



#### Input and Output Filter Design

A major advantage of SAC<sup>™</sup> systems versus conventional PWM converters is that the transformer based SAC does not require external filtering to function properly. The resonant LC tank, operated at extreme high frequency, is amplitude modulated as a function of input voltage and output current and efficiently transfers charge through the isolation transformer. A small amount of capacitance embedded in the input and output stages of the module is sufficient for full functionality and is key to achieving power density.

This paradigm shift requires system design to carefully evaluate external filters in order to:

Guarantee low source impedance:

To take full advantage of the BCM module's dynamic response, the impedance presented to its input terminals must be low from DC to approximately 5 MHz. The connection of the bus converter module to its power source should be implemented with minimal distribution inductance. If the interconnect inductance exceeds 100 nH, the input should be bypassed with a RC damper to retain low source impedance and stable operation. With an interconnect inductance of 200 nH, the RC damper may be as high as 1  $\mu$ F in series with 0.3  $\Omega$ . A single electrolytic or equivalent low-Q capacitor may be used in place of the series RC bypass.

Further reduce input and/or output voltage ripple without sacrificing dynamic response:

Given the wide bandwidth of the module, the source response is generally the limiting factor in the overall system response. Anomalies in the response of the source will appear at the output of the module multiplied by its K factor.

Protect the module from overvoltage transients imposed by the system that would exceed maximum ratings and induce stresses:

The module input/output voltage ranges shall not be exceeded. An internal overvoltage lockout function prevents operation outside of the normal operating input range. Even when disabled, the powertrain is exposed to the applied voltage and power MOSFETs must withstand it.

Total load capacitance at the output of the BCM module shall not exceed the specified maximum. Owing to the wide bandwidth and low output impedance of the module, low-frequency bypass capacitance and significant energy storage may be more densely and efficiently provided by adding capacitance at the input of the module. At frequencies <500 kHz the module appears as an impedance of R<sub>OUT</sub> between the source and load.

Within this frequency range, capacitance at the input appears as effective capacitance on the output per the relationship defined in Eq. (13).

$$C_{OUT} = \frac{C_{IN}}{K^2} \tag{13}$$

This enables a reduction in the size and number of capacitors used in a typical system.

#### **Thermal Considerations**

The ChiP package provides a high degree of flexibility in that it presents three pathways to remove heat from internal power dissipating components. Heat may be removed from the top surface, the bottom surface and the leads. The extent to which these three surfaces are cooled is a key component for determining the maximum power that is available from a ChiP, as can be seen from Figure 1.

Since the ChiP has a maximum internal temperature rating, it is necessary to estimate this internal temperature based on a real thermal solution. Given that there are three pathways to remove heat from the ChiP, it is helpful to simplify the thermal solution into a roughly equivalent circuit where power dissipation is modeled as a current source, isothermal surface temperatures are represented as voltage sources and the thermal resistances are represented as resistors. Figure 19 shows the "thermal circuit" for a VI Chip® BCM module 6123 in an application where the top, bottom, and leads are cooled. In this case, the BCM power dissipation is PD<sub>TOTAL</sub> and the three surface temperatures are represented as T<sub>CASE\_DOP</sub>. T<sub>CASE\_BOTTOM</sub>, and T<sub>LEADS</sub>. This thermal system can now be very easily analyzed using a SPICE simulator with simple resistors, voltage sources, and a current source. The results of the simulation would provide an estimate of heat flow through the various pathways as well as internal temperature.

