

100kHz to 1.4GHz Differential ADC Driver/IF Amplifier

FEATURES

- 100kHz to 1400MHz Bandwidth
- 54.4dBm OIP3 at 1MHz into a 100Ω Diff Load
- 48.0dBm OIP3 at 150MHz into a 100Ω Diff Load
- Up to 15dBm Output Power
- NF = 3.0dB at 240MHz
- Low 1/f Noise Corner
- User Defined Low Frequency
- 15.2dB Fixed Power Gain
- A-Grade 100% OIP3 Tested at 150MHz
- 0.8 nV/√Hz Total Input Noise
- >2.75V_{P-P} Linear Output Swing
- P1dB = 22.5dBm
- Insensitive to V_{CC} Variation
- Input/Output Internally Matched to 100Ω Differential
- Single 5V Supply
- DC Power = 850mW
- Unconditionally Stable

APPLICATIONS

- Differential 1GHz Bandwidth ADC Driver
- Wideband Test Instrument Amplifier
- Differential IF Amplifier
- 50Ω/75Ω Balanced IF Amplifier

DESCRIPTION

The LTC®6432-15 is an ultra-high dynamic range differential gain block amplifier designed to drive high resolution, high speed ADCs. It offers a full GHz of data bandwidth for complex spectrally efficient modulations schemes or where resistance to blockers is critical. This unique device can simultaneously achieve low noise, incomparable linearity and flat gain over the 100kHz to 1GHz band.

Unlike wideband GaAs PHEMTs, MESFETs and GaN FETs, this SiGe based amplifier exhibits low 1/f noise and can be used down to 100kHz.

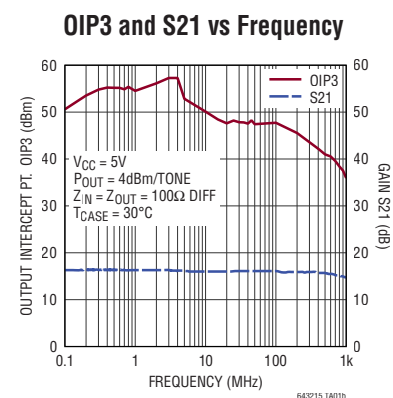
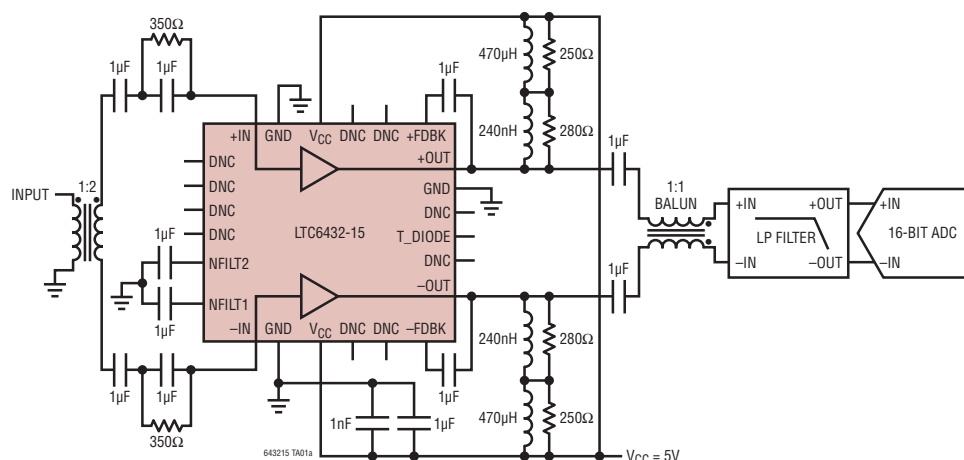
The LTC6432-15 is designed for ease of use requiring a minimum of support components. Impedance matching, temperature compensation and bias control are handled internally to ensure consistent performance over environmental changes.

All A-Grade LTC6432-15 devices are tested and guaranteed for OIP3 at 150MHz. The LTC6432-15 is housed in a 4mm × 4mm, 24L, QFN package with an exposed pad for thermal management and low inductance.

For a single-ended 50Ω IF Gain Block with similar performance, see the related LTC6433-15.

