

### POWER MANAGEMENT

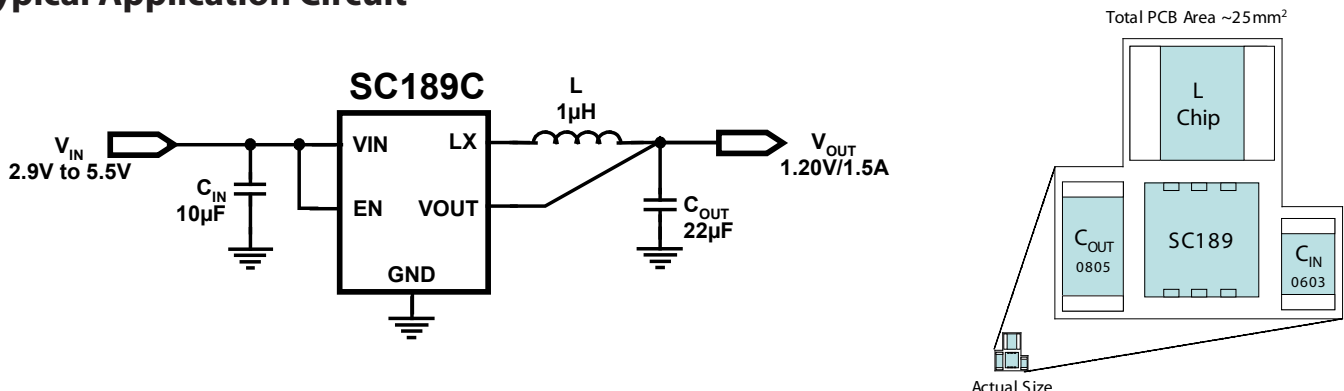
#### Features

- $V_{IN}$  Range: 2.9 – 5.5V
- $V_{OUT}$  Options: 1.0 - 3.3V
- Up to 1.5A Output Current
- Ultra-Small Footprint, <1mm Height Solution
- 2.5MHz Switching Frequency
- Efficiency Up to 93%
- Low Output Noise Across Load Range
- Excellent Transient Response
- Start Up into Pre-Bias Output
- 100% Duty-Cycle Low Dropout Operation
- <1 $\mu$ A Shutdown Current
- Internal Soft Start
- Input Under-Voltage Lockout
- Output Over-Voltage, Current Limit Protection
- Over-Temperature Protection
- Adjustable Output Voltage
- Available in SOT23-5 package and 2mm x 2mm x 0.6mm thermally enhanced MLPD-UT6 package
- -40 to +85°C Temperature Range
- Fully WEEE and RoHS Compliant

#### Applications

- Bluetooth Radios
- DSC and PMPs
- GPS Devices
- xDSL Systems
- POL Regulators
- Portable HDD
- Wireless LAN

#### Typical Application Circuit



#### Description

The SC189 is a high efficiency, synchronous step-down regulator providing up to 1.5A output current in either an ultra-small 2mm x 2mm, low profile package or a low cost SOT23-5 package. The device requires only three external filter components for a complete step down regulator solution. The input voltage range is 2.9 to 5.5V with either factory programmed outputs from 1.0 to 3.3V or adjustable output via an external resistor divider.

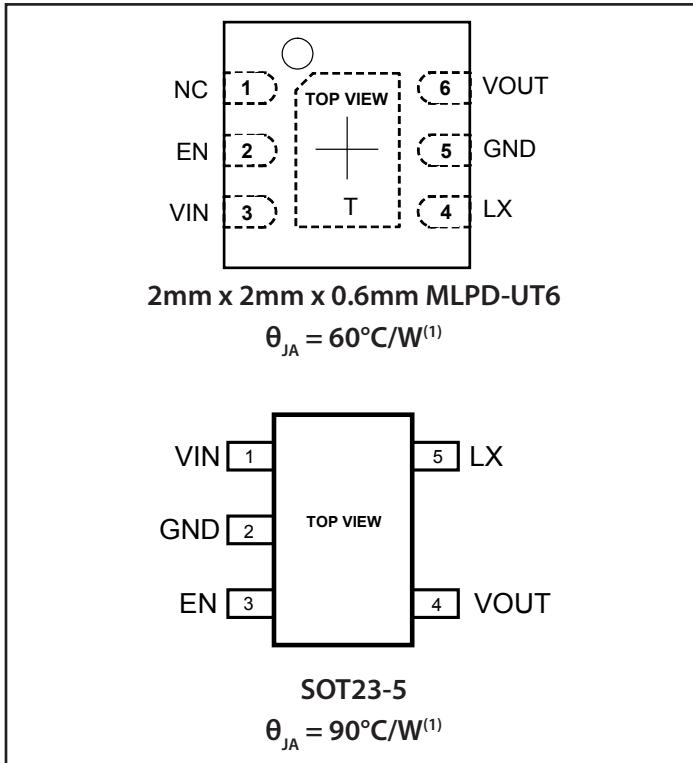
The converter operates at fixed 2.5MHz switching frequency allowing small L/C filtering components. The voltage mode architecture is compatible with chip inductors and capacitors for minimum PCB footprint and lowest overall system cost. Total footprint of 25mm<sup>2</sup> can be achieved - making the SC189 the ideal solution for high density systems. Solution height of <1mm is also possible.

Up to 93% efficiency is achieved with low  $R_{DS(ON)}$  internal switches. PWM constant frequency operation ensures low output ripple across the load range. 100% duty-cycle provides 360mV dropout voltage at 1.5A which extends the minimum input voltage for 2.5V and 3.3V outputs. Excellent transient response is achieved with no external compensation components.

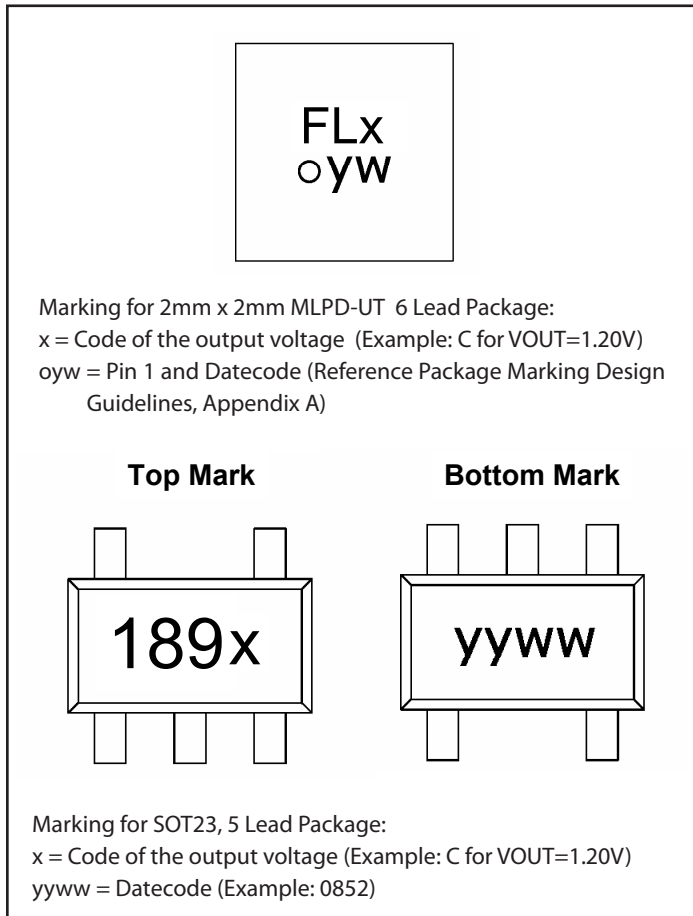
The SC189 provides input under-voltage, output over-voltage, output short circuit and over-temperature protection to safeguard the device and system under fault conditions. The regulator provides integrated soft-start to minimize inrush currents. Standby quiescent current is less than 1 $\mu$ A.

The SC189 is available in SOT23-5 and a thermally enhanced 2mm x 2mm x 0.6mm MLPD-UT6 package.

### Pin Configuration



### Marking Information



### Ordering Information

Device	Package & Description
SC189xULTRT <sup>(2)(3)(4)</sup>	2mm x 2mm x 0.6mm MLPD-UT6
SC189xSKTRT <sup>(2)(3)(4)</sup>	SOT23-5
SC189xEVB <sup>(5)</sup>	Evaluation Board for MLPD-UT6 - Standard Size (i.e., Wire Wound Inductor)
SC189xEVB-1 <sup>(5)</sup>	Evaluation Board for MLPD-UT6 - Small Size (i.e., Chip Inductor)
SC189xEVB-2 <sup>(5)</sup>	Evaluation Board for SOT23-5 - Standard Size (i.e., Wire Wound Inductor)
SC189xEVB-3 <sup>(5)</sup>	Evaluation Board for SOT23-5 - Small Size (i.e., Chip Inductor)

Notes:

- Measured in free convection, mounted on 10mm x 10mm, 2 layer FR4 PCB shown in figure 7 ( for MLPD-UT6 package) and figure 8 ( for SOT23-5 package) with copper of 1oz for each layer.
- Available in tape and reel only. A reel contains 3,000 devices.
- Available in lead-free package only. Device is WEEE and RoHS compliant.
- "x" is the code of the output voltage. See Table 1 for the code. For example, the device number for VOUT= 1.20V is SC189CULTRT.
- "x" is the code of the output voltage. See Table 1 for the code. For example, the EVB for MLPD-UT6 package with VOUT= 1.20V is SC189CEVB (Standard Size) or SC189CEVB-1 (Small Size).

**Table 1: Available Output Voltages**

Code for MLPD-UT6	Code for SOT23-5	VOUT <sup>(1)</sup>
A	A	1.00
B	B	1.10
C	C	1.20
E	Not Available	1.28
F	Not Available	1.30
H	H	1.50
L	L	1.80
N	Not Available	2.00
T	Y	2.50
Not Available	V	2.70
Z	Z	3.30

Notes:

- Contact factory for unavailable output voltage options.

## Absolute Maximum Ratings

VIN Supply Voltage	-0.3 to 6.0V
LX Voltage	-1 to $V_{IN}+1V$ , -3V (20ns Max), 6V Max
VOOUT Voltage	-0.3 to $V_{IN}+0.3V$
EN Voltage	-0.3 to $V_{IN}+0.3V$
Peak IR Reflow temperature	260°C
ESD Protection Level <sup>(2)</sup>	3kV

## Recommended Operating Conditions

VIN Supply Voltage	2.9 to 5.5V
Maximum Output Current <sup>(3)</sup>	1.5A

## Thermal Information

Thermal Resistance, Junction to Ambient<sup>(1)</sup>

MLPD-UT6 Package	60°C/W
SOT23-5 Package	90°C/W
Operating Junction Temperature	-40 to +125°C
Maximum Junction Temperature	+150°C
Storage Temperature Range	-65 to +150°C

Exceeding the absolute maximum ratings may result in permanent damage to the device and/or device malfunction. Operation outside of the parameters specified in the Electrical Characteristics section is not recommended.

### NOTES:

- (1) Measured in free convection, mounted on 10mm x 10mm, 2 layer FR4 PCB shown in figure 7 ( for MLPD-UT6 package) and figure 8 ( for SOT23-5 package) with copper of 1oz for each layer.
- (2) Tested according to JEDEC standard JESD22-A114-B.
- (3) For SOT23-5 package, the limit of the maximum power dissipation shown in figure 2 may reduce the maximum output current.

## Electrical Characteristics

Unless specified:  $V_{IN}=5.0V$ ,  $C_{IN}=10\mu F$ ,  $C_{OUT}=10\mu F$ ;  $L=2.2\mu H$ ;  $-40^{\circ}C < T_A < +85^{\circ}C$ ;  $T_{J(MAX)}=125^{\circ}C$ ; Unless otherwise noted typical values are  $T_A=+25^{\circ}C$ .

Parameter	Symbol	Conditions	Min	Typ	Max	Units
Under-Voltage Lockout	UVLO	Rising $V_{IN}$	2.60	2.70	2.80	V
		Hysteresis		250		mV
Output Voltage Tolerance <sup>(1)</sup>	$\Delta V_{OUT}$	$V_{IN}=3.6V$ to $5.0V$ ; No Load	-2.5		+2.5	%
Current Limit	$I_{LIMIT}$	Peak inductor current	2.0			A
VIN Supply Current	$I_Q$	EN= VIN, No Load		7.5		mA
VIN Shutdown Current	$I_{SHDN}$	EN= GND		1	10	$\mu A$
High Side Switch Resistance	$R_{DSON\_P}$	$I_{LX}= 100mA$ , for MLPD-UT6		0.13		$\Omega$
		$I_{LX}= -100mA$ , for SOT23-5		0.15		
Low Side Switch Resistance	$R_{DSON\_N}$	$I_{LX}= -100mA$ , for MLPD-UT6		0.10		$\Omega$
		$I_{LX}= -100mA$ , for SOT23-5		0.125		
LX Leakage Current	$I_{LK(LX)}$	$V_{IN}=5.5V$ ; $L_X=0V$ ; EN=GND		1	10	$\mu A$
		$V_{IN}=5.5V$ ; $L_X=5.0V$ ; EN=GND	-10	-1		
Line Regulation	$\Delta V_{LINE-REG}$	$V_{IN}= 3.6 - 5.0V$ ; $I_{OUT}=0A$		$\pm 1.0$		%
Load Regulation <sup>(2)</sup>	$\Delta V_{LOAD-REG}$	$V_{IN}= 5.0V$ ; $I_{OUT}=10mA - 1.5A$		$\pm 1.0$		%
Oscillator Frequency	$F_{OSC}$		2.0	2.5	3.0	MHz
Soft-Start Time <sup>(2)</sup>	$T_{SS}$			100		$\mu s$
EN Input High Current	$I_{EN\_HI}$	EN=VIN	-2.0		2.0	$\mu A$

## Electrical Characteristics (continued)

Unless specified:  $V_{IN} = 5.0V$ ,  $C_{IN} = 10\mu F$ ,  $C_{OUT} = 10\mu F$ ;  $L = 2.2\mu H$ ;  $-40^{\circ}C < T_A < +85^{\circ}C$ ;  $T_{J(MAX)} = 125^{\circ}C$ ; Unless otherwise noted typical values are  $T_A = +25^{\circ}C$ .

