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REVISION HISTORY

2/07—Rev. 0 to Rev. A

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6/05—Revision 0: Initial Version

SPECIFICATIONS

$V_{CC} = 3.0\text{ V}$ to 3.6 V . All specifications T_{MIN} to T_{MAX}^1 , unless otherwise noted. Typical values as specified at 25°C .

Table 1.

Parameter	Min	Typ	Max	Unit	Conditions/Comments
LASER BIAS CURRENT (IBIAS)					
Output Current (IBIAS)	2		100	mA	
Compliance Voltage	1.2		V_{CC}	V	
IBIAS when ALS is High			0.1	mA	
MODULATION CURRENT (IMODP, IMODN) ²					
Output Current (IMOD)	5		90	mA	
Compliance Voltage	1.5		V_{CC}	V	
IMOD when ALS is High			0.1	mA	5 mA < IMOD < 90 mA
Rise Time, Single-Ended Output ^{2,3}		60	104	ps	5 mA < IMOD < 90 mA
Fall Time, Single-Ended Output ^{2,3}		60	96	ps	5 mA < IMOD < 90 mA
Random Jitter, Single-Ended Output ^{2,3}		0.8	1.1	ps (rms)	5 mA < IMOD < 90 mA
Deterministic Jitter, Single-Ended Output ^{3,4}		19	35	ps	20 mA < IMOD < 90 mA
Pulse-Width Distortion, Single-Ended Output ^{2,3}		21	30	ps	20 mA < IMOD < 90 mA
Rise Time, Differential Output ^{3,5}		47.1		ps	5 mA < IMOD < 30 mA
Fall Time, Differential Output ^{3,5}		46		ps	5 mA < IMOD < 30 mA
Random Jitter, Differential Output ^{3,5}		0.64		ps (rms)	5 mA < IMOD < 30 mA
Deterministic Jitter, Differential Output ^{3,6}		12		ps	5 mA < IMOD < 30 mA
Pulse-Width Distortion, Differential Output ^{3,5}		2.1		ps	5 mA < IMOD < 30 mA
Rise Time, Differential Output ^{3,5}		56		ps	5 mA < IMOD < 90 mA
Fall Time, Differential Output ^{3,5}		55		ps	5 mA < IMOD < 90 mA
Random Jitter, Differential Output ^{3,5}		0.61		ps (rms)	5 mA < IMOD < 90 mA
Deterministic Jitter, Differential Output ^{3,7}		17		ps	5 mA < IMOD < 90 mA
Pulse-Width Distortion, Differential Output ^{3,5}		1.6		ps	5 mA < IMOD < 90 mA
AVERAGE POWER SET (PAVSET)					
Pin Capacitance			80	pF	
Voltage	1.1	1.2	1.3	V	
Photodiode Monitor Current (Average Current)	50		1200	μA	Resistor setpoint mode
EXTINCTION RATIO SET INPUT (ERSET)					
Resistance Range	1.5		25	k Ω	Resistor setpoint mode
Resistance Range	0.99	1	1.01	k Ω	Voltage setpoint mode
AVERAGE POWER REFERENCE VOLTAGE INPUT (PAVREF)					
Voltage Range	0.07		1	V	Voltage setpoint mode (RPAV fixed at 1 k Ω)
Photodiode Monitor Current (Average Current)	70		1000	μA	Voltage setpoint mode (RPAV fixed at 1 k Ω)
EXTINCTION RATIO REFERENCE VOLTAGE INPUT (ERREF)					
Voltage Range	0.05		0.9	V	Voltage setpoint mode (RERSET fixed at 1 k Ω)
ERREF Voltage to IMOD Gain		100		mA/V	
DATA INPUTS (DATAP, DATAN) ⁸					
V p-p (Differential)	0.4		2.4	V	AC-coupled
Input Impedance (Single-Ended)		50		Ω	
LOGIC INPUTS (ALS)					
V_{IH}	2			V	
V_{IL}			0.8	V	

ADN2871

Parameter	Min	Typ	Max	Unit	Conditions/Comments
ALARM OUTPUT (FAIL) ⁹					
V_{OFF}		>1.8		V	Voltage required at FAIL for IBIAS and IMOD to turn off when FAIL asserted
V_{ON}		<1.3		V	Voltage required at FAIL for IBIAS and IMOD to stay on when FAIL asserted
IBMON/IMMON DIVISION RATIO					
IBIAS/IBMON ³	76	94	112	A/A	2 mA < IBIAS < 11 mA
IBIAS/IBMON ³	85	100	115	A/A	11 mA < IBIAS < 50 mA
IBIAS/IBMON ³	92	100	108	A/A	50 mA < IBIAS < 100 mA
IBIAS/IBMON Stability ^{3, 10}			±5	%	10 mA < IBIAS < 100 mA
IMOD/IMMON		42		A/A	
IBMON Compliance Voltage	0		1.3	V	
SUPPLY					
I_{CC} ¹¹		32		mA	When IBIAS = IMOD = 0
V_{CC} (with respect to GND) ¹²	3.0	3.3	3.6	V	

¹ Temperature range: -40°C to +85°C.

² Measured into a single-ended 15 Ω load (22 Ω resistor in parallel with digital scope 50 Ω input) using a 1111111100000000 pattern at 2.5 Gbps, shown in Figure 2.

³ Guaranteed by design and characterization. Not production tested.

⁴ Measured into a single-ended 15 Ω load using a K28.5 pattern at 2.5 Gbps, shown in Figure 2.

⁵ Measured into a differential 30 Ω (43 Ω differential resistor in parallel with a digital scope of 50 Ω input) load using a 1111111100000000 pattern at 4.25 Gbps, as shown in Figure 3.

⁶ Measured into a differential 30 Ω load using a K28.5 pattern at 4.25 Gbps, as shown in Figure 3.

⁷ Measured into a differential 30 Ω load using a K28.5 pattern at 2.7 Gbps, as shown in Figure 3.

⁸ When the voltage on DATAP is greater than the voltage on DATAN, the modulation current flows in the IMODP pin.

⁹ Guaranteed by design. Not production tested.

¹⁰ IBIAS/IBMON ratio stability is defined in SFF-8472 Revision 9 over temperature and supply variation.

¹¹ See the I_{CC} minimum for power calculation in the Power Consumption section.

¹² All V_{CC} pins should be shorted together.