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TYPICAL APPLICATION



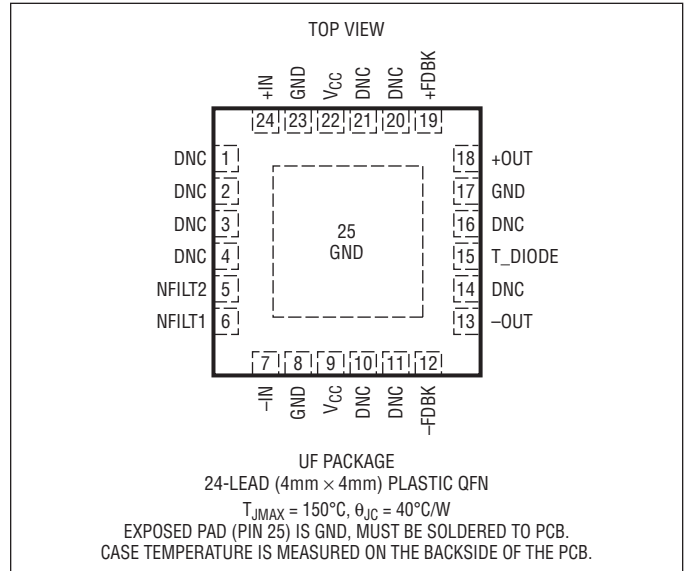
LTC6432-15

ABSOLUTE MAXIMUM RATINGS

(Note 1)

Total Supply Voltage (V_{CC} to GND)	5.5V
Amplifier Output Current (+OUT)	105mA
Amplifier Output Current (–OUT)	105mA
RF Input Power, Continuous, 50 Ω (Note 2)	+15dBm
RF Input Power, 100 μ s pulse, 50 Ω (Note 2)	+20dBm
Operating Case Temperature Range (T_{CASE})	–40°C to 85°C
Storage Temperature Range	–65°C to 150°C
Junction Temperature (T_J)	150°C
Lead Temperature (Soldering, 10 sec)	300°C

PIN CONFIGURATION



ORDER INFORMATION

<http://www.linear.com/product/LTC6432-15#orderinfo>

LEAD FREE FINISH	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	TEMPERATURE RANGE (T_{CASE})
LTC6432AIUF-15#PBF	LTC6432AIUF-15#TRPBF	43215	24-Lead (4mm × 4mm) Plastic QFN	–40°C to 85°C
LTC6432BIUF-15#PBF	LTC6432BIUF-15#TRPBF	43215	24-Lead (4mm × 4mm) Plastic QFN	–40°C to 85°C

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.

For more information on lead free part marking, go to: <http://www.linear.com/leadfree/>

For more information on tape and reel specifications, go to: <http://www.linear.com/tapeandree/>. Some packages are available in 500 unit reels through designated sales channels with #TRMPBF suffix.

The LTC6432-15 is available in two grades. Grade A guarantees a minimum OIP3 at 150MHz while grade B does not. A- and B-grades are identified by a label on the shipping container.

DC ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}\text{C}$, $V_{CC} = 5\text{V}$, $Z_{SOURCE} = Z_{LOAD} = 100\Omega$. Typical measured DC electrical performance using Test Circuit A (Note 3).

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
V_S	Operating Supply Range		4.75	5	5.25	V
$I_{S,TOT}$	Total Supply Current	All V_{CC} Pins Plus +OUT and –OUT.	● 145 110	166	195 220	mA mA
$I_{S,OUT}$	Total Supply Current to OUT Pins	Current to +OUT and –OUT	● 130 100	152	185 200	mA mA
I_{VCC}	Current to V_{CC} Pin	Either V_{CC} Pin May Be Used	● 13 12.5	14	17 17.5	mA mA

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_{CASE} = 30^{\circ}\text{C}$ (Note 3). $V_{CC} = 5\text{V}$, $Z_{SOURCE} = Z_{LOAD} = 100\Omega$, unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50 Ω SMA to 50 Ω SMA without de-embedding (Note 4).