Parameter	Symbol	Conditions	Min	Typ	Max	Units
EN Input Low Current	$I_{EN\_LO}$	EN=GND	-2.0		2.0	$\mu A$
EN Input High Threshold	$V_{EN\_HI}$		1.2			V
EN Input Low Threshold	$V_{EN\_LO}$				0.4	V
VOUT Over Voltage Protection <sup>(2)</sup>	$V_{OVP}$			115		%
Thermal Shutdown Temperature <sup>(2)</sup>	$T_{SD}$	Junction Temperature		+160		$^{\circ}C$
Thermal Shutdown Hysteresis <sup>(2)</sup>	$T_{SD\_HYS}$	Junction Temperature		10		$^{\circ}C$

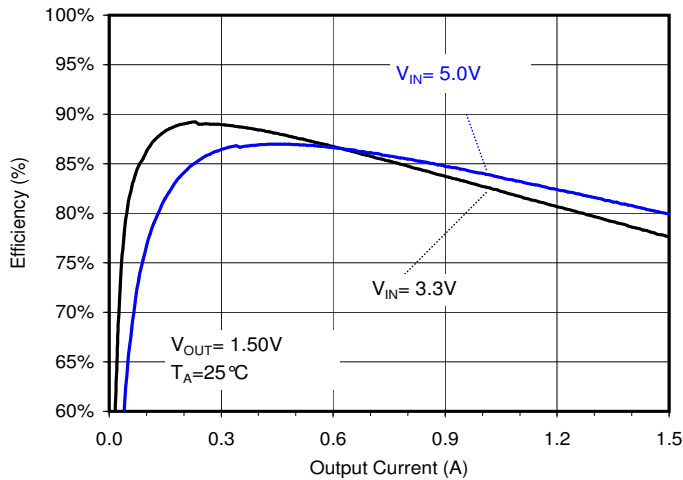
Notes:

- (1) The "Output Voltage Tolerance" includes output voltage accuracy, voltage drift over temperature and the line regulation.
- (2) Guaranteed by design.

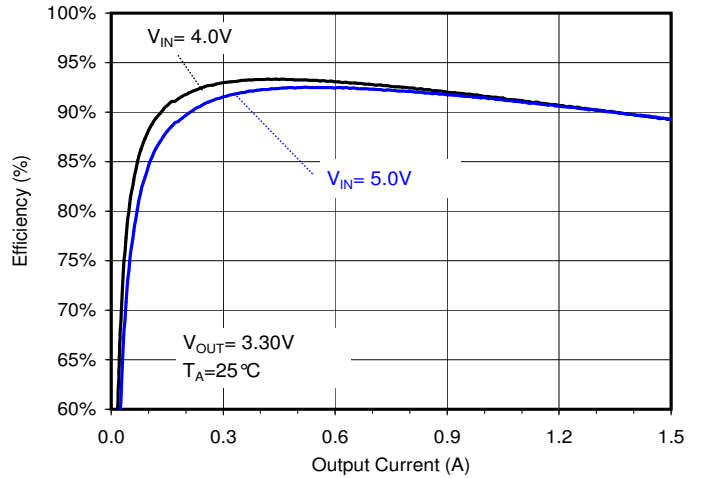
## Typical Characteristics

Circuit Conditions:  $C_{IN} = 10\mu\text{F}/6.3\text{V}$ ;  $C_{OUT} = 10\mu\text{F}/6.3\text{V}$  for  $L=2.2\mu\text{H}$ ;  $C_{OUT} = 22\mu\text{F}/6.3\text{V}$  for  $L=1\mu\text{H}$ .  
 Unless otherwise noted,  $L = 2.2\mu\text{H}$  (TOKO: 1071AS-2R2M) and SC189 in MLPD-UT6 package.

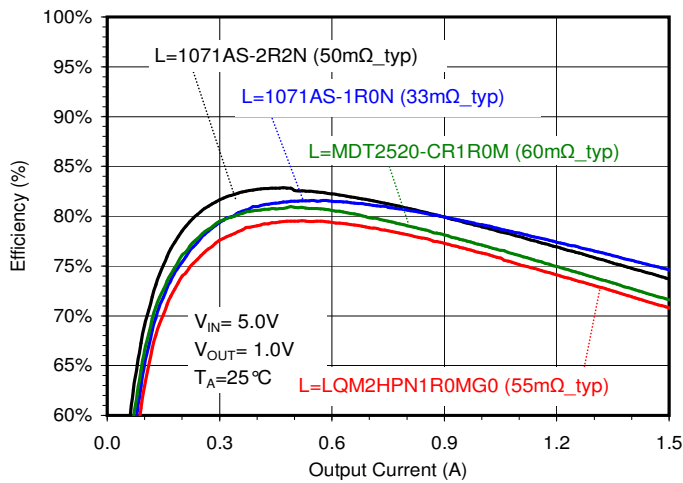
**Efficiency vs. Load Current ( $V_{OUT}=1.5\text{V}$ )**



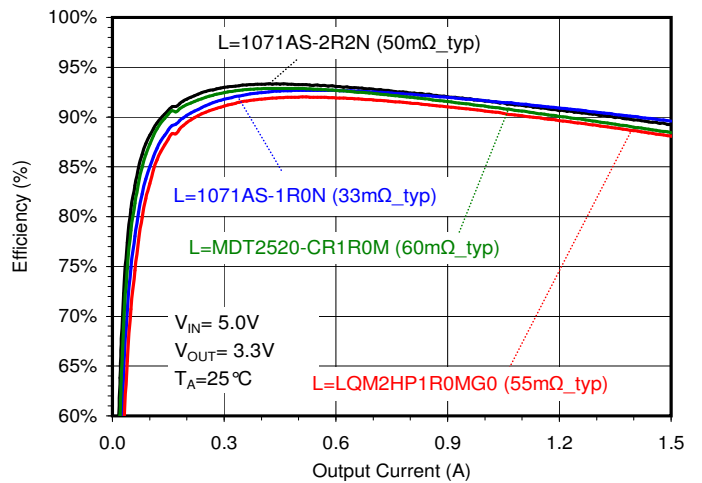
**Efficiency vs. Load Current ( $V_{OUT}=3.3\text{V}$ )**



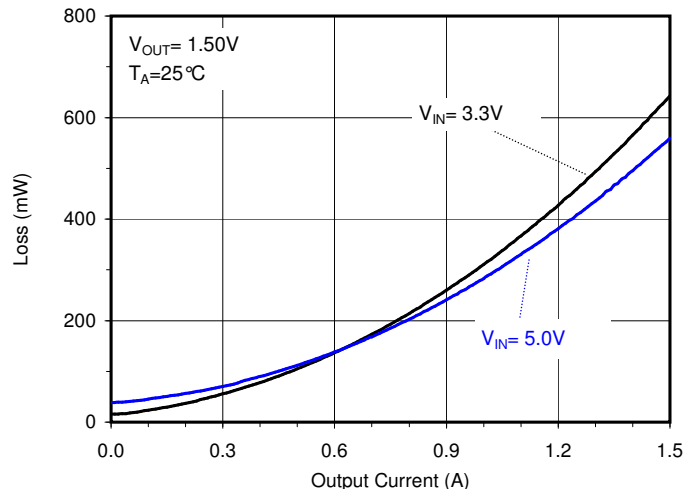
**Efficiency vs. Load Current ( $V_{IN}=5.0\text{V}, V_{OUT}=1.0\text{V}$ )**



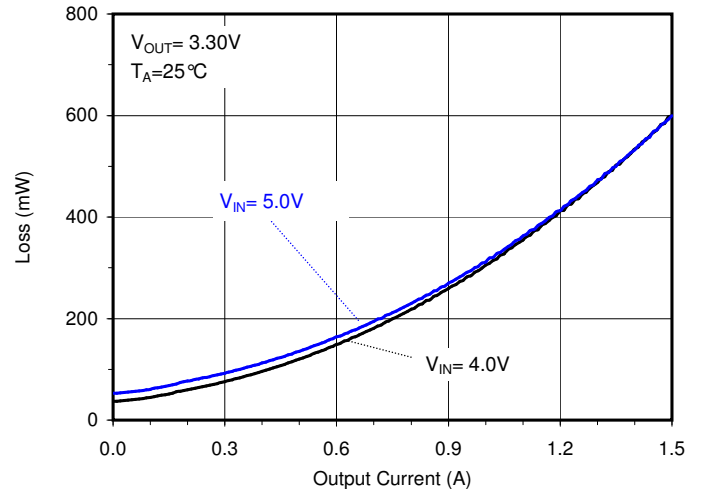
**Efficiency vs. Load Current ( $V_{IN}=5.0\text{V}, V_{OUT}=3.3\text{V}$ )**



**Total Loss vs. Load Current ( $V_{OUT}=1.5\text{V}$ )**



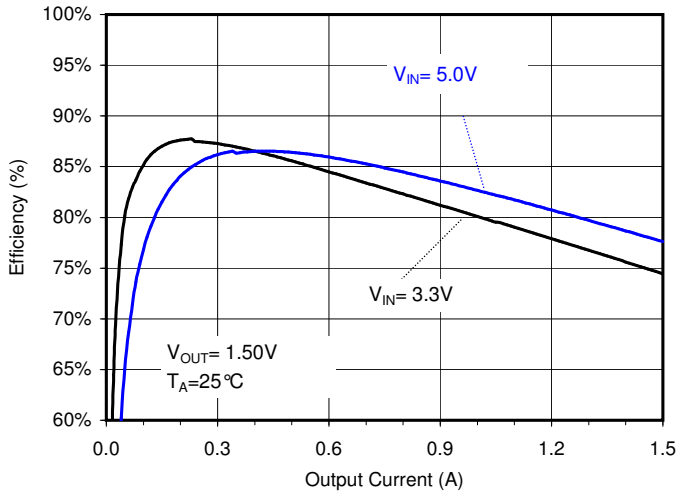
**Total Loss vs. Load Current ( $V_{OUT}=3.3\text{V}$ )**



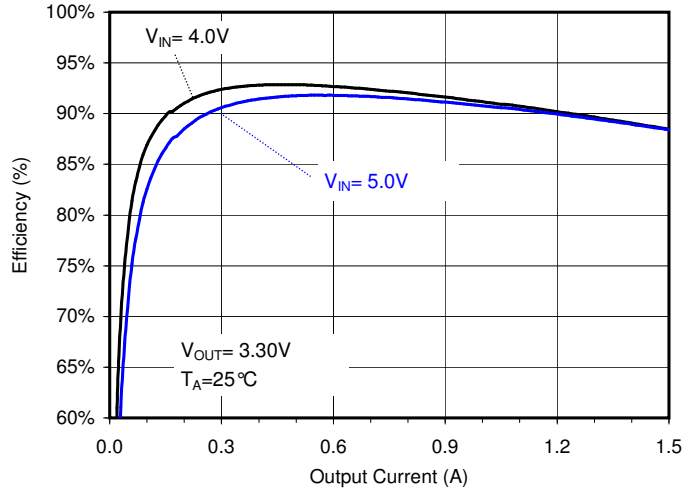
## Typical Characteristics (continued)

Circuit Conditions:  $C_{IN} = 10\mu\text{F}/6.3\text{V}$ ;  $C_{OUT} = 10\mu\text{F}/6.3\text{V}$  for  $L=2.2\mu\text{H}$ ;  $C_{OUT} = 22\mu\text{F}/6.3\text{V}$  for  $L=1\mu\text{H}$ .  
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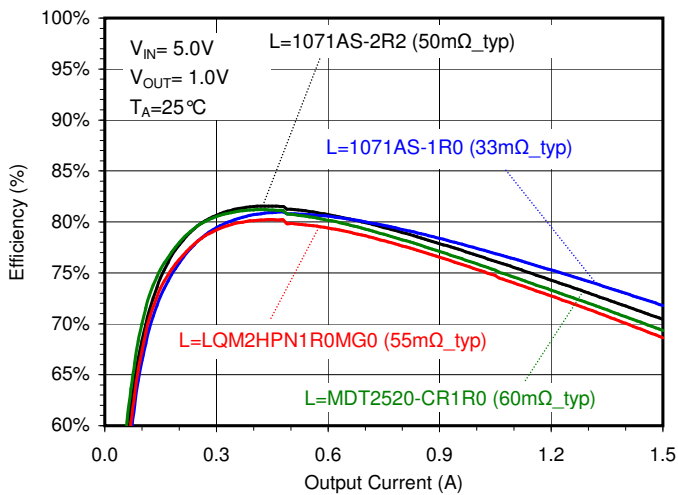
**Efficiency vs. Load Current ( $V_{OUT}=1.5\text{V}$ , SOT23-5)**



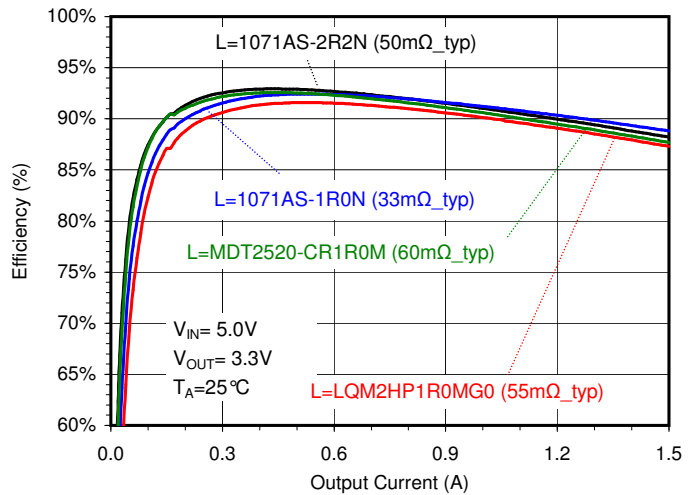
**Efficiency vs. Load Current ( $V_{OUT}=3.3\text{V}$ , SOT23-5)**