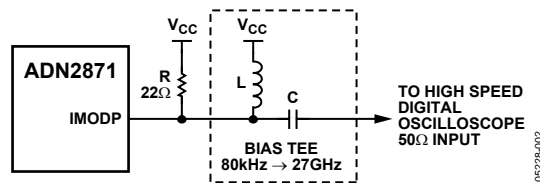


Figure 2. High Speed Electrical Test Single-Ended Output Circuit

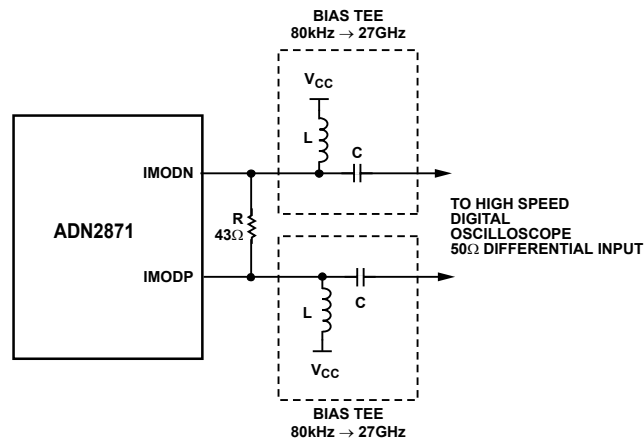


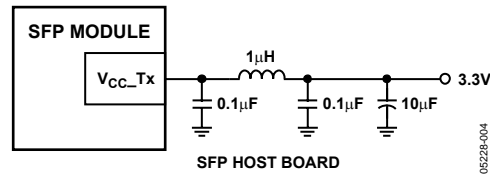
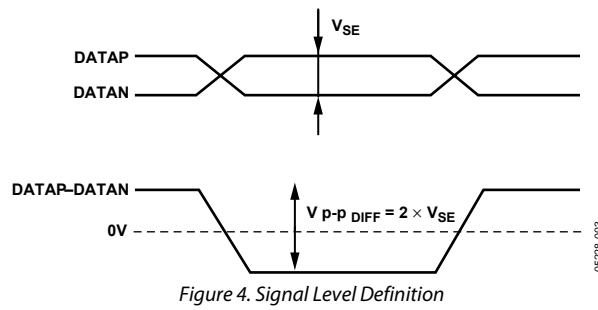
Figure 3. High Speed Electrical Test Differential Output Circuit

SFP TIMING SPECIFICATIONS

Table 2.

Parameter	Symbol	Min	Typ	Max	Unit	Conditions/Comments
ALS Assert Time	t_off	1	5		μs	Time for the rising edge of ALS (Tx_DISABLE) to when the bias current falls below 10% of nominal
ALS Negate Time ¹	t_on	0.15	0.4		ms	Time for the falling edge of ALS to when the modulation current rises above 90% of nominal
Time to Initialize, Including Reset of FAIL ¹	t_init	25	275		ms	From power-on or negation of FAIL using ALS
FAIL Assert Time	t_fault		100		μs	Time to fault to FAIL on
ALS to Reset Time	t_reset	5			μs	Time Tx_DISABLE must be held high to reset Tx_FAULT.

¹ Guaranteed by design and characterization. Not production tested.



ABSOLUTE MAXIMUM RATINGS

Table 3.

Parameter	Rating
V _{CC} to GND	4.2 V
IMODN, IMODP	–0.3 V to +4.8 V
All Other Pins	–0.3 V to +3.9 V
Junction Temperature	150°C
Operating Temperature Range	
Industrial	–40°C to +85°C
Storage Temperature Range	–65°C to +150°C
Junction Temperature (T _J max)	125°C
LFCSP	
Power Dissipation ¹	(T _J max – T _A)/θ _{JA} W
θ _{JA} Thermal Impedance ²	30°C/W
θ _{JC} Thermal Impedance	29.5°C/W
Lead Temperature (Soldering 10 sec)	300°C

¹ Power consumption equations are provided in the Power Consumption section.

² θ_{JA} is defined when part is soldered on a 4-layer board.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ESD CAUTION



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

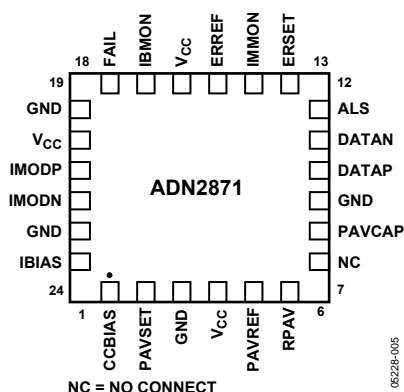


Figure 6. Pin Configuration—Top View

Note: The LFCSP has an exposed paddle that must be connected to ground.

Table 4. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	CCBIAS	In ac-coupled mode, CCBIAS can connect to either IBIAS or V_{CC} . In dc-coupled mode, CCBIAS can connect to V_{CC} .
2	PAVSET	Average Optical Power Set Pin.
3	GND	Supply Ground.
4	V_{CC}	Supply Voltage.
5	PAVREF	Reference Voltage Input for Average Optical Power Control.
6	RPAV	Average Power Resistor when Using PAVREF.
7	NC	No Connect.
8	PAVCAP	Average Power Loop Capacitor.
9	GND	Supply Ground.
10	DATAP	Data, Positive Differential Input.
11	DATAN	Data, Negative Differential Input.
12	ALS	Automatic Laser Shutdown.
13	ERSET	Extinction Ratio Set Pin.
14	IMMON	Modulation Current Monitor Current Source.
15	ERREF	Reference Voltage Input for Extinction Ratio Control.
16	V_{CC}	Supply Voltage.
17	IBMON	Bias Current Monitor Current Source.
18	FAIL	Fail Alarm Output.
19	GND	Supply Ground.
20	V_{CC}	Supply Voltage.
21	IMODP	Modulation Current Positive Output (Current Sink), Connect to Laser Diode.
22	IMODN	Modulation Current Negative Output (Current Sink).
23	GND	Supply Ground.
24	IBIAS	Laser Diode Bias (Current Sink to Ground).

OPTICAL WAVEFORMS

$V_{CC} = 3.3\text{ V}$ and $T_A = 25^\circ\text{C}$, unless otherwise noted. Note: No change to PAVCAP and ERCAP values.