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Small Signal						
BW	–3dB Bandwidth	De-Embedded to Package w Ext. 1 μF FDBK Capacitor	0.1	2000		MHz
S11	Differential Input Match, 100kHz to 1400MHz	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		–10		dB
S21	Forward Differential Power Gain, 100kHz to 400MHz	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.1		dB
S12	Reverse Differential Isolation, 100kHz to 4000MHz	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		–19		dB
S22	Differential Output Match, 100kHz to 1400MHz	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		–10		dB
Frequency = 100kHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		16.0		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		50.5 47		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		–97 –90		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–85		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–61		dBc
P1dB	Output 1dB Compression Point			22.5		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		6.6		dB
Frequency = 1MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.9		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		54.5 51		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		–105 –98		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–99.5		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–66.8		dBc
P1dB	Output 1dB Compression Point			22.5		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.9		dB
Frequency = 10MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.9		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		50.1 47		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		–96.2 –90		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–88.8		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		–84		dBc
P1dB	Output 1dB Compression Point			22.7		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.6		dB

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_{CASE} = 30^{\circ}\text{C}$ (Note 3). $V_{CC} = 5\text{V}$, $Z_{SOURCE} = Z_{LOAD} = 100\Omega$, unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50 Ω SMA to 50 Ω SMA without de-embedding (Note 4).

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Frequency = 50MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.9		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		48.0 45		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-92 -86		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-85.5		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-90.5		dBc
P1dB	Output 1dB Compression Point			22.9		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		2.9		dB
Frequency = 150MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor ●	14.5 14.2	15.9	16.5 16.8	dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 8\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		47.0 47		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 8\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-96.6 -90		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-92.2		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-86.5		dBc
P1dB	Output 1dB Compression Point			22.7		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.2		dB
Frequency = 240MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.8		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		45 42		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-86 -80		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-93.7		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-81.5		dBc
P1dB	Output 1dB Compression Point			22.6		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.4		dB
Frequency = 300MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.8		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		43.5 40		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-83 -76		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-90.7		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-81.4		dBc
P1dB	Output 1dB Compression Point			22.5		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.6		dB

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_{CASE} = 30^{\circ}\text{C}$ (Note 3). $V_{CC} = 5\text{V}$, $Z_{SOURCE} = Z_{LOAD} = 100\Omega$, unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50 Ω SMA to 50 Ω SMA without de-embedding (Note 4).

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Frequency = 500MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		15.4		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		41 39		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-78 -74		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-82.9		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-67.4		dBc
P1dB	Output 1dB Compression Point			21.9		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		3.9		dB
Frequency = 1000MHz						
S21	Differential Power Gain	De-Embedded to Package w Ext. 1 μF FDBK Capacitor		14.6		dB
OIP3	Output Third-Order Intercept Point	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		36 33		dBm dBm
IM3	Third-Order Intermodulation	$P_{OUT} = 2\text{dBm/Tone}$, $\Delta f = 1\text{MHz}$, $Z_0 = 100\Omega$ Grade A Grade B		-68 -62		dBc dBc
HD2	Second Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-67.2		dBc
HD3	Third Harmonic Distortion	$P_{OUT} = 8\text{dBm}$		-57.5		dBc
P1dB	Output 1dB Compression Point			19.2		dBm
NF	Noise Figure	De-Embedded to Package for Balun Input Loss		4.8		dB

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: Guaranteed by design and characterization. This parameter is not tested.

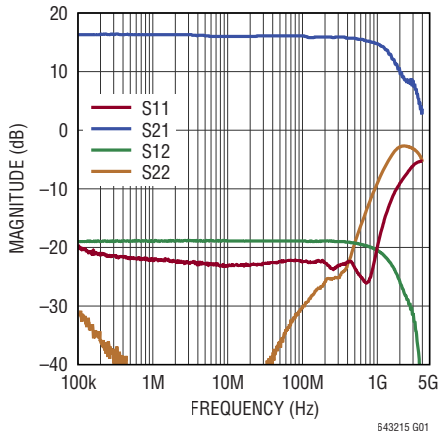
Note 3: The LTC6432-15 is guaranteed functional over the case operating temperature range of -40°C to 85°C .

Note 4: Small signal parameters S and Noise are de-embedded to the package pins, while large signal parameters are measured directly from the test circuit.

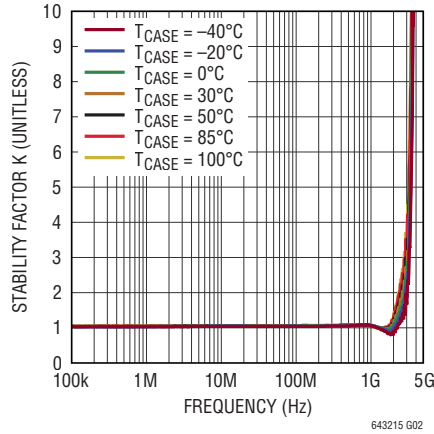
TYPICAL PERFORMANCE CHARACTERISTICS

$T_{CASE} = 30^{\circ}\text{C}$, $V_{CC} = 5\text{V}$, $Z_{IN} = Z_{OUT} = 100\Omega$ Diff.
Unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50 Ω SMA to 50 Ω SMA without de-embedding.