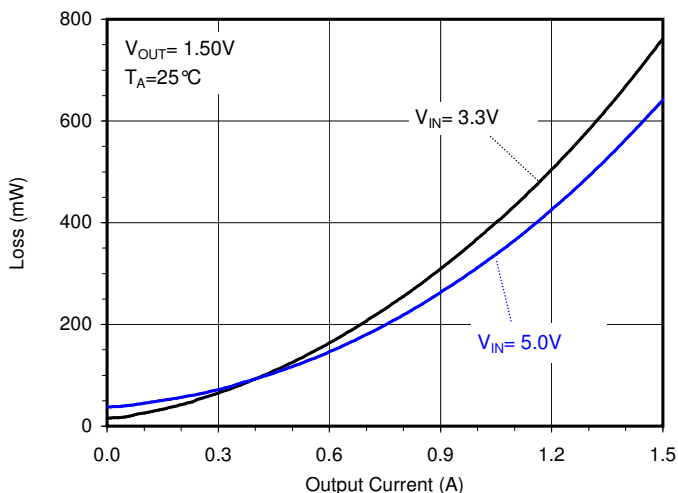
**Efficiency vs. Load Current (SOT23-5)**



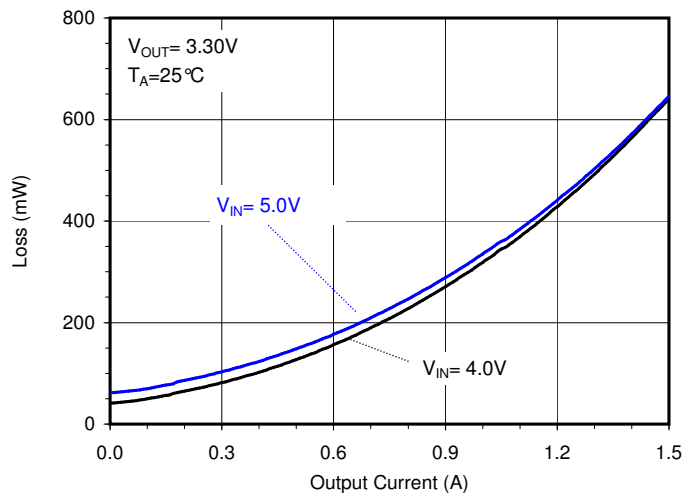
**Efficiency vs. Load Current (SOT23-5)**



**Total Loss vs. Load Current ( $V_{OUT}=1.5\text{V}$ , SOT23-5)**



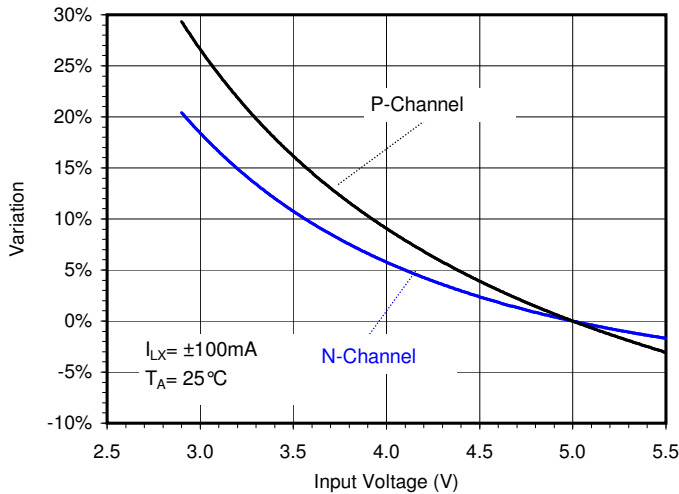
**Total Loss vs. Load Current ( $V_{OUT}=3.3\text{V}$ , SOT23-5)**



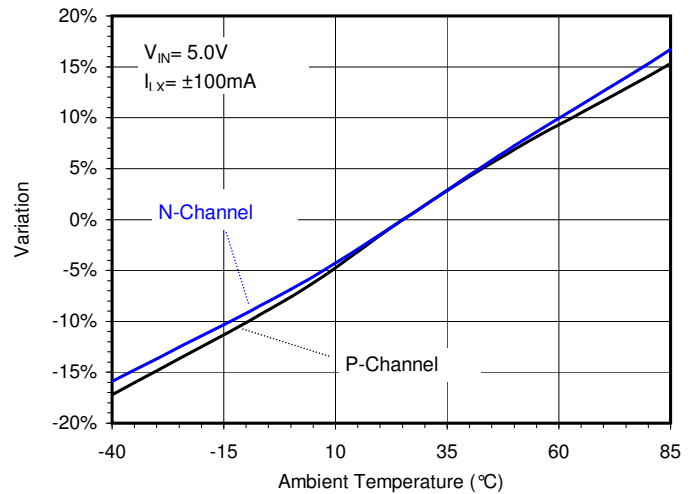
## Typical Characteristics (continued)

Circuit Conditions:  $C_{IN} = 10\mu\text{F}/6.3\text{V}$ ;  $C_{OUT} = 10\mu\text{F}/6.3\text{V}$  for  $L=2.2\mu\text{H}$ ;  $C_{OUT} = 22\mu\text{F}/6.3\text{V}$  for  $L=1\mu\text{H}$ .  
 Unless otherwise noted,  $L = 2.2\mu\text{H}$  (TOKO: 1071AS-2R2M) and SC189 in MLPD-UT6 package.

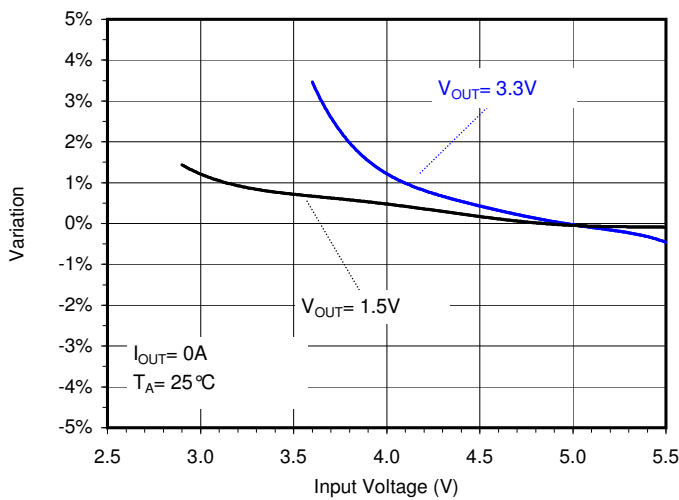
### $R_{DS(ON)}$ Variation vs. Input Voltage



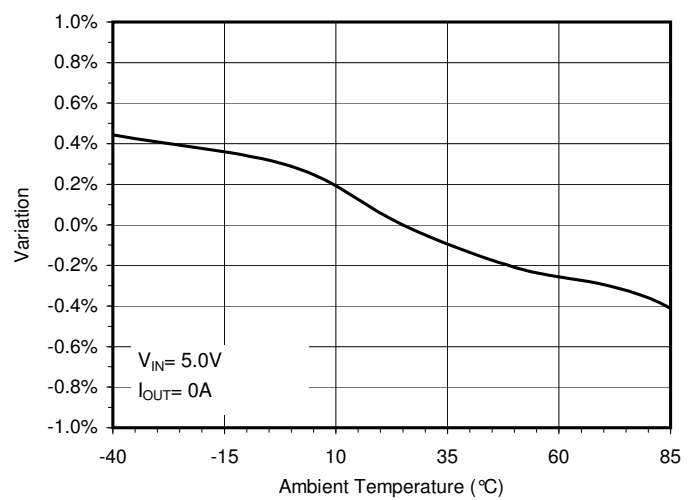
### $R_{DS(ON)}$ Variation vs. Temperature



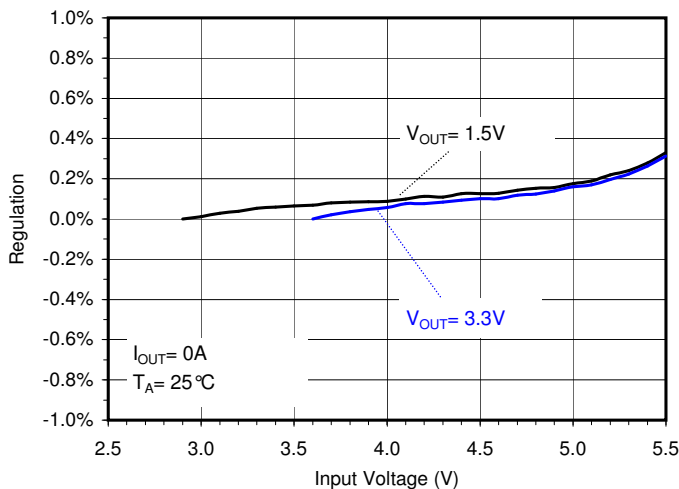
### Switching Frequency vs. Input Voltage



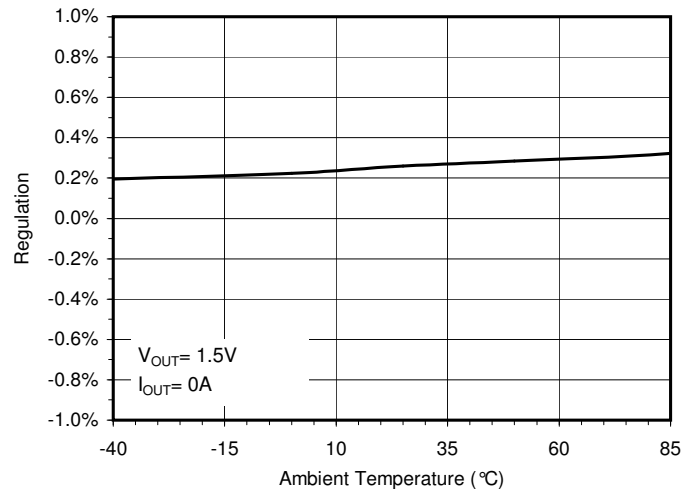
### Switching Frequency vs. Temperature



### Line Regulation



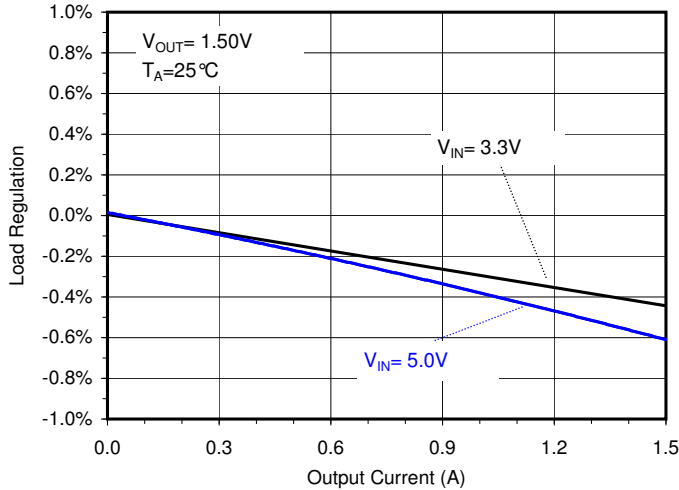
### Line Regulation vs. Temperature



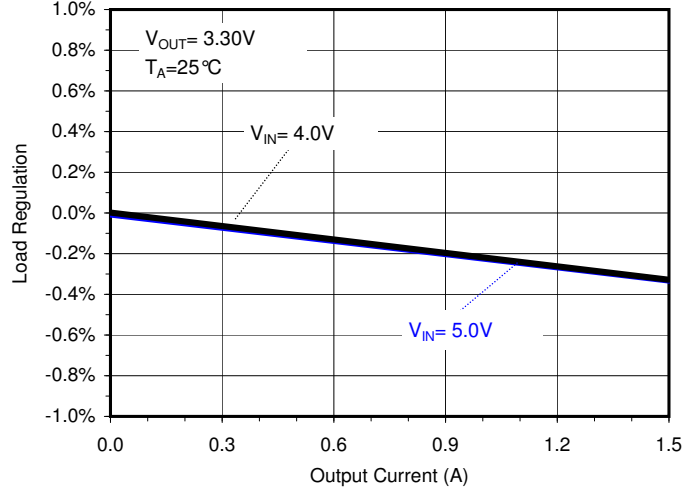
### Typical Characteristics (continued)

Circuit Conditions:  $C_{IN}=10\mu F/6.3V$ ;  $C_{OUT}=10\mu F/6.3V$  for  $L=2.2\mu H$ ;  $C_{OUT}=22\mu F/6.3V$  for  $L=1\mu H$ .  
 Unless otherwise noted,  $L=2.2\mu H$  (TOKO: 1071AS-2R2M) and SC189 in MLPD-UT6 package.