MULTIRATE PERFORMANCE USING LOW COST FABRY PEROT TOSA NEC NX7315UA

(ACQ LIMIT TEST) WAVEFORMS 1000

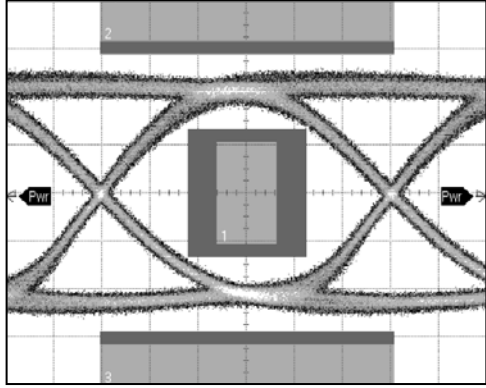


Figure 7. Optical Eye 2.488 Gbps, 65 ps/DIV, PRBS $2^{31}-1$
 $P_{AV} = -4.5\text{ dBm}$, ER = 9 dB, Mask Margin 25%

(ACQ LIMIT TEST) WAVEFORMS 1000

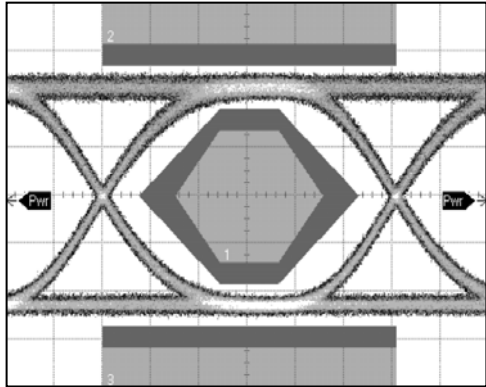


Figure 8. Optical Eye 622 Mbps, 264 ps/DIV, PRBS $2^{31}-1$
 $P_{AV} = -4.5\text{ dBm}$, ER = 9 dB, Mask Margin 50%

(ACQ LIMIT TEST) WAVEFORMS 1000

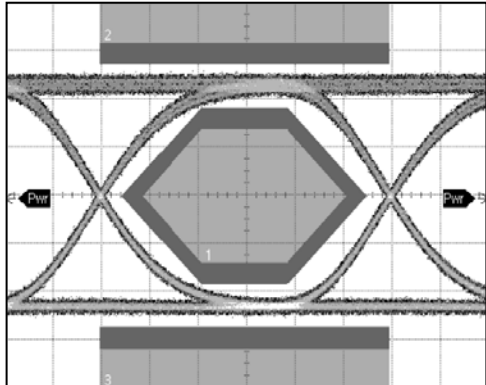


Figure 9. Optical Eye 155 Mbps, 1.078 ns/DIV, PRBS $2^{31}-1$
 $P_{AV} = -4.5\text{ dBm}$, ER = 9 dB, Mask Margin 50%

PERFORMANCE OVER TEMPERATURE USING DFB TOSA SUMITOMO SLT2486

(ACQ LIMIT TEST) WAVEFORMS 1001

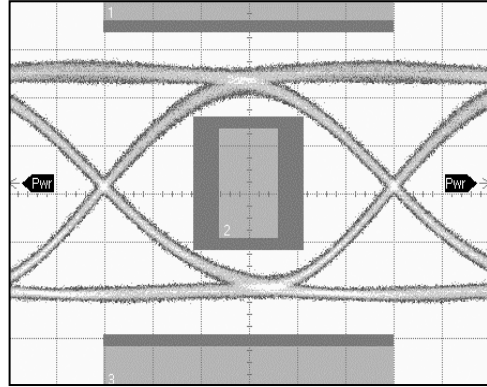


Figure 10. Optical Eye 2.488 Gbps, 65 ps/DIV, PRBS $2^{31}-1$
 $P_{AV} = 0\text{ dBm}$, ER = 9 dB, Mask Margin 22%, $T_A = 25^\circ\text{C}$

(ACQ LIMIT TEST) WAVEFORMS 1001

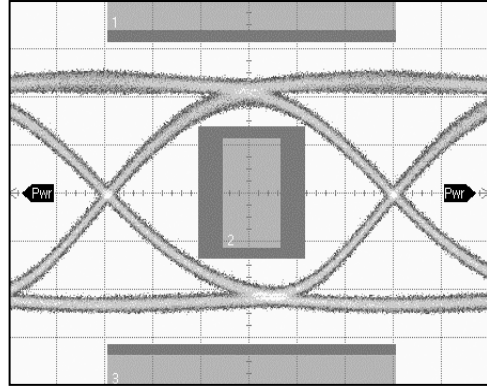


Figure 11. Optical Eye 2.488 Gbps, 65 ps/DIV, PRBS $2^{31}-1$
 $P_{AV} = -0.2\text{ dBm}$, ER = 8.96 dB, Mask Margin 21%, $T_A = 85^\circ\text{C}$

TYPICAL PERFORMANCE CHARACTERISTICS

SINGLE-ENDED OUTPUT

These performance characteristics were measured using the high speed, electrical single-ended, output circuit shown in Figure 2.