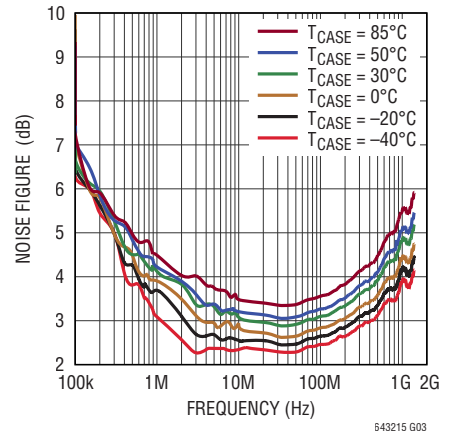
Differential S Parameters vs Frequency



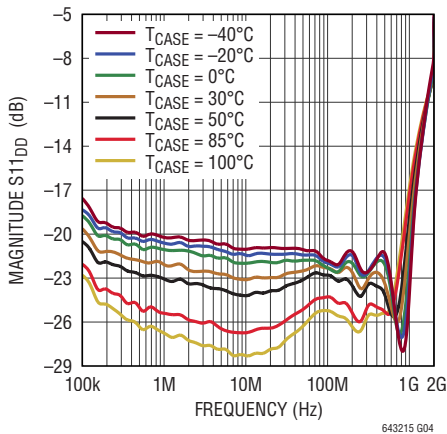
Differential Stability Factor K vs Frequency Over Temperature



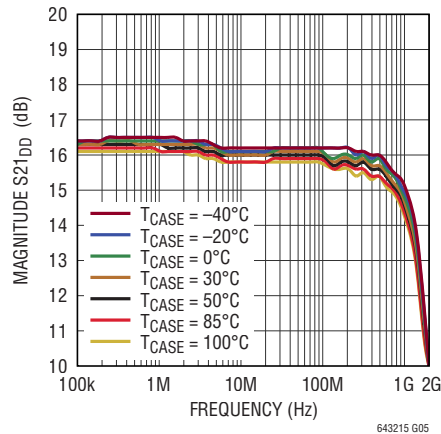
Differential Noise Figure vs Frequency Over Temperature



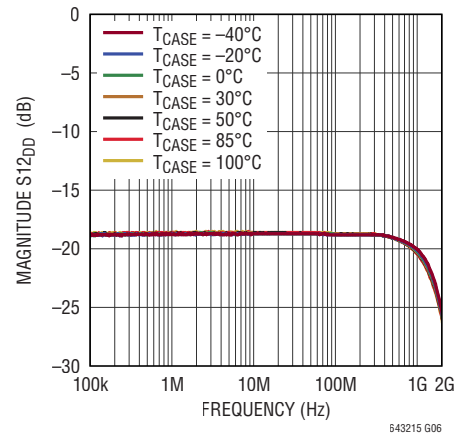
Differential Input match (S_{11DD}) vs Frequency Over Temperature



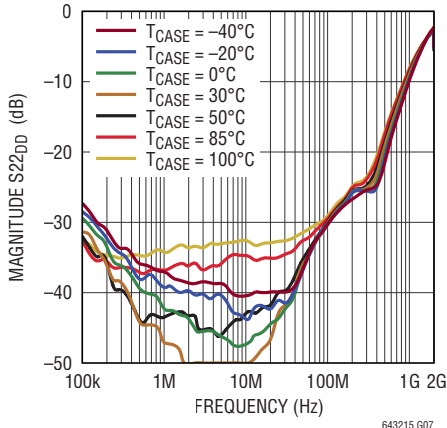
Differential Gain (S_{21DD}) vs Frequency Over Temperature



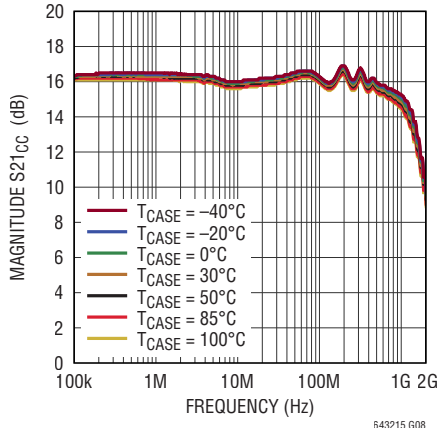
Differential Reverse Isolation (S_{12DD}) vs Frequency Over Temperature