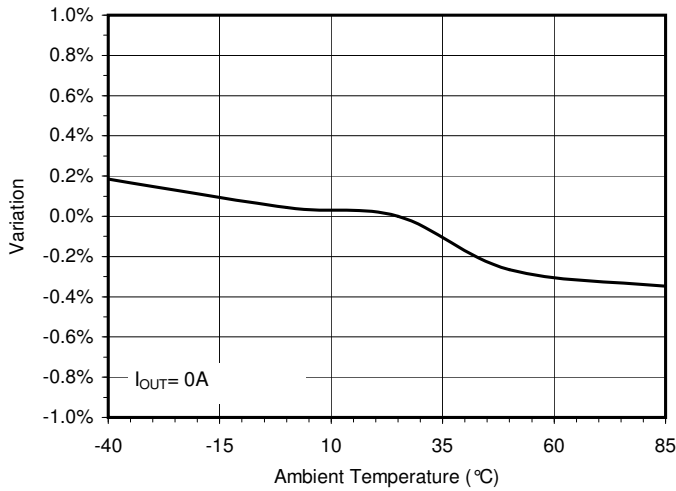
#### Load Regulation ( $V_{OUT}=1.5V$ )



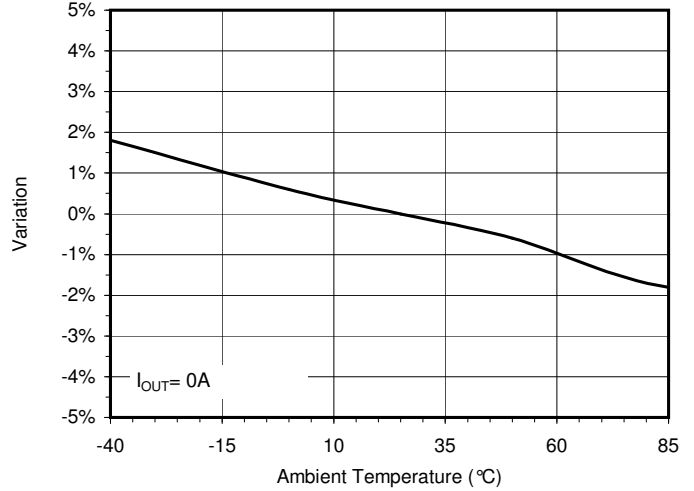
#### Load Regulation ( $V_{OUT}=3.3V$ )



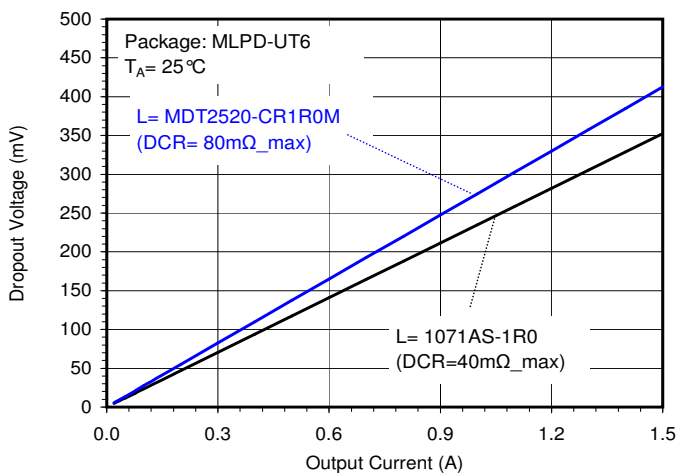
#### UVLO Rising Threshold Variation



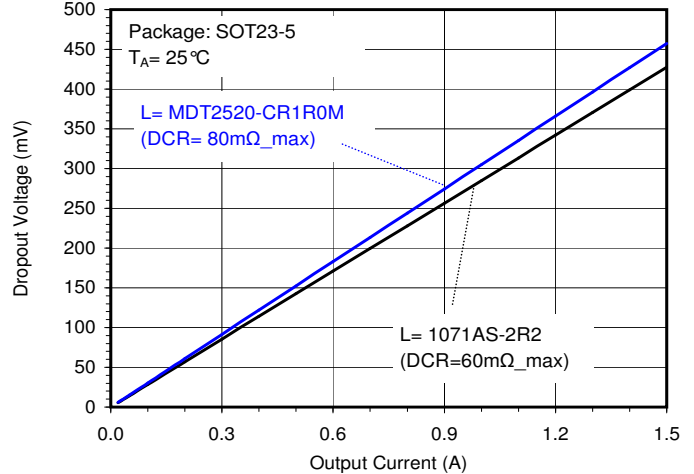
#### UVLO Hysteresis Variation



#### Dropout Voltage in 100% Duty Cycle Operation



#### Dropout Voltage in 100% Duty Cycle Operation

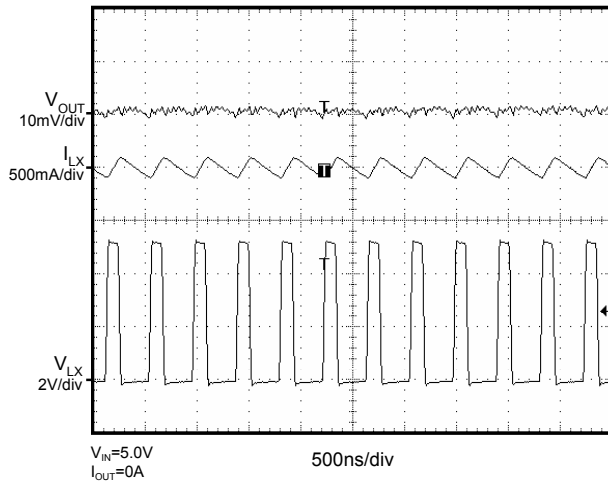




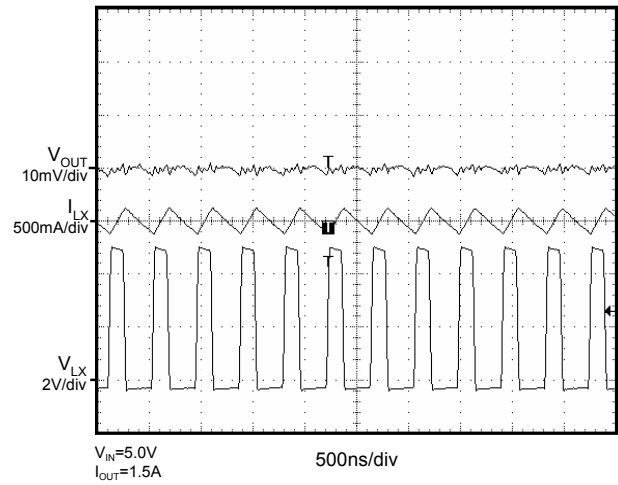
## Typical Waveforms

Circuit Conditions:  $V_{OUT}=1.5V$  (SC189HULTRT);  $L=2.2\mu H$  (TOKO: 1071AS-2R2M);  $C_{IN}=C_{OUT}=10\mu F/6.3V$  (Murata: GRM21BR60J106K).

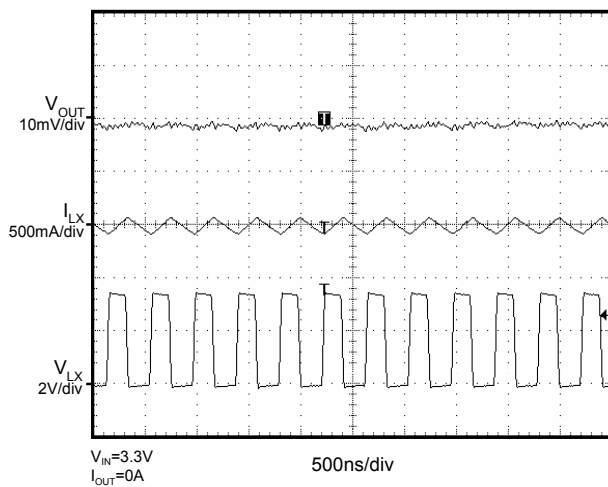
Output Voltage Ripple ( $V_{OUT}=1.5V$ )



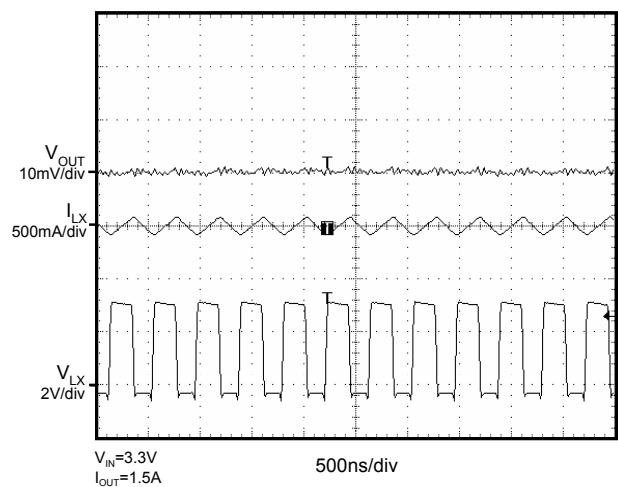
Output Voltage Ripple ( $V_{OUT}=1.5V$ )



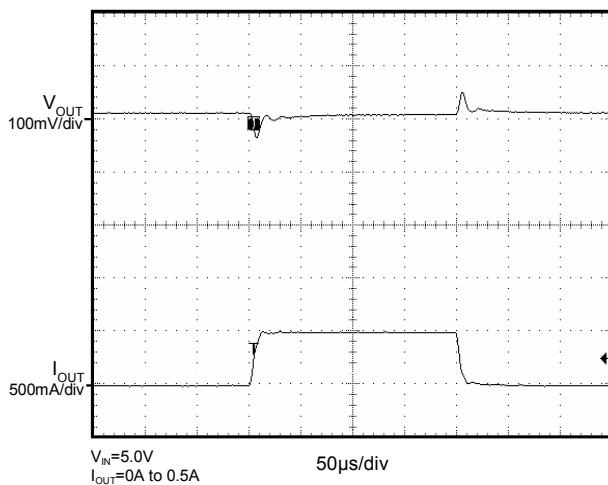
Output Voltage Ripple ( $V_{OUT}=1.5V$ )



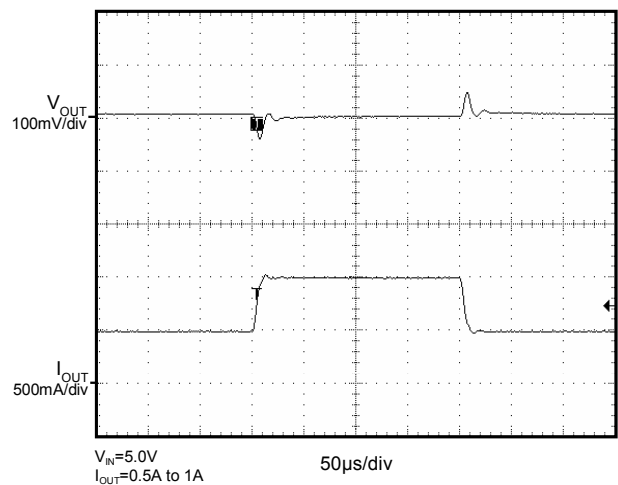
Output Voltage Ripple ( $V_{OUT}=1.5V$ )



Transient Response ( $V_{OUT}=1.5V$ ; 0A to 0.5A)



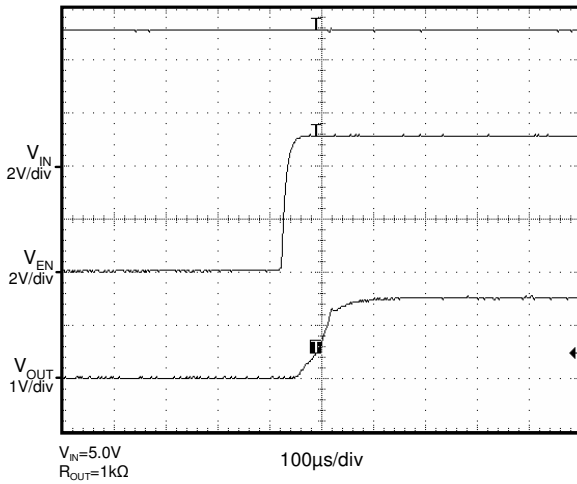
Transient Response ( $V_{OUT}=1.5V$ ; 0.5A to 1.0A)



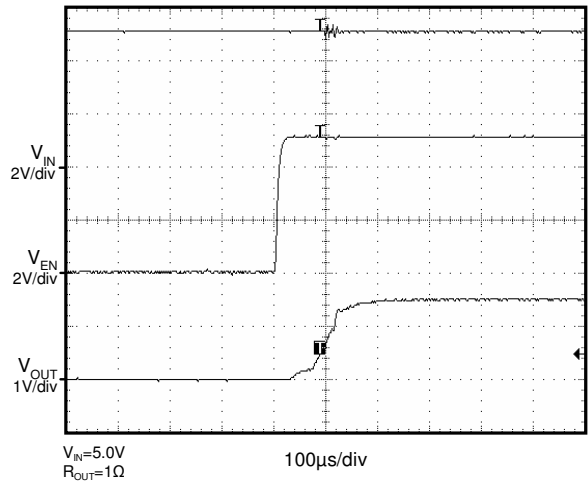
## Typical Waveforms (continued)

Circuit Conditions:  $V_{OUT}=1.5V$  (SC189HULTRT);  $L=2.2\mu H$  (TOKO: 1071AS-2R2);  $C_{IN}=C_{OUT}=10\mu F/6.3V$  (Murata: GRM21BR60J106K).

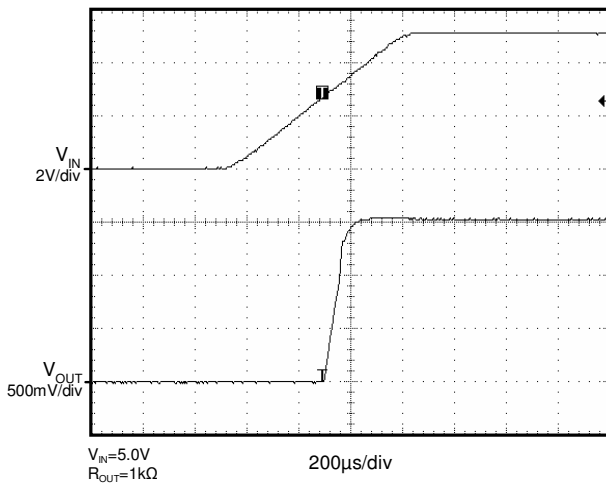
Start Up (Enable) ( $V_{OUT}=1.5V$ )



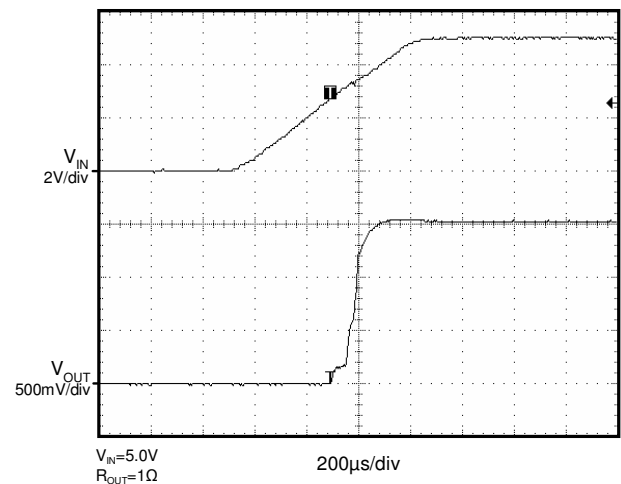
Start Up (Enable) ( $V_{OUT}=1.5V$ )