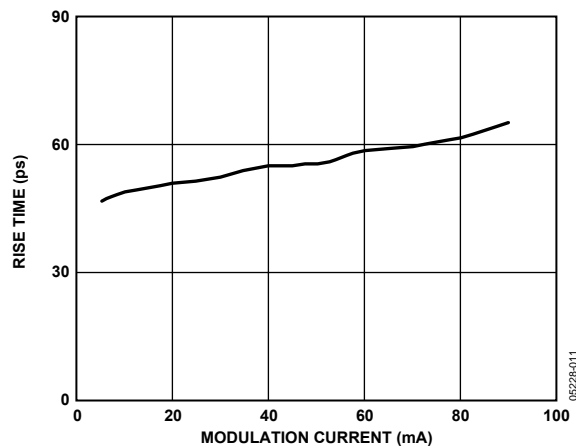


Figure 12. Rise Time vs. Modulation Current, $I_{BIAS} = 20$ mA

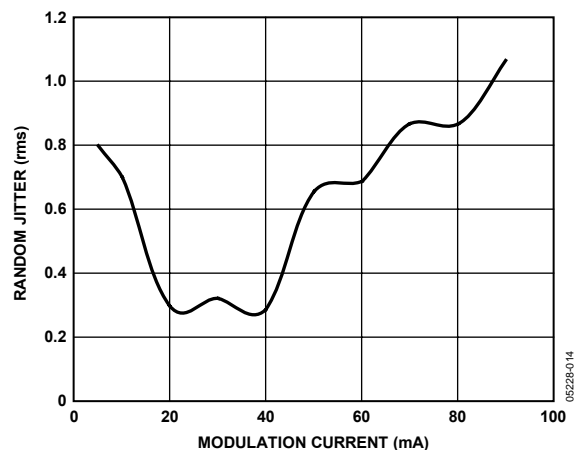


Figure 14. Random Jitter vs. Modulation Current, $I_{BIAS} = 20$ mA

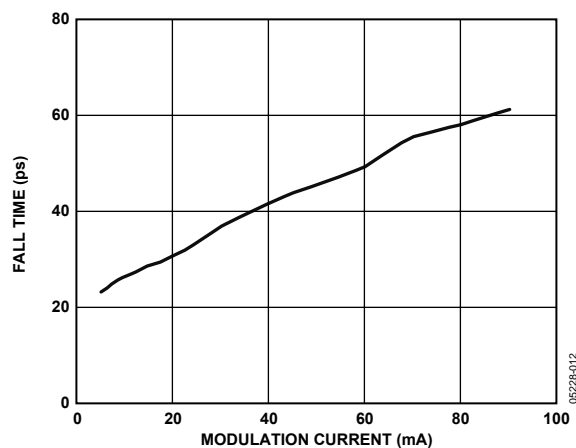


Figure 13. Fall Time vs. Modulation Current, $I_{BIAS} = 20$ mA

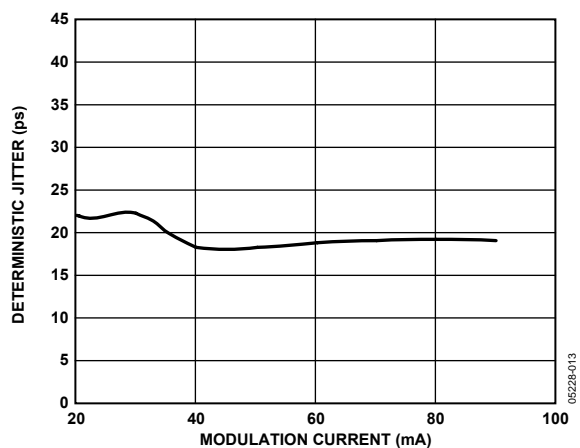


Figure 15. Deterministic Jitter at 2.488 Gbps vs. Modulation Current, $I_{BIAS} = 20$ mA

DIFFERENTIAL OUTPUT

These performance characteristics were measured using the high speed, electrical differential output circuit shown in Figure 3.

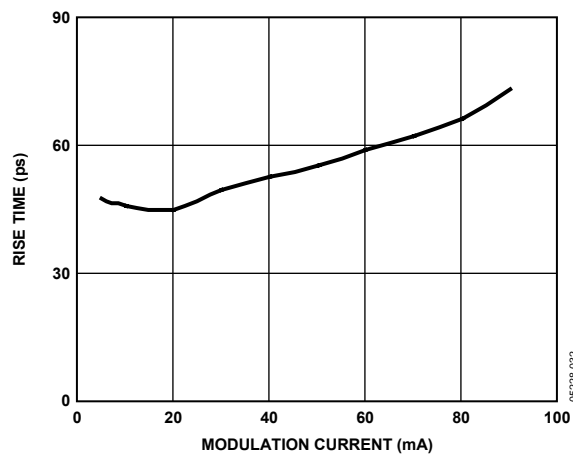


Figure 16. Rise Time vs. Modulation Current, $I_{BIAS} = 20\text{ mA}$

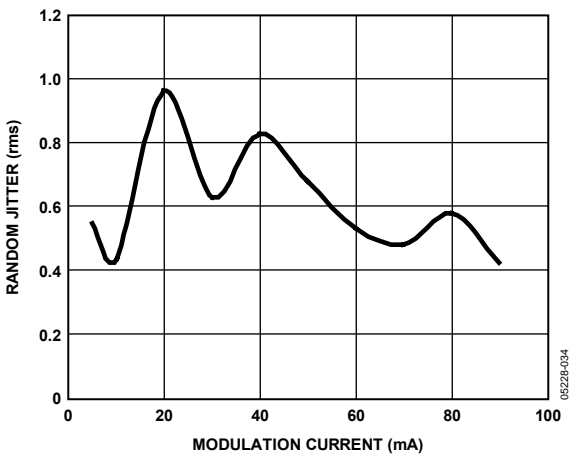


Figure 18. Random Jitter vs. Modulation Current, $I_{BIAS} = 20\text{ mA}$

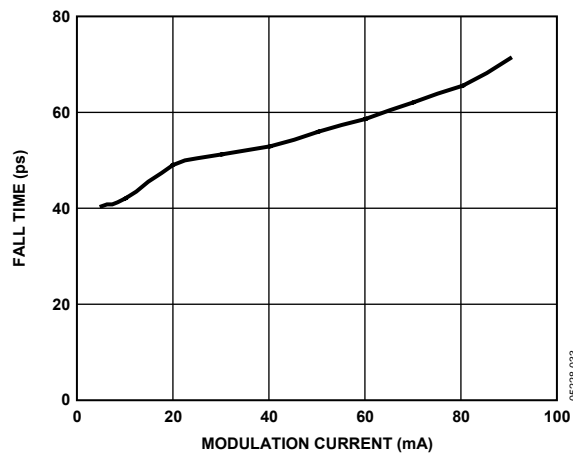


Figure 17. Fall Time vs. Modulation Current, $I_{BIAS} = 20\text{ mA}$

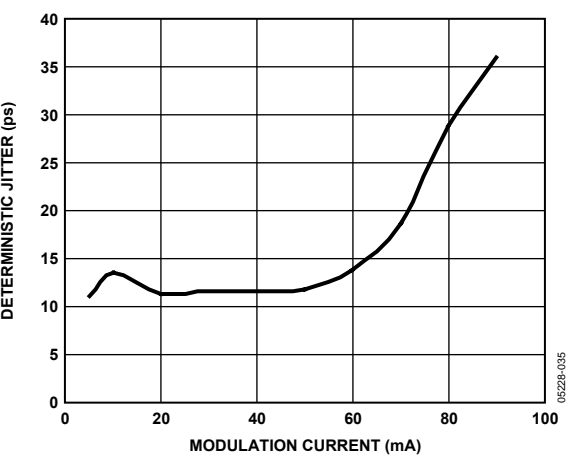


Figure 19. Deterministic Jitter at 4.25 Gbps vs. Modulation Current, $I_{BIAS} = 20\text{ mA}$