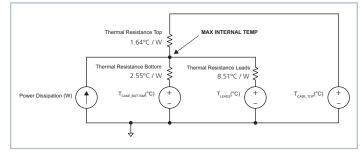


Figure 19 — Double side cooling and leads thermal model

Alternatively, equations can be written around this circuit and analyzed algebraically:

$$T_{INT} - PD_1 \bullet 1.24 = T_{CASE\_TOP}$$
  
 $T_{INT} - PD_2 \bullet 1.24 = T_{CASE\_BOTTOM}$ 

 $T_{INT} - PD_3 \bullet 7 = T_{LEADS}$ 

 $PD_{TOTAL} = PD_1 + PD_2 + PD_3$ 

Where  $T_{\rm INT}$  represents the internal temperature and PD<sub>1</sub>, PD<sub>2</sub>, and PD<sub>3</sub> represent the heat flow through the top side, bottom side, and leads respectively.

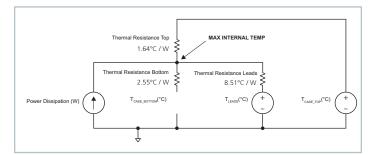


Figure 20 — One side cooling and leads thermal model



Figure 20 shows a scenario where there is no bottom side cooling. In this case, the heat flow path to the bottom is left open and the equations now simplify to:

 $T_{INT} - PD_1 \bullet 1.24 = T_{CASE\_TOP}$  $T_{INT} - PD_3 \bullet 7 = T_{LEADS}$  $PD_{TOTAL} = PD_1 + PD_3$ 

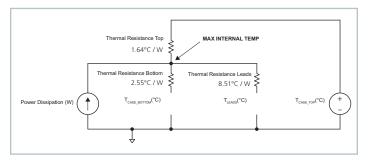


Figure 21 — One side cooling thermal model

Figure 21 shows a scenario where there is no bottom side and leads cooling. In this case, the heat flow path to the bottom is left open and the equations now simplify to:

 $T_{INT} - PD_1 \bullet 1.24 = T_{CASE\_TOP}$ 

 $PD_{TOTAL} = PD_1$ 

Please note that Vicor has a suite of online tools, including a simulator and thermal estimator which greatly simplify the task of determining whether or not a BCM thermal configuration is valid for a given condition. These tools can be found at:

http://www.vicorpower.com/powerbench.

### **Current Sharing**

The performance of the SAC<sup>™</sup> topology is based on efficient transfer of energy through a transformer without the need of closed loop control. For this reason, the transfer characteristic can be approximated by an ideal transformer with a positive temperature coefficient series resistance.

This type of characteristic is close to the impedance characteristic of a DC power distribution system both in dynamic (AC) behavior and for steady state (DC) operation.

When multiple BCM modules of a given part number are connected in an array they will inherently share the load current according to the equivalent impedance divider that the system implements from the power source to the point of load.

Some general recommendations to achieve matched array impedances include:

- Dedicate common copper planes within the PCB to deliver and return the current to the modules.
- Provide as symmetric a PCB layout as possible among modules
- An input filter is required for an array of BCMs in order to prevent circulating currents.

For further details see <u>AN:016 Using BCM Bus Converters</u> in High Power Arrays.

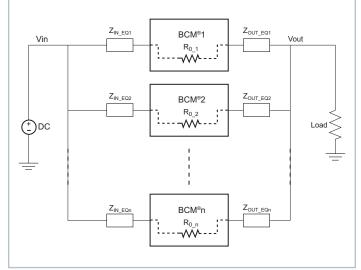


Figure 22 — BCM module array

#### **Fuse Selection**

In order to provide flexibility in configuring power systems VI Chip® modules are not internally fused. Input line fusing of VI Chip products is recommended at system level to provide thermal protection in case of catastrophic failure.