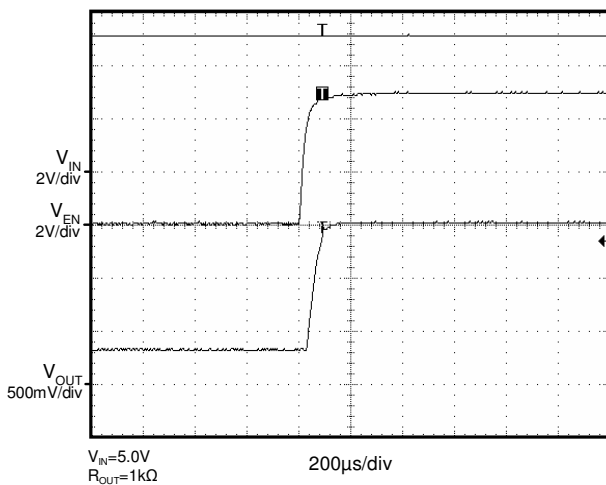
Start Up (Power up  $V_{IN}$ ) ( $V_{OUT}=1.5V$ )



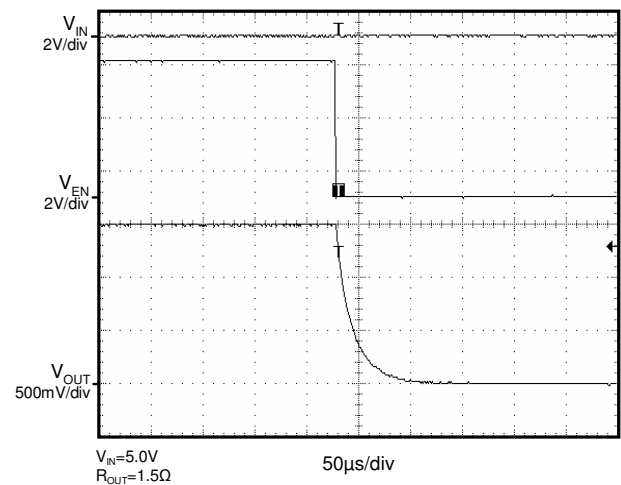
Start Up (Power up  $V_{IN}$ ) ( $V_{OUT}=1.5V$ )



Start Up into Pre-Bias Output (Enable)



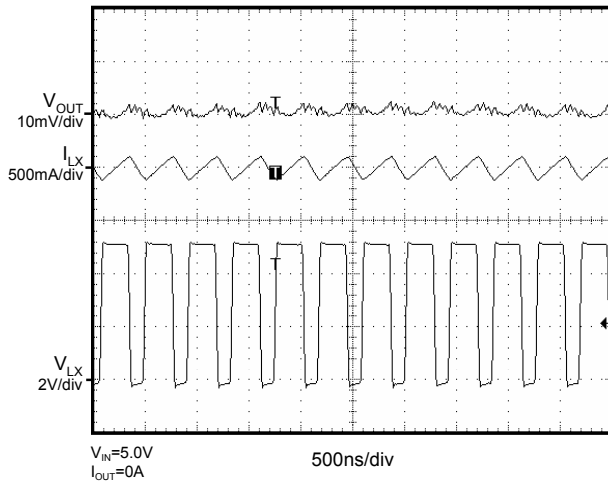
Shutdown (Disable) ( $V_{OUT}=1.5V$ )



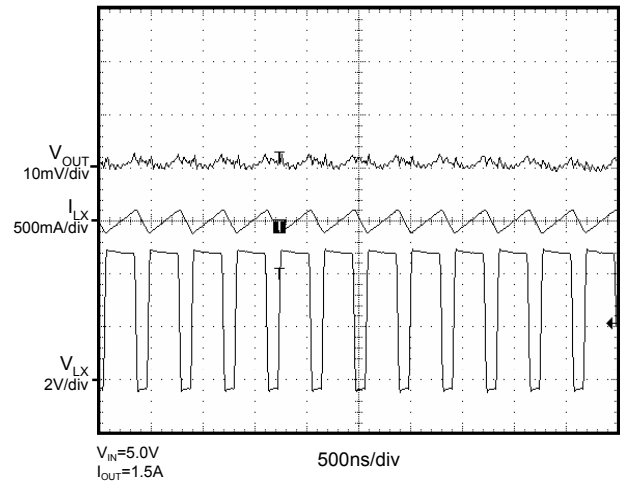
## Typical Waveforms (continued)

Circuit Conditions:  $V_{OUT}=3.3V$  (SC189ZULTRT);  $L=2.2\mu H$  (TOKO: 1071AS-2R2);  $C_{IN}=C_{OUT}=10\mu F/6.3V$  (Murata: GRM21BR60J106K).

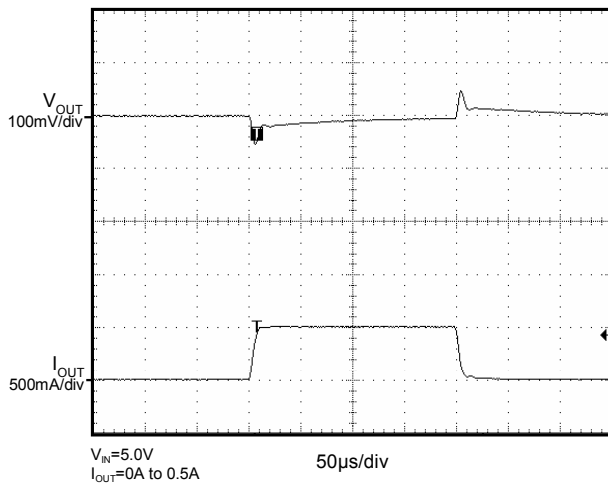
Output Voltage Ripple ( $V_{OUT}=3.3V$ )



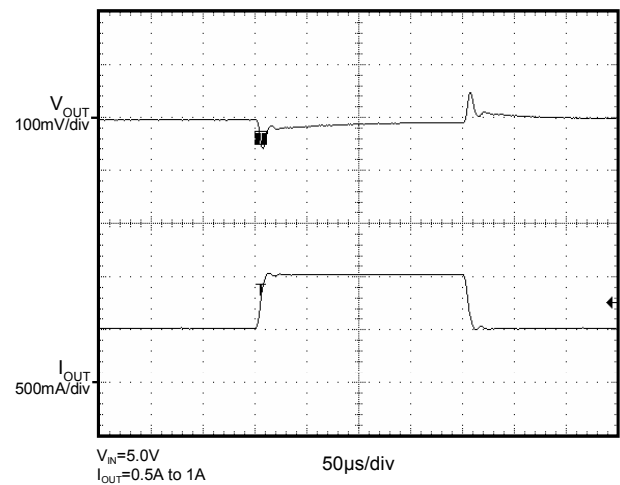
Output Voltage Ripple ( $V_{OUT}=3.3V$ )



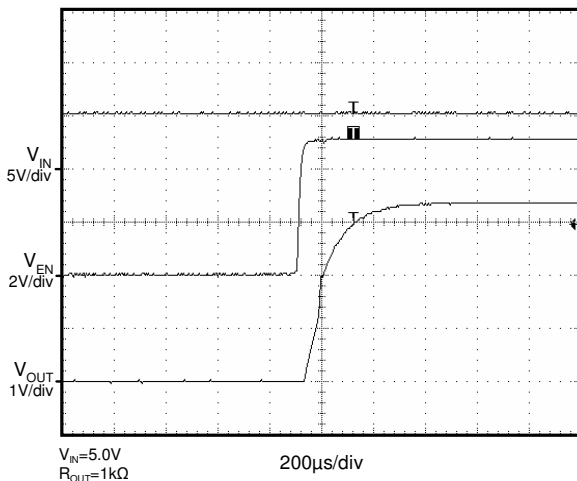
Transient Response ( $V_{OUT}=3.3V$ ; 0A to 0.5A)



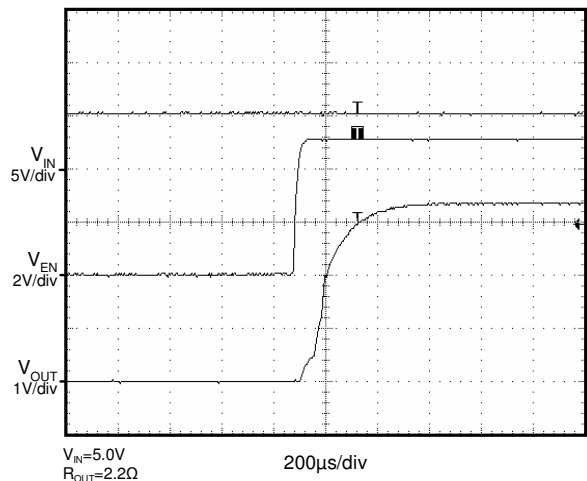
Transient Response ( $V_{OUT}=3.3V$ ; 0.5A to 1.0A)



Start Up (Enable) ( $V_{OUT}=3.3V$ )

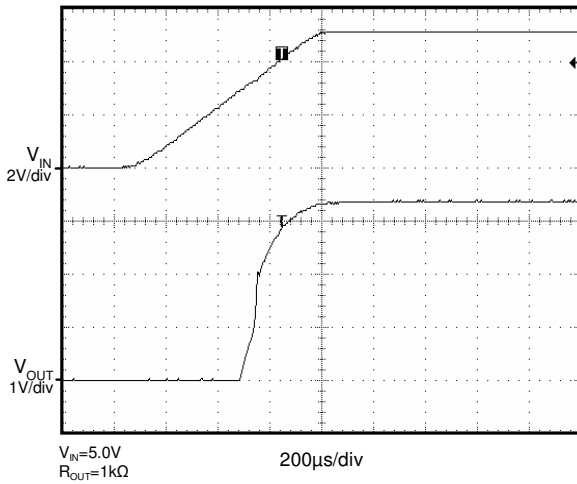
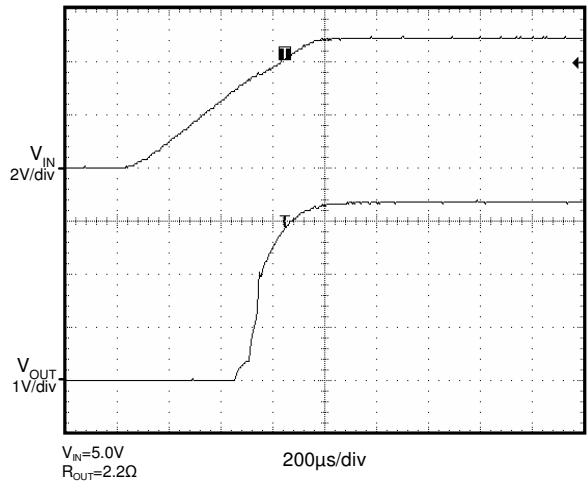
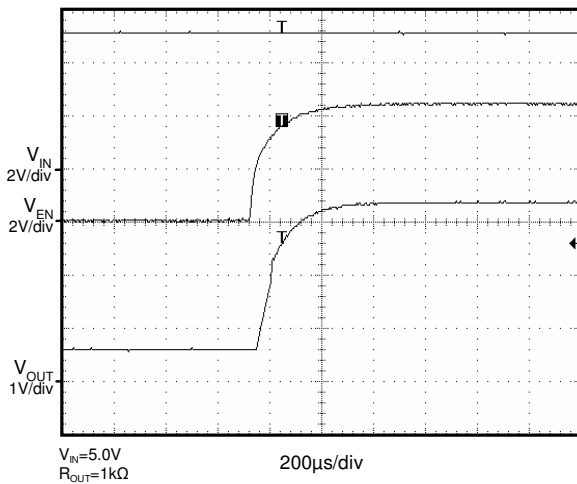
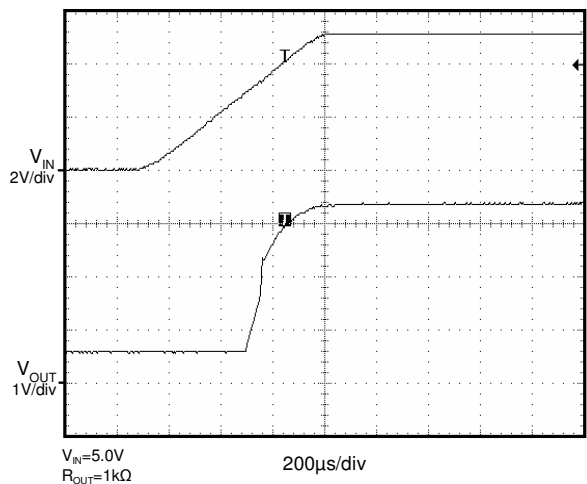
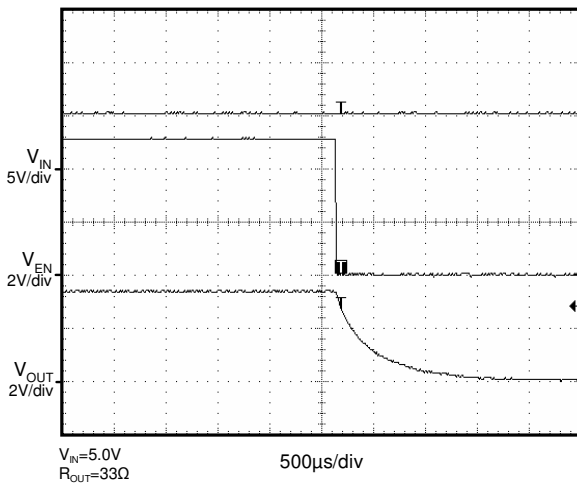
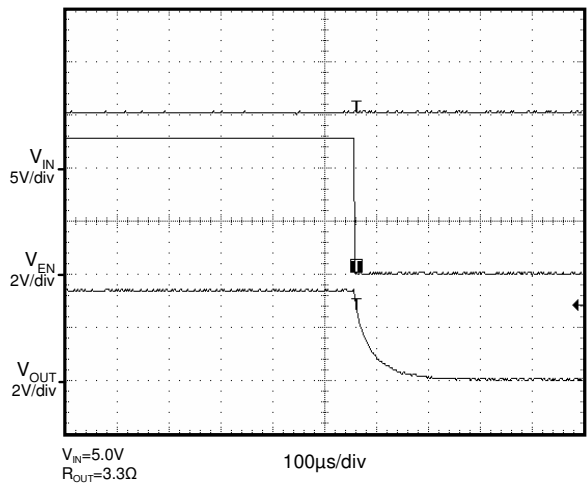


Start Up (Enable) ( $V_{OUT}=3.3V$ )