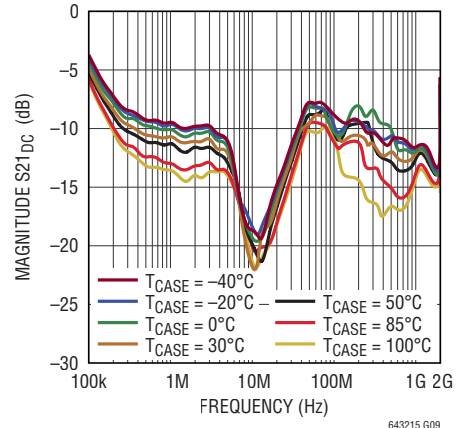
Differential Output Match (S_{22DD}) vs Frequency Over Temperature



Common Mode Gain (S_{21CC}) vs Frequency Over Temperature



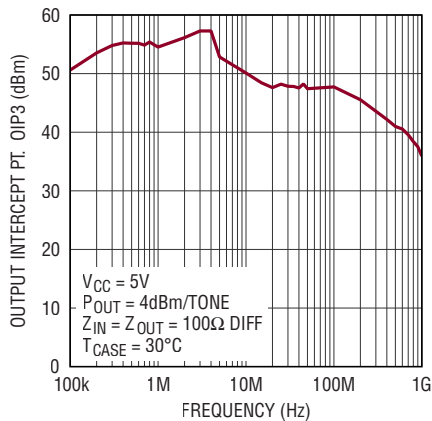
CM to DM Gain (S_{21DC}) vs Frequency Over Temperature



TYPICAL PERFORMANCE CHARACTERISTICS

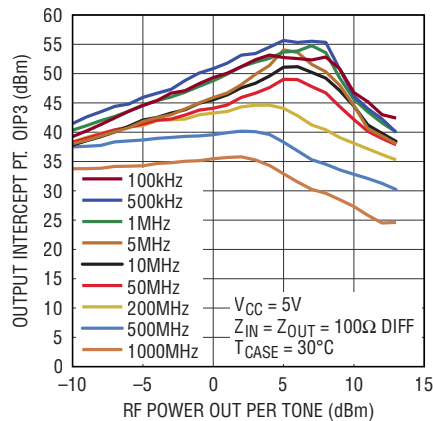
$T_{CASE} = 30^{\circ}\text{C}$, $V_{CC} = 5\text{V}$, $Z_{IN} = Z_{OUT} = 100\Omega$ DIFF.
Unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50 Ω SMA to 50 Ω SMA without de-embedding.