The fuse shall be selected by closely matching system requirements with the following characteristics:

- Current rating (usually greater than maximum current of BCM module)
- Maximum voltage rating
  - (usually greater than the maximum possible input voltage)
- Ambient temperature
- Nominal melting I<sup>2</sup>t
- Recommend fuse: ≤ 5 A Bussmann PC-Tron

#### **Reverse Operation**

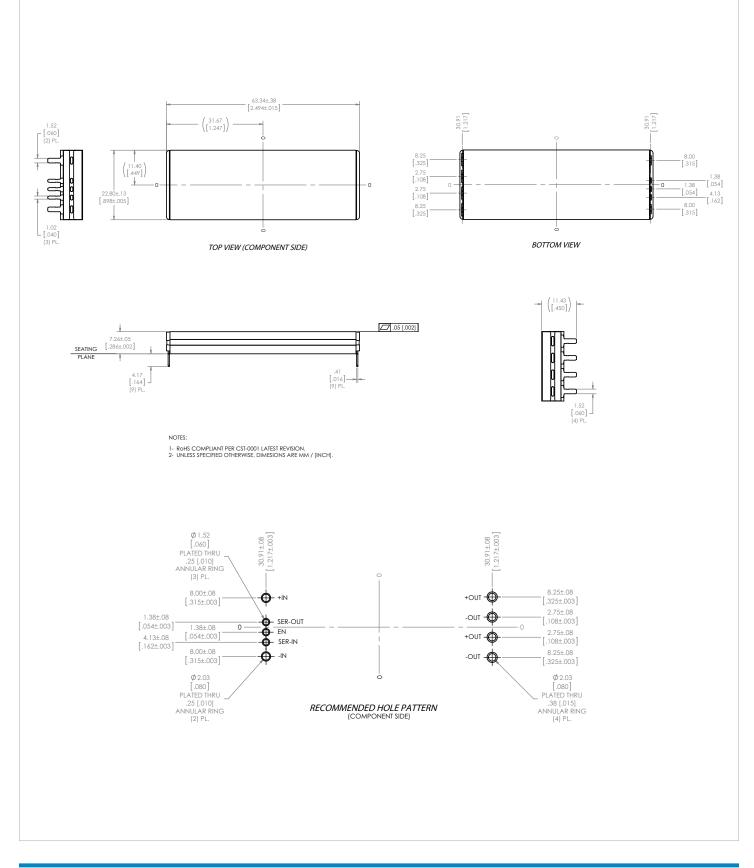
BCM modules are capable of reverse power operation. Once the unit is started, energy will be transferred from secondary back to the primary whenever the secondary voltage exceeds  $V_{IN} \bullet K$ . The module will continue operation in this fashion for as long as no faults occur.

The BCM380y475x800A31 has not been qualified for continuous operation in a reverse power condition. Furthermore fault protections which help protect the module in forward operation will not fully protect the module in reverse operation.

Transient operation in reverse is expected in cases where there is significant energy storage on the output and transient voltages appear on the input. Transient reverse power operation of less than 10 ms, 10% duty cycle is permitted and has been qualified to cover these cases.



### BCM Module Through Hole Package Mechanical Drawing and Recommended Land Pattern





#### Vicor's comprehensive line of power solutions includes high density AC-DC and DC-DC modules and accessory components, fully configurable AC-DC and DC-DC power supplies, and complete custom power systems.

Information furnished by Vicor is believed to be accurate and reliable. However, no responsibility is assumed by Vicor for its use. Vicor makes no representations or warranties with respect to the accuracy or completeness of the contents of this publication. Vicor reserves the right to make changes to any products, specifications, and product descriptions at any time without notice. Information published by Vicor has been checked and is believed to be accurate at the time it was printed; however, Vicor assumes no responsibility for inaccuracies. Testing and other quality controls are used to the extent Vicor deems necessary to support Vicor's product warranty. Except where mandated by government requirements, testing of all parameters of each product is not necessarily performed.

Specifications are subject to change without notice.

#### **Vicor's Standard Terms and Conditions**

All sales are subject to Vicor's Standard Terms and Conditions of Sale, which are available on Vicor's webpage or upon request.

#### **Product Warranty**

In Vicor's standard terms and conditions of sale, Vicor warrants that its products are free from non-conformity to its Standard Specifications (the "Express Limited Warranty"). This warranty is extended only to the original Buyer for the period expiring two (2) years after the date of shipment and is not transferable.