PERFORMANCE CHARACTERISTICS

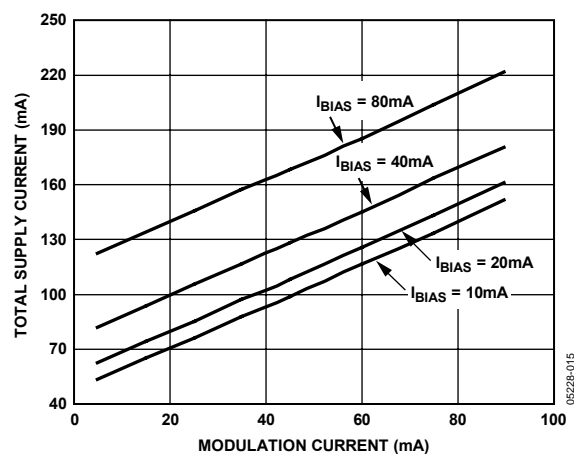


Figure 20. Total Supply Current vs. Modulation Current
 $Total\ Supply\ Current = I_{CC} + I_{BIAS} + I_{MOD}$

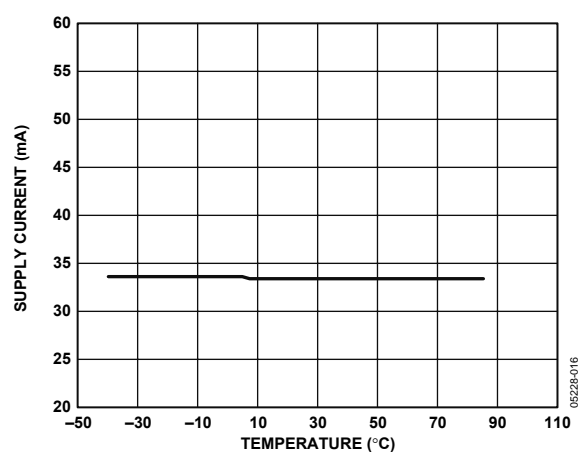


Figure 23. Supply Current (I_{CC}) vs. Temperature with ALS Asserted, $I_{BIAS} = 20\ mA$