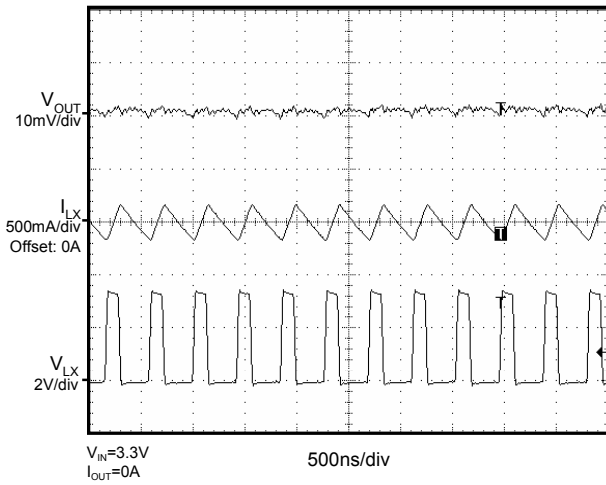
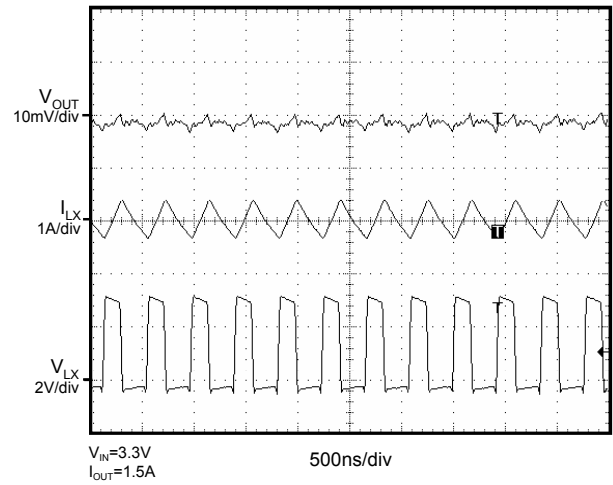
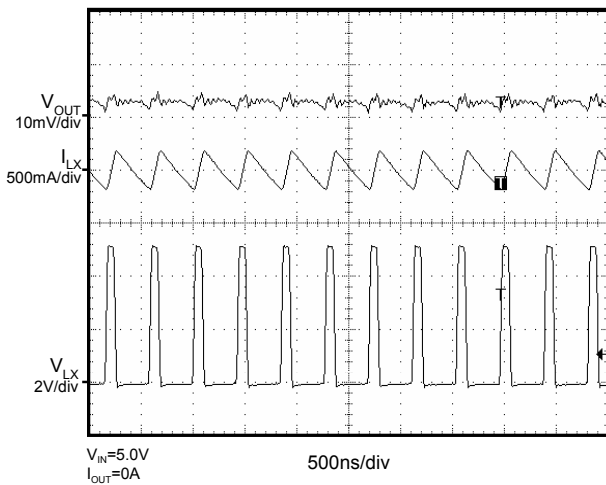
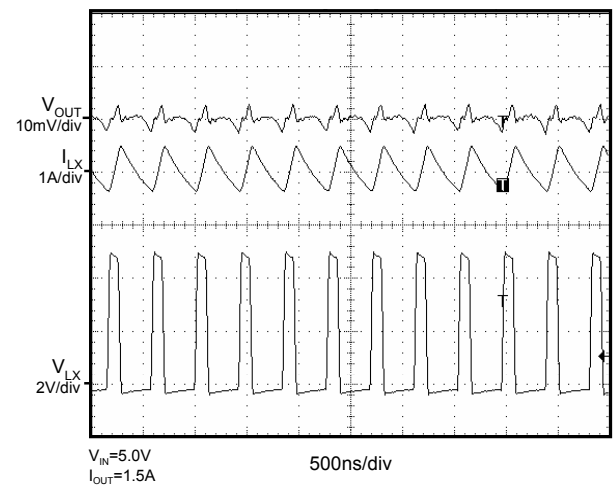
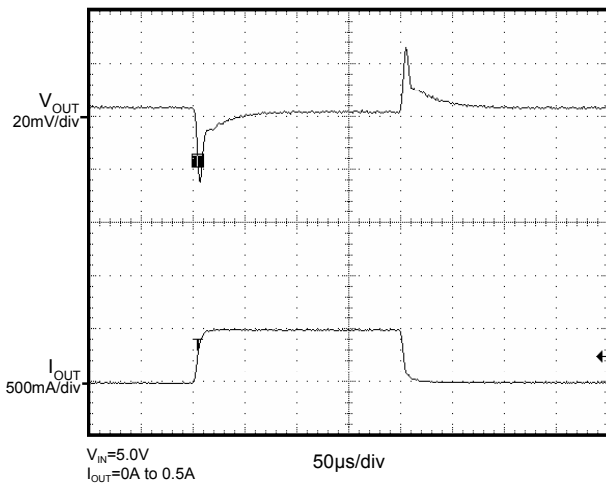
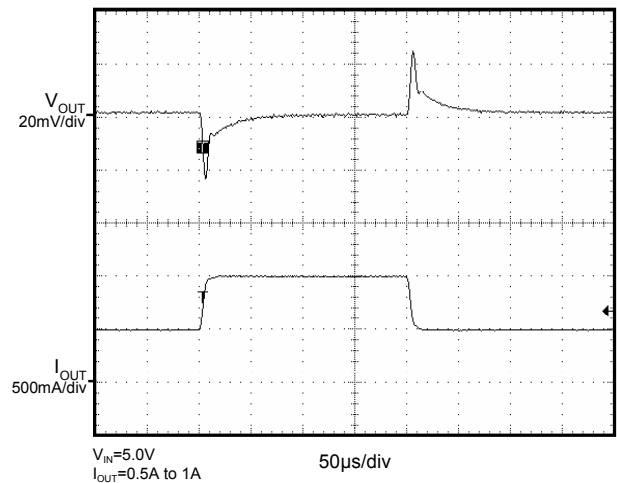
**Typical Waveforms (continued)**

 Circuit Conditions:  $V_{OUT}=3.3V$  (SC189ZULTRT);  $L=2.2\mu H$  (TOKO: 1071AS-2R2);  $C_{IN}=C_{OUT}=10\mu F/6.3V$  (Murata: GRM21BR60J106K).

**Start Up (Power up  $V_{IN}$ ) ( $V_{OUT}=3.3V$ )**

**Start Up (Power up  $V_{IN}$ ) ( $V_{OUT}=3.3V$ )**

**Start Up into Pre-Bias Output (Enable)**

**Start Up into Pre-Bias Output (Power Up  $V_{IN}$ )**

**Shutdown (Disable) ( $V_{OUT}=3.3V$ )**

**Shutdown (Disable) ( $V_{OUT}=3.3V$ )**


**Typical Waveforms (continued)**

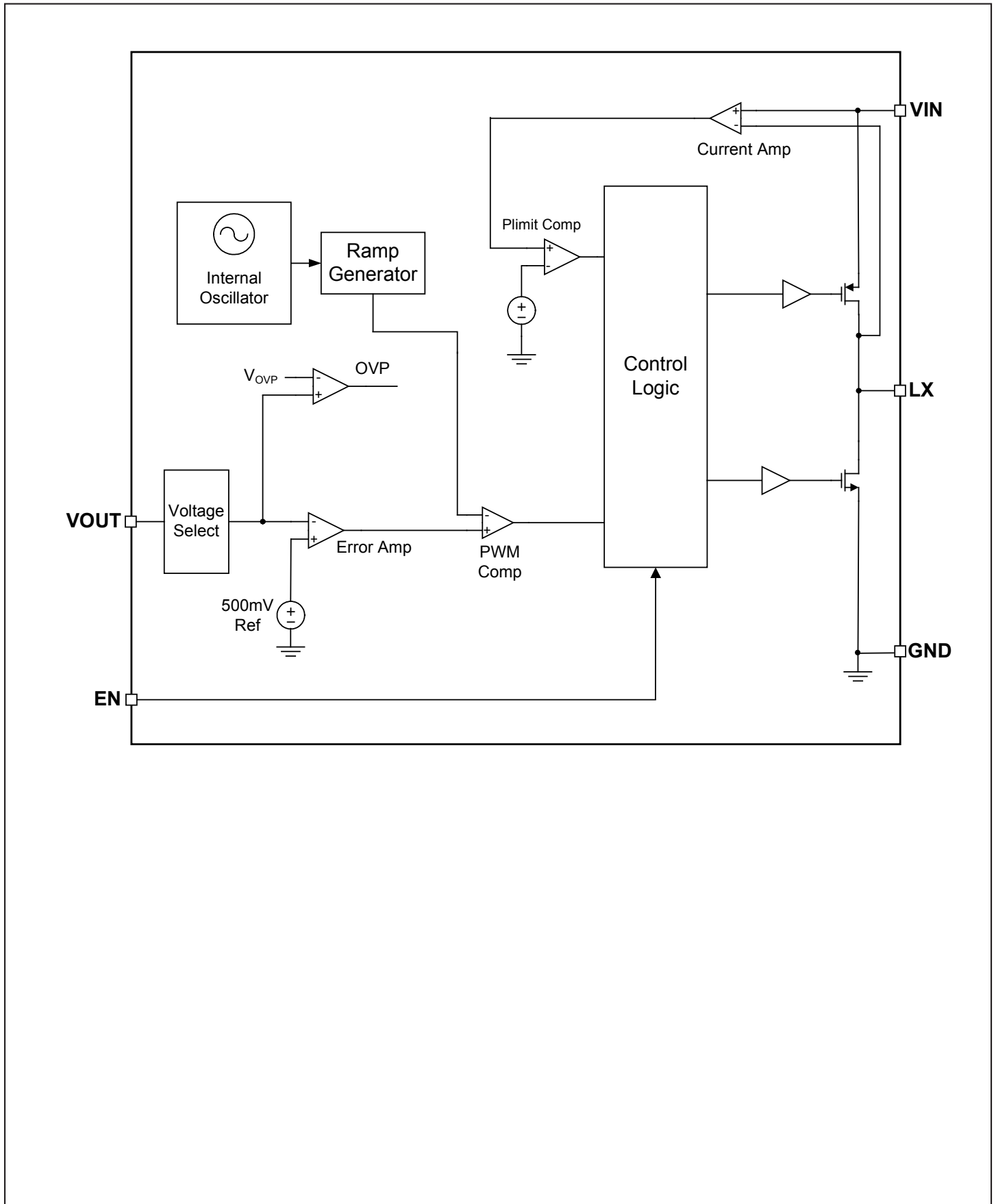
 Circuit Conditions:  $V_{OUT}=1.0V$  (SC189AULTRT);  $L=1\mu H$  (Murata: LQM2HPN1R0NG0L);  $C_{IN}=10\mu F/6.3V$ ;  $C_{OUT}=22\mu F/6.3V$  (Murata: GRM21BR60J226M).

**Output Voltage Ripple ( $V_{OUT}=1.0V$ )**

**Output Voltage Ripple ( $V_{OUT}=1.0V$ )**

**Output Voltage Ripple ( $V_{OUT}=1.0V$ )**

**Output Voltage Ripple ( $V_{OUT}=1.0V$ )**

**Transient Response ( $V_{OUT}=1.0V$ )**

**Transient Response ( $V_{OUT}=1.0V$ )**


## Pin Descriptions

Pin # (MPLD-UT6)	Pin # (SOT23-5)	Pin Name	Pin Function
1	Not Available	NC	No connection.
2	3	EN	Enable pin. When connected to logic high or tied to VIN pin, the SC189 is on. When connected to logic low, the device enters shutdown and consumes less than 1 $\mu$ A of current. The enable pin has a 1 M $\Omega$ internal pulldown resistor. This resistor is switched in circuit whenever the EN pin is below the enable input high threshold, or when the part is in undervoltage lockout.
3	1	VIN	Input power supplies. Powers the internal circuitry and is connected to the source of high-side P channel MOSFET.
4	5	LX	Switching node - connect an inductor between this pin and the output capacitor.
5	2	GND	Ground connection.
6	4	VOUT	Output voltage sense pin.
T	Not Available	Thermal Pad	Thermal pad for heatsinking purposes. This pad is not connected internally. Connect it to GND plane.

**Block Diagram**



## Applications Information

### Detailed Description

The SC189 is a synchronous step-down pulse width modulated (PWM) voltage mode DC-DC regulator operating at 2.5MHz fixed-frequency. The switching frequency is chosen to minimize the size of the external inductor and capacitors while maintaining high efficiency.

### Operation

During normal operation, the internal high-side PMOS device is activated on each rising edge of the internal oscillator. The voltage feedback loop uses an internal feedback resistor divider. The period is set by the on board oscillator when in PWM mode at average to high loads. The device has an internal low-side synchronous NMOS device and does not require a Schottky diode on the LX pin. The device operates as a buck converter in PWM mode with a fixed frequency of 2.5MHz.

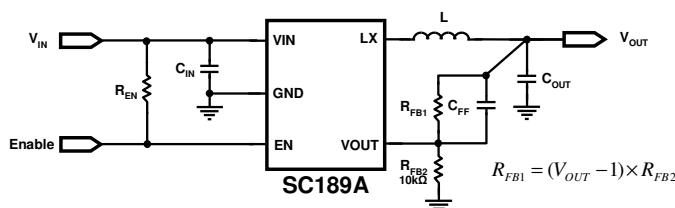
### Output Voltage Selection

The SC189 is designed for fixed output voltage. There are some options for preset output voltage shown in Table 1. If the voltage desired is not shown in the Table 1, it can be programmed via an external resistor divider. There will be typical 1uA current flowing into the VOUT pin. The typical schematic of adjustable output voltage option from the part with standard 1.0V, the SC189A, is shown in Figure 1. The  $C_{FF}$  is needed for maintain the performance of the transient response. The proper value of  $C_{FF}$  can be calculated by the equation

$$C_{FF} [nF] = 10 \times \frac{(V_{OUT} - 0.5)^2}{R_{FB1} [k\Omega] \cdot (V_{OUT} - V_{OSTD})} \times \left( \frac{V_{OSTD}}{V_{OSTD} - 0.5} \right)$$

,where the  $V_{OSTD}$  is the standard voltage shown in Table 1.