UNLESS OTHERWISE EXPRESSLY STATED IN A WRITTEN SALES AGREEMENT SIGNED BY A DULY AUTHORIZED VICOR SIGNATORY, VICOR DISCLAIMS ALL REPRESENTATIONS, LIABILITIES, AND WARRANTIES OF ANY KIND (WHETHER ARISING BY IMPLICATION OR BY OPERATION OF LAW) WITH RESPECT TO THE PRODUCTS, INCLUDING, WITHOUT LIMITATION, ANY WARRANTIES OR REPRESENTATIONS AS TO MERCHANTABILITY, FITNESS FOR PARTICULAR PURPOSE, INFRINGEMENT OF ANY PATENT, COPYRIGHT, OR OTHER INTELLECTUAL PROPERTY RIGHT, OR ANY OTHER MATTER.

This warranty does not extend to products subjected to misuse, accident, or improper application, maintenance, or storage. Vicor shall not be liable for collateral or consequential damage. Vicor disclaims any and all liability arising out of the application or use of any product or circuit and assumes no liability for applications assistance or buyer product design. Buyers are responsible for their products and applications using Vicor products and components. Prior to using or distributing any products that include Vicor components, buyers should provide adequate design, testing and operating safeguards.

Vicor will repair or replace defective products in accordance with its own best judgment. For service under this warranty, the buyer must contact Vicor to obtain a Return Material Authorization (RMA) number and shipping instructions. Products returned without prior authorization will be returned to the buyer. The buyer will pay all charges incurred in returning the product to the factory. Vicor will pay all reshipment charges if the product was defective within the terms of this warranty.

#### Life Support Policy

VICOR'S PRODUCTS ARE NOT AUTHORIZED FOR USE AS CRITICAL COMPONENTS IN LIFE SUPPORT DEVICES OR SYSTEMS WITHOUT THE EXPRESS PRIOR WRITTEN APPROVAL OF THE CHIEF EXECUTIVE OFFICER AND GENERAL COUNSEL OF VICOR CORPORATION. As used herein, life support devices or systems are devices which (a) are intended for surgical implant into the body, or (b) support or sustain life and whose failure to perform when properly used in accordance with instructions for use provided in the labeling can be reasonably expected to result in a significant injury to the user. A critical component is any component in a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system or to affect its safety or effectiveness. Per Vicor Terms and Conditions of Sale, the user of Vicor products and components in life support applications assumes all risks of such use and indemnifies Vicor against all liability and damages.

#### **Intellectual Property Notice**

Vicor and its subsidiaries own Intellectual Property (including issued U.S. and Foreign Patents and pending patent applications) relating to the products described in this data sheet. No license, whether express, implied, or arising by estoppel or otherwise, to any intellectual property rights is granted by this document. Interested parties should contact Vicor's Intellectual Property Department.

The products described on this data sheet are protected by the following U.S. Patents Numbers: 5,945,130; 6,403,009; 6,710,257; 6,911,848; 6,930,893; 6,934,166; 6,940,013; 6,969,909; 7,038,917; 7,145,186; 7,166,898; 7,187,263; 7,202,646; 7,361,844; D496,906; D505,114; D506,438; D509,472; and for use under 6,975,098 and 6,984,965.

Vicor Corporation 25 Frontage Road Andover, MA, USA 01810 Tel: 800-735-6200 Fax: 978-475-6715

email

Customer Service: <u>custserv@vicorpower.com</u> Technical Support: <u>apps@vicorpower.com</u>





Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;

- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);

- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;

- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком):

- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



Телефон: 8 (812) 309-75-97 (многоканальный) Факс: 8 (812) 320-03-32 Электронная почта: ocean@oceanchips.ru Web: http://oceanchips.ru/ Адрес: 198099, г. Санкт-Петербург, ул. Калинина, д. 2, корп. 4, лит. А