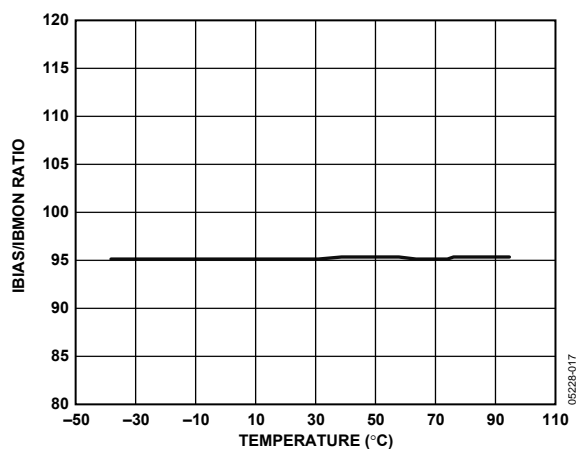


Figure 21. I_{BIAS}/I_{BMON} Gain vs. Temperature, $I_{BIAS} = 20\ mA$

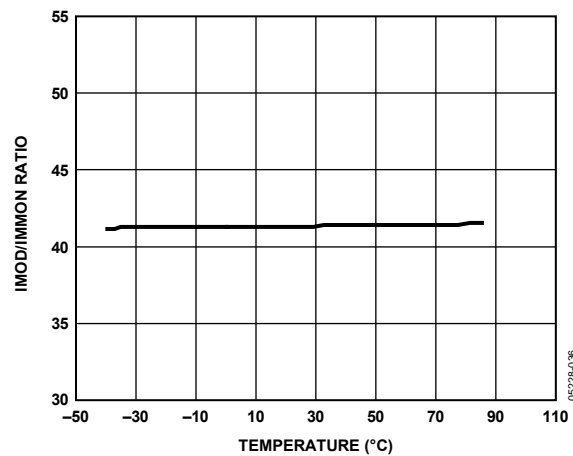


Figure 24. I_{MOD}/I_{IMON} Gain vs. Temperature, $I_{MOD} = 30\ mA$

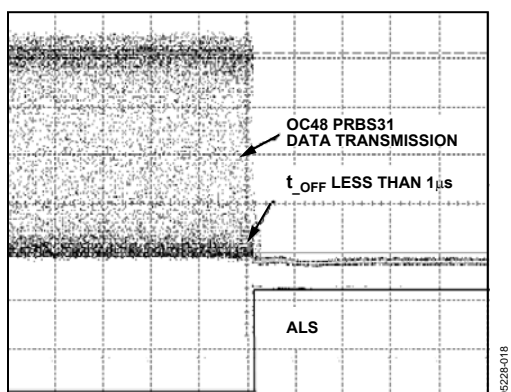


Figure 22. ALS Assert Time, $5\ \mu s/DIV$

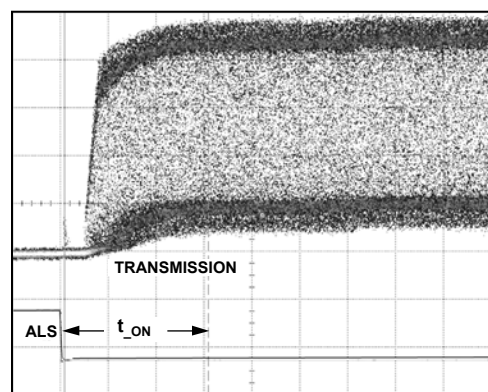


Figure 25. ALS Negate Time, $50\ \mu s/DIV$

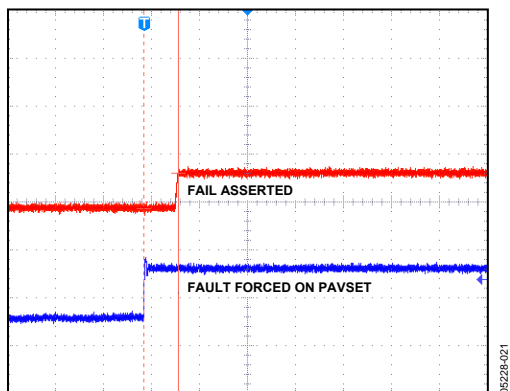


Figure 26. FAIL Assert Time, 1 μ s/DIV

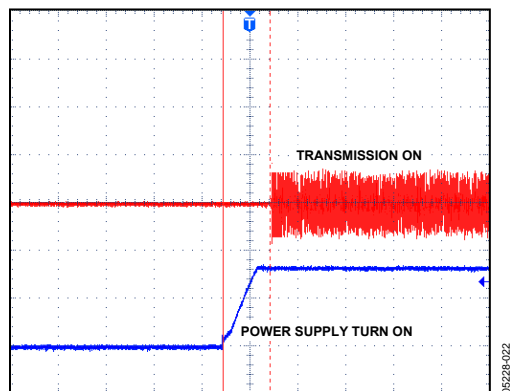


Figure 27. Time to Initialize, Including Reset, 40 ms/DIV

THEORY OF OPERATION

Laser diodes have a current-in to light-out transfer function, as shown in Figure 28. Two key characteristics of this transfer function are the threshold current, I_{th} , and the slope in the linear region beyond the threshold current, referred to as the slope efficiency, LI .

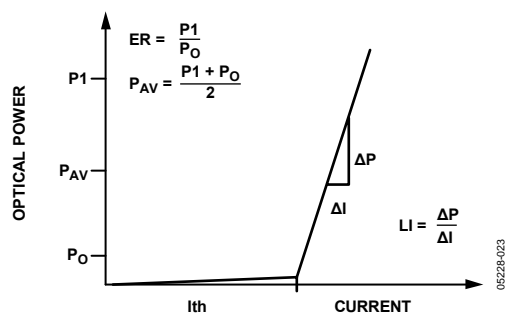


Figure 28. Laser Transfer Function

LASER CONTROL

Typically, laser threshold current and slope efficiency are both functions of temperature. For FP- and DFB-type lasers, the threshold current increases and the slope efficiency decreases with increasing temperature. In addition, these parameters vary as the laser ages. To maintain a constant optical average power and a constant optical extinction ratio over temperature and laser lifetime, it is necessary to vary the applied electrical bias current and modulation current to compensate for the changing LI characteristics of the laser.

Average Power Control Loop (APCL)

The APCL compensates for changes in I_{th} and LI by varying I_{BIAS} . Average power control is performed by measuring the MPD current, I_{MPD} . This current is bandwidth-limited by the MPD. This is not a problem because the APCL is required to respond to the average current from the MPD.

Extinction Ratio (ER) Control

ER control is implemented by adjusting the modulation current. Temperature calibration is required to adjust the modulation current to compensate for variations of the laser characteristics with temperature.

CONTROL METHODS

The ADN2871 has two methods for setting the average power (P_{AV}) and extinction ratio (ER). The average power and extinction ratio can be voltage-set using the output of a microcontroller's voltage DACs to provide controlled reference voltages, $PAVREF$ and $ERREF$. Alternatively, the average power and extinction ratio can be resistor-set using potentiometers at the $PAVSET$ and $ERSET$ pins, respectively.

VOLTAGE SETPOINT CALIBRATION

The ADN2871 allows interface to a microcontroller for both control and monitoring (see Figure 29). The average power and extinction ratio can be set using the microcontroller DACs to provide controlled reference voltages, $PAVREF$ and $ERREF$.

$$PAVREF = P_{AV} \times R_{SP} \times R_{PAV} \quad (V)$$

$$ERREF = \frac{I_{MOD} \times R_{ERSET}}{100} \quad (V)$$

where:

R_{SP} is the optical responsivity (in amperes per watt).

P_{AV} is the average power required.

$R_{PAV} = R_{ERSET} = 1 \text{ k}\Omega$.

I_{MOD} is the modulation current.

In voltage setpoint mode, R_{PAV} and R_{ERSET} must be $1 \text{ k}\Omega$ resistors with a 1% tolerance and a temperature coefficient of $50 \text{ ppm}/^\circ\text{C}$.

Power-On Sequence in Voltage Setpoint Mode

Note that during power-up, there is an internal sequence that allows 25 ms before enabling the alarms; therefore, the customer must ensure that the voltages for $PAVREF$ and $ERREF$ are active within 20 ms after ramp-up of the power supply. If the $PARREF$ and $ERREF$ voltages are supplied after 25 ms, then the part alarms and $FAIL$ is activated.



Figure 29. ADN2871 Using Microconverter Voltage Setpoint Calibration and Monitoring



Figure 30. ADN2871 Using Resistor Setpoint Calibration of Average Power and Extinction Ratio

RESISTOR SETPOINT CALIBRATION

In resistor setpoint calibration, Pin PAVREF, Pin ERREF, and Pin RPAV must all be tied to V_{CC} . The average power and extinction ratio can be set using the PAVSET and ERSET pins, respectively. A resistor is placed between the pin and GND to set the current flowing in each pin, as shown in Figure 30. The ADN2871 ensures that both PAVSET and ERSET are kept 1.23 V above GND. The PAVSET and ERSET resistors are given by

$$R_{PAVSET} = \frac{1.2 \text{ V}}{P_{AV} \times R_{SP}} \quad (\Omega)$$

$$R_{ERSET} = \frac{1.2 \text{ V} \times 100}{I_{MOD}} \quad (\Omega)$$

where:

R_{SP} is the optical responsivity (in amperes per watt).

I_{MOD} is the modulation current required (mA).

P_{AV} is the average power required (mW).

Power-On Sequence in Resistor Setpoint Mode

After power-on, the ADN2871 starts an initial process sequence that takes 25 ms before enabling the alarms. Therefore, the resistors connected to Pin PAVSET and Pin ERSET should be stabilized within 20 ms after power-on. If the PAVSET and ERSET resistors are connected to the ADN2871 20 ms after the power supply is turned on, the ADN2871 alarm may kick in and assert FAIL.

I_{MPD} MONITORING

I_{MPD} monitoring can be implemented for voltage setpoint and resistor setpoint as described next.

Voltage Setpoint

In voltage setpoint calibration, two methods can be used for I_{MPD} monitoring.

Method 1: Measuring Voltage at RPAV

The I_{MPD} current is equal to the voltage at RPAV divided by the value of RPAV (see Figure 31) as long as the laser is on and is being controlled by the control loop. This method does not provide a valid I_{MPD} reading when the laser is in shutdown or fail mode. A MicroConverter buffered ADC input can be connected to RPAV to make this measurement. No decoupling or filter capacitors should be placed on the RPAV node because this can disturb the control loop.