OIP3 vs Frequency



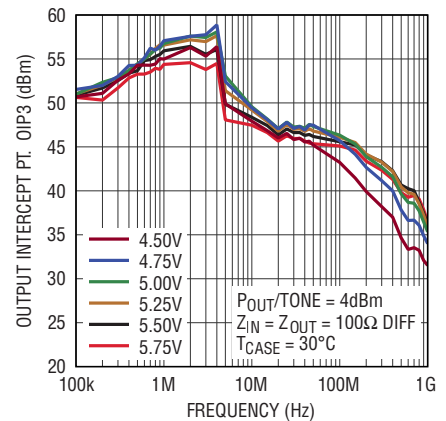
643215 G10

OIP3 vs RF Power Out/Tone Over Frequency



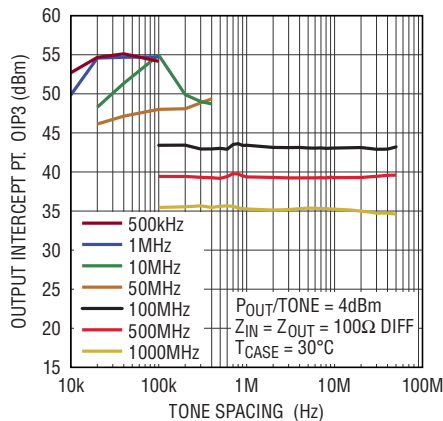
643215 G11

OIP3 vs Supply Voltage Over Frequency



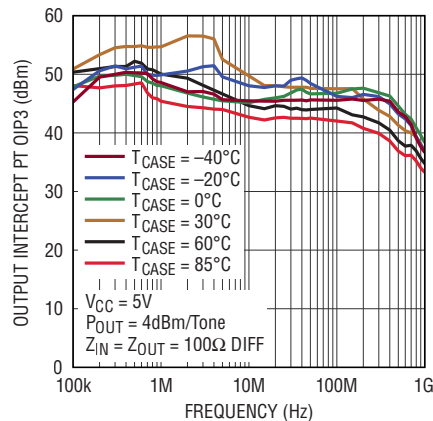
643215 G12

OIP3 vs Tone Spacing Over Frequency



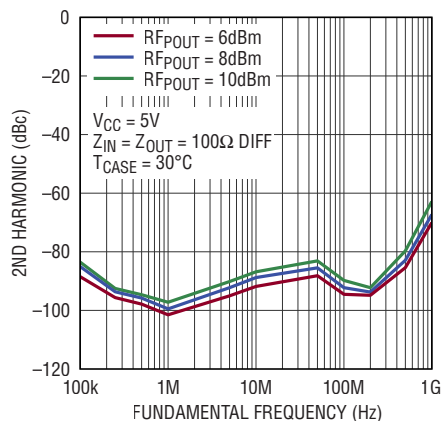
643215 G13

OIP3 vs Frequency Over Temperature



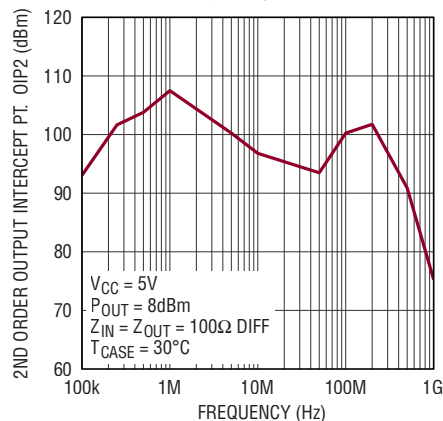
643215 G14

HD2 vs Frequency Over RF Power Out



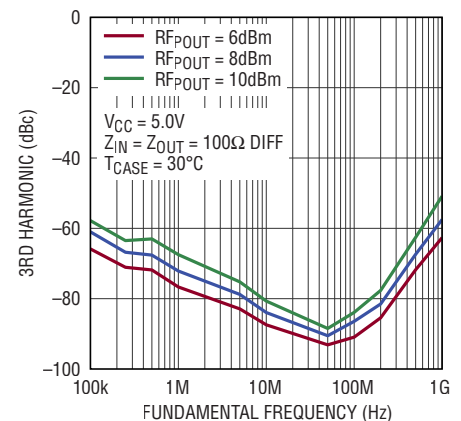
643215 G15

OIP2 vs Frequency



643215 G16

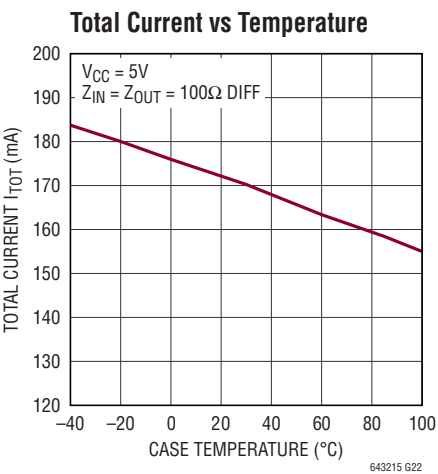
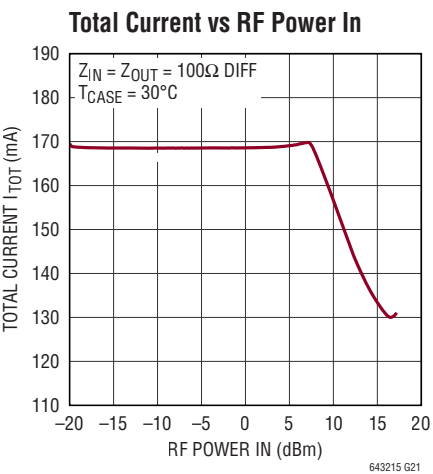
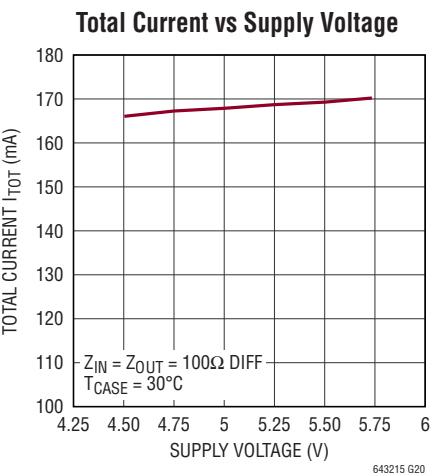
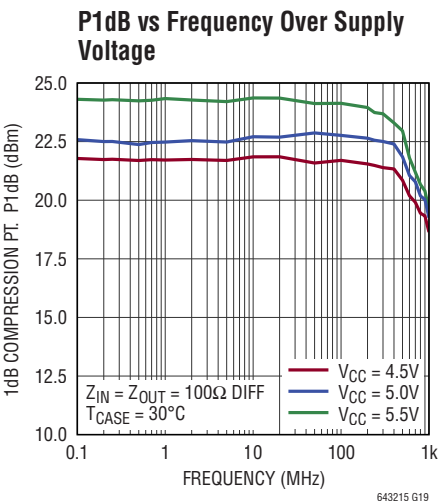
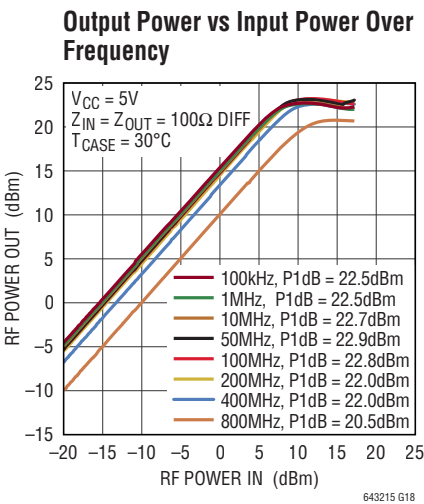
HD3 vs Frequency Over RF Power Out



643215 G17

643215f

TYPICAL PERFORMANCE CHARACTERISTICS $T_{CASE} = 30^{\circ}C, V_{CC} = 5V, Z_{IN} = Z_{OUT} = 100\Omega$ Diff.
Unless otherwise noted, measurements are performed using Test Circuit A, measuring from 50Ω SMA to 50Ω SMA without de-embedding.



PIN FUNCTIONS

DNC (Pins 1, 2, 3, 4, 10, 11, 14, 16, 20, 21): Do Not Connect. Do not connect to these pins, allow them to float. *Failure to float these pins may impair the performance of the LTC6432-15.*

NFILT2 (Pin 5): A 1 μ F capacitor to ground is required to reduce the low frequency noise of the internal bias supply.