To simplify the design, it is recommended to program the desired output voltage from standard 1.0V as shown in Figure 1 with a proper  $C_{FF}$  calculated from the equation



**Figure 1 — Typical schematic for adjustable output voltage option from standard 1.0V of SC189A**

shown above. For programming the output voltage from other standard voltage, the  $R_{FB1}$ ,  $R_{FB2}$  and  $C_{FF}$  need to be adjusted to meet the equation shown above.

### Maximum Power Dissipation of SOT23-5 Package

The maximum power dissipation for junction temperature of less than 125°C on SOT23-5 package is shown in figure 2. The curve is drawn based on the  $\Theta_{JA}$  of 90°C/W which is measured in free convection, mounted on 10mm x 10mm, 2 layer FR4 PCB shown in figure 8 with copper of 1oz for each layer. The maximum power dissipation may limit the maximum output current over temperature. The figure 3 and figure 4 show the typical maximum output current for  $T_j \leq 125^\circ\text{C}$  over temperature of  $V_{IN}=5.0\text{V}$  and  $V_{IN}=3.3\text{V}$ , respectively. If using inductor with higher loss (i.e., chip inductor), due to the higher board temperature, the  $\Theta_{JA}$  will be a little bit higher.

### Protection Features

The SC189 provides the following protection features:

- Thermal Shutdown
- Current Limit
- Over-Voltage Protection
- Soft-Start Operation

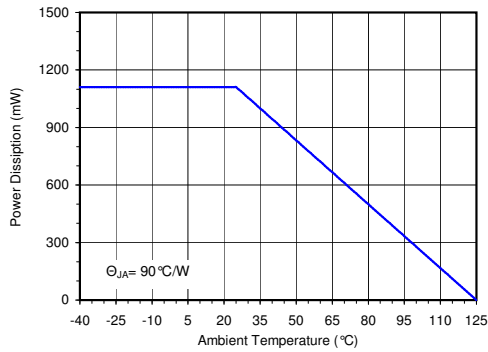
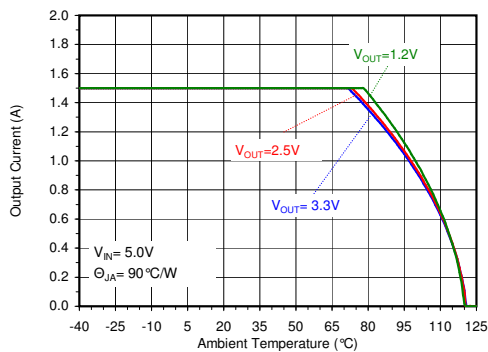
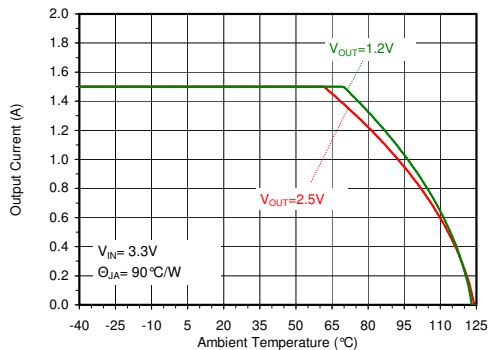
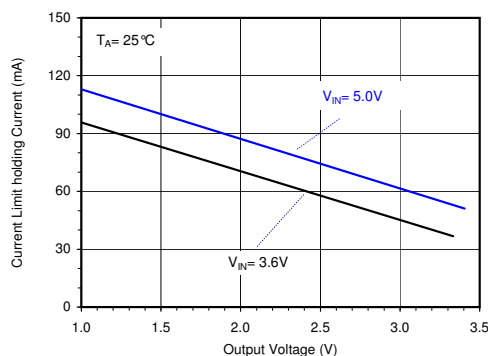
### Thermal Shutdown

The device has a thermal shutdown feature to protect the SC189 if the junction temperature exceeds 160°C. During thermal shutdown, the on-chip power devices are disabled with the LX output floating. When the die temperature drops by 10°C, the part will initiate a soft start recovery to normal operation.

### Current Limit

The internal PMOS power device in the switching stage is protected by current limit feature. If the output is loaded above the PMOS current limit for 32 consecutive cycles, the SC189 enters foldback current limit mode and the output current is limited to the current limit holding current ( $I_{CL\_HOLD}$ ) of a few hundred milliamperes. Under these conditions the output voltage will be the product of  $I_{CL\_HOLD}$  and the load resistance. The current limit holding current ( $I_{CL\_HOLD}$ ) will be decreased when output voltage is increased. The load presented must fall below



**Applications Information (continued)**

**Figure 2 — Maximum power dissipation of SOT23-5 package over temperature**

**Figure 3 — Typical maximum output current over temperature of SOT23-5 package,  $V_{IN} = 5.0V$** 

**Figure 4 — Typical maximum output current over temperature of SOT23-5 package,  $V_{IN} = 3.3V$** 

**Figure 5 — Current limit holding current decreasing rate vs. output voltage**

the current limit holding current for the SC189 to exit foldback current limit mode. Figure 5 shows the typical current limit holding current decreasing rate over different output voltage. The SC189 is capable of sustaining an indefinite short circuit without damage and will resume normal operation when the fault is removed. The foldback current limit mode will be disabled during the soft-start.

**Over-Voltage Protection**

In the event of a 15% over-voltage on the output, the PWM drive is disabled with LX pin floating.

**Soft-Start**

The soft-start mode is activated after  $V_{IN}$  reaches its UVLO and EN signal is set high to enable the part. An over temperature shutdown event will also activate the soft start sequence. Soft-start mode controls the maximum current during startup thus limiting in-rush current. The PMOS current limit is stepped through four soft start levels of approximately 20%, 25%, 40%, & 100%. Each step is maintained for 20 $\mu$ s following internal reference start up of 20 $\mu$ s giving the total nominal startup period of 100 $\mu$ s. During startup, the chip operates in controlling the inductor current swings between 0A and current limit. If  $V_{OUT}$  reaches 90% of the target within the first 2 current levels, the chip continues in hysteretic mode till the end of the soft-start time period before switching to PWM mode. If  $V_{OUT}$  does not reach 90% by the end of the second current limit level, soft start will continue to level 3 or level 4 till the output voltage reaches 96% and will then transition into PWM mode. After the full soft start time period, the SC189 will switch into PWM mode operation regardless of the  $V_{OUT}$  level.

The SC189 is capable of starting up into a pre-biased output. When the output is precharged by another supply rail, the SC189 will not discharge the output during the soft start interval.

**Shut Down**

When the EN pin voltage goes low, the SC189 will run in shutdown mode, drawing less than 1 $\mu$ A from the input power supply. The internal switches and bandgap voltage will be immediately turned off.

**Inductor Selection**

The SC189 converter has internal loop compensation. The

**Applications Information (continued)**

Vout Code (Vout)		A(1.0V),B(1.1V),C(1.2V),E(1.28V),F(1.3V),H(1.5V)				
Inductor			Output Capacitor			
Description	Vender	Part Number	Description	Vender	Part Number	Qty.
2.2uH, 60mΩ(max) Wire Wound 2.8x3.0x1.5(mm)	TOKO	1071AS-2R2N	10uF, 6.3V X5R,0805	Murata	GRM21BR60J106K	1
1.0uH, 40mΩ(max) Wire Wound 2.8x3.0x1.5(mm)	TOKO	1071AS-1R0N	22uF, 6.3V X5R,0805	Murata	GRM21BR60J226M	1
1.0uH, 80mΩ(max) Multilayer Chip 2.5x2.0x1.0(mm)	TOKO	MDT2520-CR1R0M	22uF, 6.3V X5R,0805	Murata	GRM21BR60J226M	1
			10uF, 6.3V X5R,0805	Murata	GRM219R60J106K	1
1.0uH, 69mΩ(max) Multilayer Chip 2.5x2.0x1.0(mm)	Murata	LQM2HPN1R0MG0	22uF, 6.3V X5R,0805	Murata	GRM21BR60J226M	1
			10uF, 4.0V X5R,0603	Murata	GRM188R60G106M	2

**Table 2a – Recommended L and output capacitors for Vout=1.0V to 1.5V**

Vout Code (Vout)		L(1.8V),N(2.0V),T(Y)(2.5V),V(2.7V),Z(3.3V)				
Inductor			Output Capacitor			
Description	Vender	Part Number	Description	Vender	Part Number	Qty.
2.2uH, 60mΩ(max) Wire Wound 2.8x3.0x1.5(mm)	TOKO	1071AS-2R2N	10uF, 6.3V X5R,0805	Murata	GRM21BR60J106K	1
1.0uH, 40mΩ(max) Wire Wound 2.8x3.0x1.5(mm)	TOKO	1071AS-1R0N	22uF, 6.3V X5R,0805	Murata	GRM21BR60J226M	1
1.0uH, 80mΩ(max) Multilayer Chip 2.5x2.0x1.0(mm)	TOKO	MDT2520-CR1R0M	22uF, 6.3V X5R,0805	Murata	GRM21BR60J226M	1
			10uF, 4.0V X5R,0603	Murata	GRM188R60G106M	2

**Table 2b – Recommended L and output capacitors for Vout=1.8V to 3.3V**

## Applications Information (continued)

compensation is designed to work with a output filter corner frequency of less than 100kHz over any operating condition, tolerance and bias effect. The corner frequency of output filter can be defined by the equation

$$f_c = \frac{1}{2\pi\sqrt{L \cdot C_{OUT}}}$$

Values outside this range may lead to instability, malfunction, or out-of-specification performance.

When choosing an inductor, it is important to consider the change in inductance with DC bias current. The inductor saturation current is specified as the current at which the inductance drops a specific percentage from the nominal value. This is approximately 30%. Except for short-circuit or other fault conditions, the peak current must always be less than the saturation current specified by the manufacturer. The peak current is the maximum load current plus one half of the inductor ripple current at the maximum input voltage. Load and/or line transients can cause the peak current to exceed his level for short durations. Maintaining the peak current below the inductor saturation specification keeps the inductor ripple current and the output voltage ripple at acceptable levels. Manufacturers often provide graphs of actual inductance and saturation characteristics versus applied inductor current. The saturation characteristics of the inductor can vary significantly with core temperature. Core and ambient temperatures should be considered when examining the core saturation characteristics.

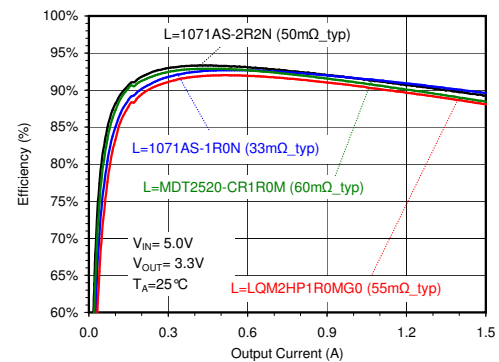
When the inductance has been determined, the DC resistance (DCR) must be examined. The efficiency that can be achieved is dependent on the DCR of the inductor. The lower values give higher efficiency. The RMS DC current rating of the inductor is associated with losses in the copper windings and the resulting temperature rise of the inductor. This is usually specified as the current which produces a 40°C temperature rise. Most copper windings are rated to accommodate this temperature rise above maximum ambient.

Magnetic fields associated with the output inductor can interfere with nearby circuitry. This can be minimized by the use of low noise shielded inductors which use the

minimum gap possible to limit the distance that magnetic fields can radiate from the inductor. However shielded inductors typically have a higher DCR and are thus less efficient than a similar sized non-shielded inductor.

The SC189 is compatible with small shielded chip inductors for low cost, low profile applications. The inductance roll off characteristic of chip inductor is worse resulting in high ripple current and increased output voltage ripple at heavy load operation. SC189 has OCP peak inductor current threshold of 2.0A minimum, to support 1.5A DC load current, the inductor ripple current at 1.5A DC load current needs to be less than 1A.

Final inductor selection depends on various design considerations such as efficiency, EMI, size, and cost. Table 2a and 2b list the manufacturers of recommended inductor and output capacitors. Chip inductors provide smaller footprint and height with lower efficiency and increased output voltage ripple. Transient load performance is equivalent to wire wound inductors. Figure 6 shows the typical efficiency curves for different inductors.



**Figure 6 — Typical efficiency curves**  
( $V_{IN}=5.0V$ ,  $V_{OUT}=3.3V$ )

### $C_{OUT}$ Selection

The internal voltage loop compensation in the SC189 limits the minimum output capacitor value to 10μF if using the inductor of 2.2μH. This is due to its influence on the the loop crossover frequency, phase margin, and gain margin. Increasing the output capacitor above this minimum value will reduce the crossover frequency and provide greater phase margin. A total output capacitance should not exceed 30uF to avoid any start-up problems. For most typical applications, it is recommended to use output capacitance of 10uF to 22uF. When choosing output

## Applications Information (continued)

capacitor's capacitance, verify the voltage derating effect from the capacitor vendors data sheet.

Capacitors with X7R or X5R ceramic dielectric are recommended for their low ESR and superior temperature and voltage characteristics. Y5V capacitors should not be used as their temperature coefficients make them unsuitable for this application.

The output voltage droop due to a load transient is determined by the capacitance of the ceramic output capacitor. The ceramic capacitor supplies the load current initially until the loop responds. Within a few switching cycles the loop will respond and the inductor current will increase to match the required load. The output voltage droop during the period prior to the loop responding can be related to the choice of output capacitor by the relationship.

$$C_{OUT} = \frac{3 \cdot \Delta I_{LOAD}}{V_{DROOP} \cdot f_{OSC}}$$

The output capacitor RMS current ripple may be calculated from the equation

$$I_{COUT(RMS)} = \frac{1}{2\sqrt{3}} \left( \frac{V_{OUT} \cdot (V_{IN(MAX)} - V_{OUT})}{L \cdot f_{OSC} \cdot V_{IN}} \right)$$

Table 3 lists the manufacturers of recommended output capacitor options.