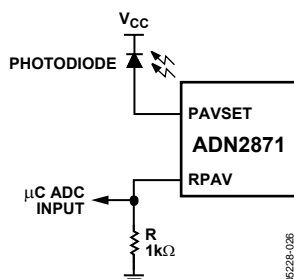


Figure 31. Single Measurement of I_{MPD} at RPAV in Voltage Setpoint Mode

Method 2: Measuring I_{MPD} Across a Sense Resistor

The second method has the advantage of providing a valid I_{MPD} reading at all times, but has the disadvantage of requiring a differential measurement across a sense resistor directly in series with the I_{MPD} . As shown in Figure 32, a small resistor, R_x , is placed in series with the I_{MPD} . If the laser used in the design has a pinout where the monitor photodiode cathode and the lasers anode are not connected, a sense resistor, R_x , can be placed in series with the photodiode cathode and V_{CC} , as shown in Figure 33. When choosing the value of the resistor, the user must take into account the expected I_{MPD} value in normal operation. The resistor must be large enough to make a significant signal for the buffered ADC to read, but small enough not to cause a significant voltage reduction across the I_{MPD} . The voltage across the sense resistor should not exceed 250 mV when the laser is in normal operation. It is recommended that a 10 pF capacitor be placed in parallel with the sense resistor.

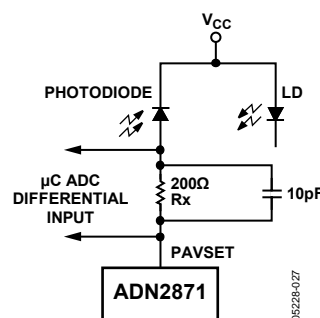


Figure 32. Differential Measurement of I_{MPD} Across a Sense Resistor

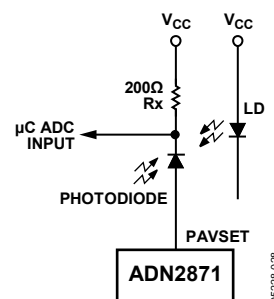


Figure 33. Single Measurement of I_{MPD} Across a Sense Resistor

Resistor Setpoint

In resistor setpoint calibration, the current through the resistor from PAVSET to ground is the I_{MPD} current. The recommended method for measuring the I_{MPD} current is to place a small resistor in series with the PAVSET resistor (or potentiometer) and measure the voltage across this resistor, as shown in Figure 34. The I_{MPD} current is then equal to this voltage divided by the value of resistor used. In resistor setpoint calibration, PAVSET is held to 1.2 V nominal; it is recommended that the sense resistor be selected so that the voltage across the sense resistor does not exceed 250 mV.

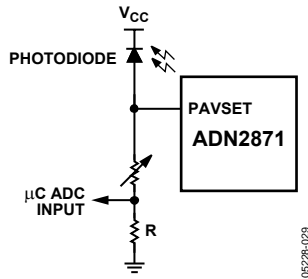


Figure 34. Single Measurement of I_{MPD} Across a Sense Resistor in Resistor Setpoint I_{MPD} Monitoring

LOOP BANDWIDTH SELECTION

To ensure that the ADN2871 control loop has sufficient bandwidth, the average power loop capacitor (PAVCAP) is calculated using the laser's slope efficiency (watts/amps) and the average power required.

For resistor setpoint control:

$$PAVCAP = 3.2 \times 10^{-6} \times \frac{LI}{P_{AV}} \quad (\text{Farad})$$

For voltage setpoint control:

$$PAVCAP = 1.28 \times 10^{-6} \times \frac{LI}{P_{AV}} \quad (\text{Farad})$$

where:

P_{AV} is the average power required (mW).

LI is the typical slope efficiency at 25°C of a batch of lasers that are used in a design (mW/mA).

LI can be calculated as

$$LI = \frac{P1 - P0}{I_{MOD}} \quad (\text{mW/mA})$$

where:

$P1$ is the optical power at the one level (mW).

$P0$ is the optical power at the zero level (mW).

The capacitor value equation is used to get a centered value for the particular type of laser that is used in a design and an average power setting. The laser LI can vary by a factor of 7 between different physical lasers of the same type and across temperatures without the need to recalculate the PAVCAP value.

This capacitor is placed between the PAVCAP pin and ground. It is important that the capacitor is a low leakage, multilayer ceramic type with an insulation resistance greater than 100 GΩ or a time constant of 1000 seconds, whichever is less. Pick a standard off-the-shelf capacitor value such that the actual capacitance is within $\pm 30\%$ of the calculated value after the capacitor's own tolerance is taken into account.

POWER CONSUMPTION

The ADN2871 die temperature must be kept below 125°C. The LFCSP has an exposed paddle, which should be connected so that it is at the same potential as the ADN2871 ground pins. Power consumption can be calculated as

$$I_{CC} = I_{CC \text{ min}} + 0.3 I_{MOD}$$

$$P = V_{CC} \times I_{CC} + (I_{BIAS} \times V_{BIAS_PIN}) + I_{MOD} (V_{MODP_PIN} + V_{MODN_PIN})/2$$

$$T_{DIE} = T_{AMBIENT} + \theta_{JA} \times P$$

Thus, the maximum combination of $I_{BIAS} + I_{MOD}$ must be calculated, where:

$I_{CC \text{ min}} = 30 \text{ mA}$, the typical value of I_{CC} provided in Table 1 with $I_{BIAS} = I_{MOD} = 0$.

T_{DIE} is the die temperature.

$T_{AMBIENT}$ is the ambient temperature.

V_{BIAS_PIN} is the voltage at the IBIAS pin.

V_{MODP_PIN} is the voltage at the IMODP pin.

V_{MODN_PIN} is the voltage at the IMODN pin.

AUTOMATIC LASER SHUTDOWN (Tx_DISABLE)

ALS (Tx_DISABLE) is an input that is used to shut down the transmitter's optical output. The ALS pin is pulled up internally with a 6 kΩ resistor and conforms to SFP MSA specifications. When ALS is logic high or when open, both the bias and modulation currents are turned off. If an alarm has triggered, and the bias and modulation currents are turned off, ALS can be brought high and then low to clear the alarm.