NFILT1 (Pin 6): A 1 μ F capacitor to ground is required to reduce the low frequency noise of the internal bias supply.

-IN (Pin 7): Negative Signal Input Pin. This pin has an internally generated 2V DC bias. A DC blocking capacitor is required. See Application Information for specific recommendations.

GND (Pins 8, 17, 23 Exposed Pad Pin 25): Ground. For best RF performance, all ground pins should be connected to the printed circuit board ground plane. The Exposed Pad (Pin 25) should have multiple via holes to an underlying ground plane for low inductance and good thermal dissipation.

V_{CC} (Pins 9, 22): Positive Power Supply. Either or both V_{CC} pins should be connected to the 5V supply. Pins 9 and 22 are internally connected on chip. Bypass the V_{CC} Pin with 1000pF and 0.1 μ F capacitors. The 1000pF capacitor should be physically close to the V_{CC} Pin.

-FDBK (Pin 12): A 1 μ F capacitor is required between this pin and -OUT to extend the low frequency cutoff.

-OUT (Pin 13): Negative Amplifier Output Pin. A transformer with a center tap tied to V_{CC} or a choke inductor is required to provide DC current and RF isolation. For best performance select a choke with low loss and high Self Resonant Frequency (SRF). See Applications Information Section for more information.

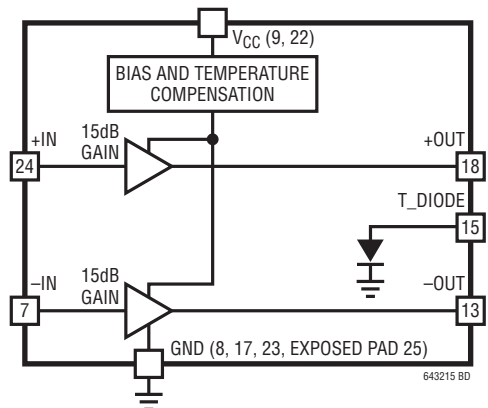
T₋DIODE (Pin 15): Optional. A diode which can be forward biased to ground with up to 1mA of current. The measured voltage will be an indicator of the chip temperature.