### C<sub>IN</sub> Selection

The SC189 source input current is a DC supply current with a triangular ripple imposed on it. To prevent large input voltage ripple, a low ESR ceramic capacitor is required. A minimum value of 4.7µF should be used. It is important to consider the DC voltage coefficient characteristics when determining the actual required value. To estimate the required input capacitor, determine the acceptable input ripple voltage and calculate the minimum value required for C<sub>IN</sub> from the equation

$$C_{IN} = \frac{\frac{V_{OUT}}{V_{IN}} \left( 1 - \frac{V_{OUT}}{V_{IN}} \right)}{\left( \frac{\Delta V}{I_{OUT}} - ESR \right) \cdot f_{OSC}}$$

The input capacitor RMS ripple current varies with the input and output voltage. The maximum input capacitor RMS current is found from the equation

$$I_{CIN(RMS)} = \sqrt{\frac{V_{OUT}}{V_{IN}} \left( 1 - \frac{V_{OUT}}{V_{IN}} \right)}$$

The input voltage ripple and RMS current ripple are at maximum when the input voltage is twice the output voltage or 50% duty cycle.

The input capacitor provides a low impedance loop for the edges of pulsed current drawn by the PMOS switch. Low ESR/ESL X5R ceramic capacitors are recommended for this function. To minimise stray inductance, the capacitor should be placed as closely as possible to the VIN and GND pins of the SC189.

Manufacturer Part Number	Value (µF)	Type	Rated Voltage (VDC)	Value at 3.3V (µF)	Dimensions LxWxH (mm)
Murata GRM21BR61A106K	10±10%	X5R	10	4.42	2.0x1.25x1.25 (EIA:0805)
Murata GRM21BR71A106K	10±10%	X7R	10	4.88	2.0x1.25x1.25 (EIA:0805)
Murata GRM21BR60J106K	10±10%	X5R	6.3	4.05	2.0x1.25x1.25 (EIA:0805)
Murata GRM21BR70J106K	10±10%	X7R	6.3	4.91	2.0x1.25x1.25 (EIA:0805)
Murata GRM21BR60J226M	22±20%	X5R	6.3	6.57	2.0x1.25x1.25 (EIA:0805)

**Table 3 – Recommended Capacitors**

## Applications Information (continued)

### PCB Layout Considerations

The layout diagram in figure 7 and figure 8 shows a recommended PCB for MLPD-UT6 2x2 and SOT23-5 package, respectively. Fundamental layout rules must be followed since the layout is critical for achieving the performance specified in the Electrical Characteristics table. Poor layout can degrade the performance of the DC-DC converter and can contribute to EMI problems, ground bounce, and resistive voltage losses. Poor regulation and instability can result.

The following guidelines are recommended when developing a PCB layout:

1. The input capacitor,  $C_{IN}$  should be placed as close to the VIN and GND pins as possible. This capacitor provides a low impedance loop for the pulsed currents present at the buck converter's input. Use short wide traces to connect as closely to the IC as possible. This will minimize EMI and input voltage ripple by localizing the high frequency current pulses.
2. Keep the LX pin traces as short as possible to minimize pickup of high frequency switching edges to other parts of the circuit.  $C_{OUT}$  and L should be connected as close as possible between the LX and GND pins, with a direct return to the GND pin from  $C_{OUT}$ .
3. Route the output voltage feedback/sense path away from inductor and LX node to minimize noise and magnetic interference.
4. Use a ground plane referenced to the SC189 GND pin. Use several vias to connect to the component side ground to further reduce noise and interference on sensitive circuit nodes.
5. If possible, minimize the resistance from the VOUT and GND pins to the load. This will reduce the voltage drop on the ground plane and improve the load regulation. And it will also improve the overall efficiency by reducing the copper losses on the output and ground planes.

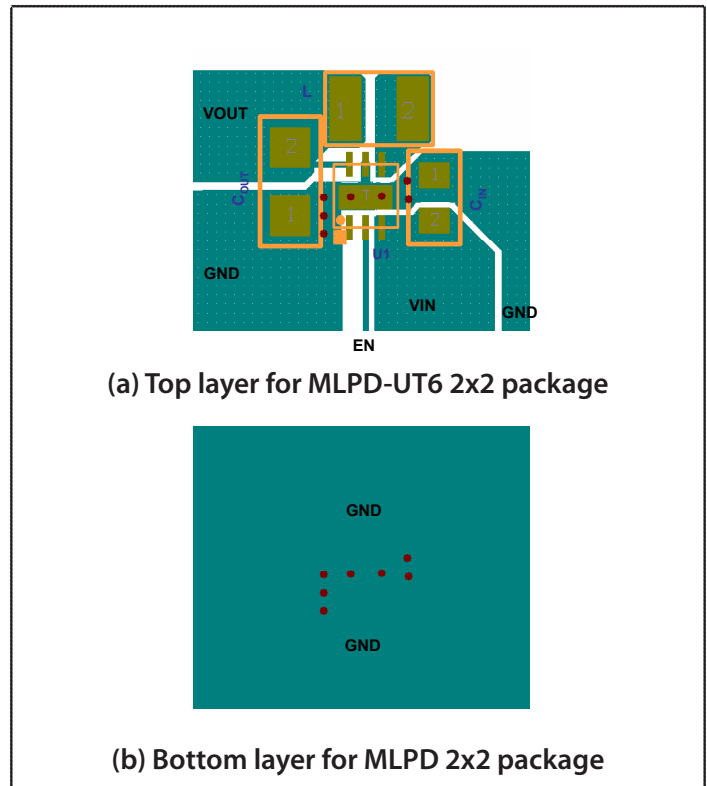


Figure 7 — Recommended PCB Top & Bottom Layer Layout for MLPD-UT6 2x2 Package

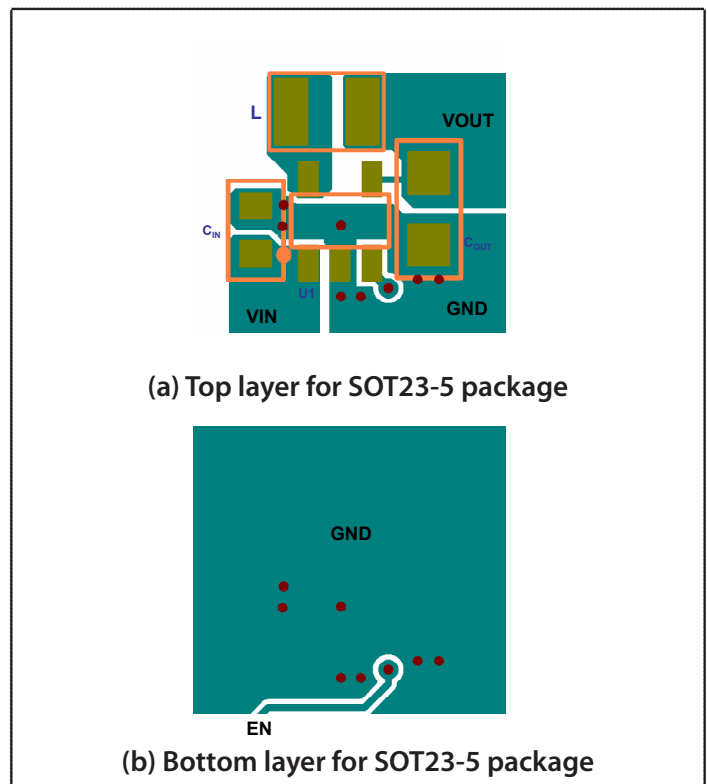
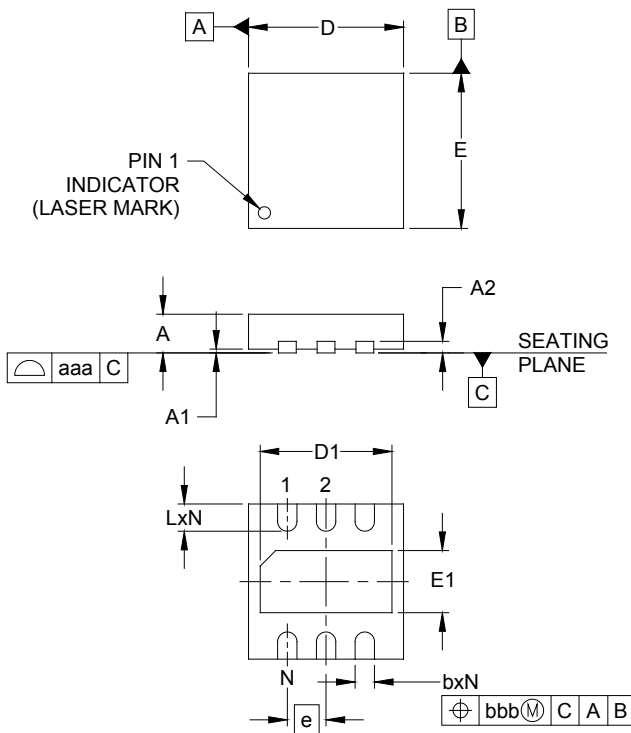


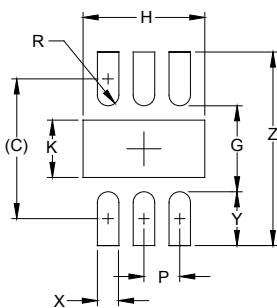
Figure 8 — Recommended PCB Top & Bottom Layer Layout for SOT23-5 Package

**Outline Drawing – 2x2 MLPD-UT6**


DIM	INCHES			MILLIMETERS		
	MIN	NOM	MAX	MIN	NOM	MAX
A	.018	-	.024	0.45	-	0.60
A1	.000	-	.002	0.00	-	0.05
A2	(.006)			(0.1524)		
b	.007	.010	.012	0.18	0.25	0.30
D	.075	.079	.083	1.90	2.00	2.10
D1	.061	.067	.071	1.55	1.70	1.80
E	.075	.079	.083	1.90	2.00	2.10
E1	.026	.031	.035	0.65	0.80	0.90
e	.020 BSC			0.50 BSC		
L	.010	.014	.018	0.25	0.35	0.45
N	6			6		
aaa	.003			0.08		
bbb	.004			0.10		

**NOTES:**

1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).
2. COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS TERMINALS.

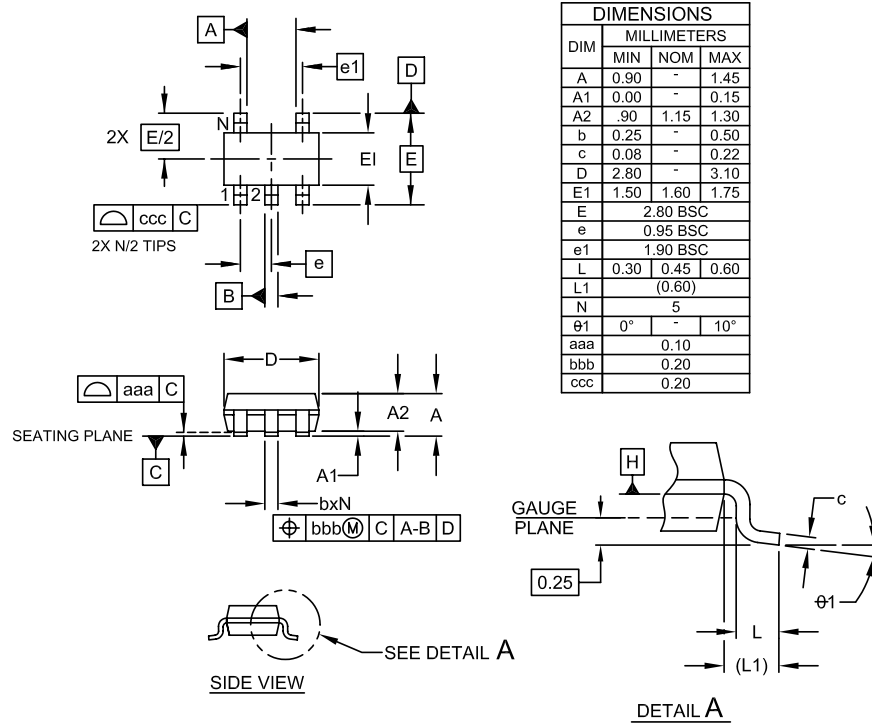
**Land Pattern – 2x2 MLPD-UT6**


DIM	INCHES	MILLIMETERS
C	(.077)	(1.95)
G	.047	1.20
H	.067	1.70
K	.031	0.80
P	.020	0.50
R	.006	0.15
X	.012	0.30
Y	.030	0.75
Z	.106	2.70

**NOTES:**

1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).
2. THIS LAND PATTERN IS FOR REFERENCE PURPOSES ONLY. CONSULT YOUR MANUFACTURING GROUP TO ENSURE YOUR COMPANY'S MANUFACTURING GUIDELINES ARE MET.
3. THERMAL VIAS IN THE LAND PATTERN OF THE EXPOSED PAD SHALL BE CONNECTED TO A SYSTEM GROUND PLANE. FAILURE TO DO SO MAY COMPROMISE THE THERMAL AND/OR FUNCTIONAL PERFORMANCE OF THE DEVICE.

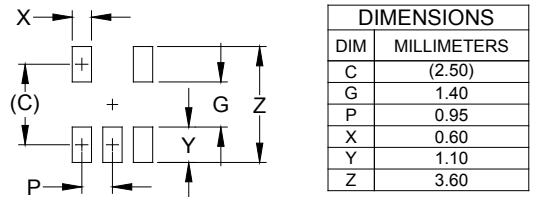
Outline Drawing – SOT23-5



DIMENSIONS			
DIM	MILLIMETERS		
	MIN	NOM	MAX
A	0.90	-	1.45
A1	0.00	-	0.15
A2	.90	1.15	1.30
b	0.25	-	0.50
c	0.08	-	0.22
D	2.80	-	3.10
E1	1.50	1.60	1.75
E	2.80 BSC		
e	0.95 BSC		
e1	1.90 BSC		
L	0.30	0.45	0.60
L1	(0.60)		
N	5		
θ1	0°	-	10°
aaa	0.10		
bbb	0.20		
ccc	0.20		

- NOTES:
1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).
  2. DATUMS **-A-** AND **-B-** TO BE DETERMINED AT DATUM PLANE **-H-**
  3. DIMENSIONS "E1" AND "D" DO NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.

Land Pattern – SOT23-5



DIMENSIONS	
DIM	MILLIMETERS
C	(2.50)
G	1.40
P	0.95
X	0.60
Y	1.10
Z	3.60

- NOTES:
1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).
  2. THIS LAND PATTERN IS FOR REFERENCE PURPOSES ONLY. CONSULT YOUR MANUFACTURING GROUP TO ENSURE YOUR COMPANY'S MANUFACTURING GUIDELINES ARE MET.

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- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

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## JONHON

«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



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