BIAS AND MODULATION MONITOR CURRENTS

IBMON and IMMON are current-controlled current sources that mirror a ratio of the bias and modulation current. The monitor bias current (IBMON) and the monitor modulation current (IMMON) should both be connected to ground through a resistor to provide a voltage proportional to the bias current and modulation current, respectively. When using a microcontroller, the voltage developed across these resistors can be connected to two of the ADC channels, making available a digital representation of the bias and modulation current.

ALARMS

The ADN2871 has a latched, active high monitoring alarm (FAIL). The FAIL alarm output is an open drain in conformance to SFP MSA specification requirements.

The ADN2871 has a three-fold alarm system that covers

- Use of a bias current higher than expected, probably as a result of laser aging.
- Out-of-bounds average voltage at the monitor photodiode (MPD) input, indicating an excessive amount of laser power or a broken loop.
- Undervoltage in the IBIAS node (laser diode cathode) that would increase the laser power.

The bias current alarm trip point is set by selecting the value of resistor on the IBMON pin to GND. The alarm is triggered when the voltage on the IBMON pin goes above 1.2 V. FAIL is activated when the single-point faults in Table 5 occur. The

circuit in Figure 37 can be used to indicate that FAIL has been activated while allowing the bias and modulation currents to remain on. The transistor's V_{BE} clamps the FAIL voltage to below 1.3 V disabling the automatic shutdown of bias and modulation currents. If an alarm has triggered and FAIL is activated, ALS can be brought high and then low to clear the alarm.

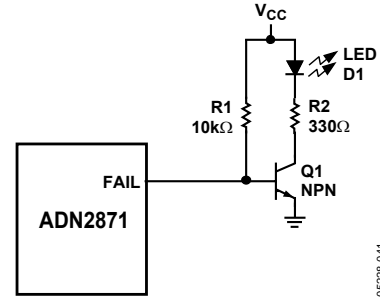


Figure 37. FAIL Indication Circuit

Table 5. ADN2871 Single-Point Alarms

Alarm Type	Mnemonic	Overvoltage or Short to V_{CC} Condition	Undervoltage or Short to GND Condition
Bias Current	IBMON	Alarm if > 1.2 V typical ($\pm 10\%$ tolerance)	Ignore
MPD Current	PAVSET	Alarm if $>$ threshold (typical threshold: 1.5 V to 2.1 V)	Alarm if $<$ threshold (typical threshold: 0.6 V to 1.1 V)
Crucial Nodes	ERREF (the ERREF designed tied to V_{CC} in resistor setting mode)	Alarm if shorted to V_{CC} (the alarm is valid for voltage setting mode only)	Ignore
	IBIAS	Ignore	Alarm if shorted to GND

Table 6. ADN2871 Response to Various Single-Point Faults in AC-Coupled Configuration (as shown in Figure 35)

Pin	Short to V_{CC}	Short to GND	Open
CCBIAS	Fault state occurs	Fault state occurs	Does not increase laser average power
PAVSET	Fault state occurs	Fault state occurs	Fault state occurs
PAVREF	Voltage mode: Fault state occurs Resistor mode: Tied to V_{CC}	Fault state occurs	Fault state occurs Circuit designed to tie to V_{CC} in resistor setting mode, so no open case
RPAV	Voltage mode: Fault state occurs Resistor mode: Tied to V_{CC}	Fault state occurs	Voltage mode: Fault state occurs Resistor mode: Does not increase average power
PAVCAP	Fault state occurs	Fault state occurs	Fault state occurs
DATAP	Does not increase laser average power	Does not increase laser average power	Does not increase laser average power
DATAN	Does not increase laser average power	Does not increase laser average power	Does not increase laser average power
ALS	Output currents shut off	Normal currents	Output currents shut off
ERSET	Does not increase laser average power	Does not increase laser average power	Does not increase laser average power
IMMON	Does not affect laser power	Does not increase laser average power	Does not increase laser average power
ERREF	Voltage mode: Fault state occurs Resistor mode: Tied to V_{CC}	Voltage mode: Does not increase average power Resistor mode: Fault state occurs	Does not increase laser average power
IBMON	Fault state occurs	Does not increase laser average power	Does not increase laser average power
FAIL	Fault state occurs	Does not increase laser average power	Does not increase laser average power
IMODP	Does not increase laser average power	Does not increase laser average power	Does not increase laser average power
IMODN	Does not increase laser average power	Does not increase laser average power	Does not increase laser power
IBIAS	Fault state occurs	Fault state occurs	Fault state occurs

OUTLINE DIMENSIONS

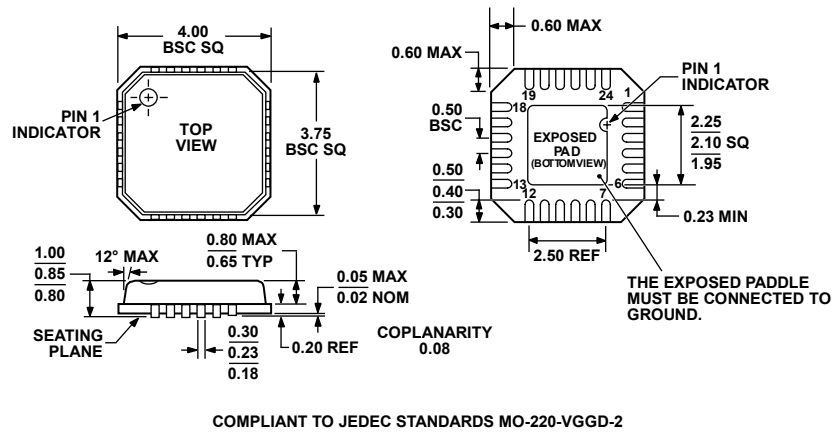


Figure 38. 24-Lead Lead Frame Chip Scale Package [LFCSP_VQ]
 4 mm × 4 mm Body, Very Thin Quad
 (CP-24-1)
 Dimensions shown in millimeters

ORDERING GUIDE

Model	Temperature Range	Package Description	Package Option
ADN2871ACPZ ¹	−40°C to +85°C	24-Lead Lead Frame Chip Scale Package (LFCSP_VQ)	CP-24-1
ADN2871ACPZ-RL ¹	−40°C to +85°C	24-Lead Lead Frame Chip Scale Package (LFCSP_VQ)	CP-24-1
ADN2871ACPZ-RL7 ¹	−40°C to +85°C	24-Lead Lead Frame Chip Scale Package (LFCSP_VQ)	CP-24-1

¹ Z = Pb-free part.

ADN2871

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- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

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