+OUT (Pin 18): Positive Amplifier Output Pin. A transformer with a center tap tied to V_{CC} or a choke inductor tied to 5V supply is required to provide DC current and RF isolation. For best performance select a choke with low loss and high Self Resonant Frequency (SRF). See Applications Information Section for more information.

+FDBK (Pin 19): A 1 μ F capacitor is required between this pin and +OUT to extend the low frequency cutoff.

+IN (Pin 24): Positive Signal Input Pin. This pin has an internally generated 2V DC bias. A DC blocking capacitor is required. See Application Information Section for specific recommendations.

BLOCK DIAGRAM



TEST CIRCUIT A

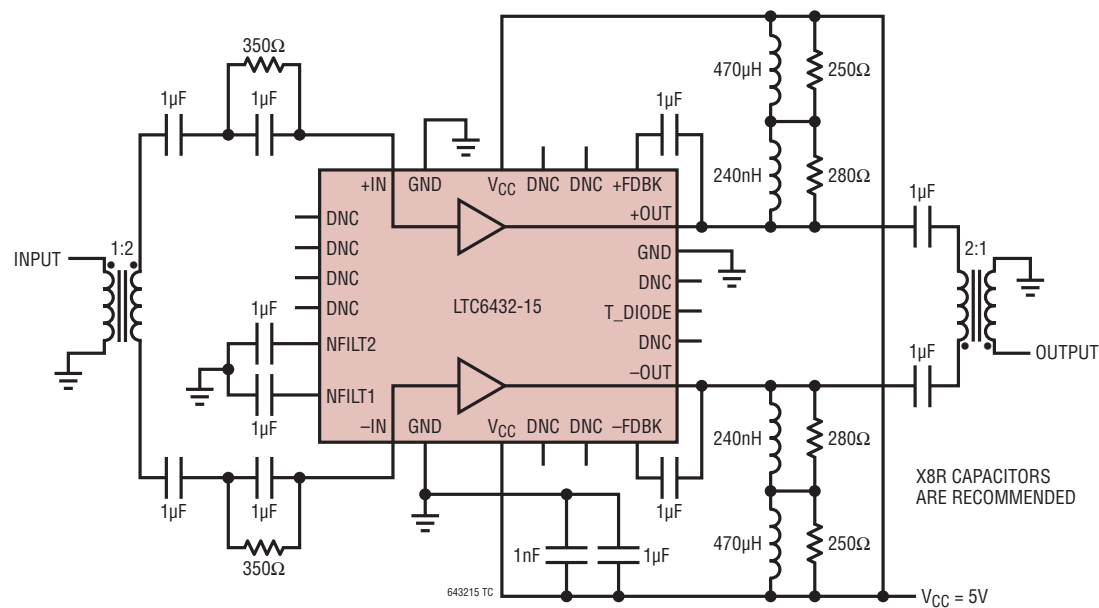


Figure 1. Differential Application Test Circuit A (Balanced Amp)

OPERATION

The LTC6432-15 is a highly linear, fixed gain differential amplifier. It can be considered a pair of 50Ω single-ended devices operating 180 degrees apart. Its core signal path consists of a single amplifier stage minimizing stability issues. The input is a Darlington pair for high input impedance and high current gain. Additional circuit enhancements increase the output impedance commensurate with the input impedance and minimize the effects of internal Miller capacitance.

The LTC6432-15 uses a classic RF gain block topology, with enhancements to achieve excellent linearity. Shunt and Series feedback elements are added to simultaneously lower the input/output impedance and match them to the 100Ω differential source and load. An internal bias controller optimizes the bias point for peak linearity over environmental changes. This circuit architecture provides low noise, good RF power handling capability and wide bandwidth; characteristics that are desirable for IF signal chain applications.

APPLICATIONS INFORMATION

The LTC6432-15 is a highly linear fixed gain amplifier designed for ease of use. Both the input and output are matched to 100Ω differential source and load impedance from 100kHz to 1000MHz using the specified evaluation circuit. Biasing and temperature compensation are also handled internally to deliver optimized performance. The designer need only supply input/output blocking caps, RF chokes, feedback caps, filter caps and decoupling caps for the 5V supply. However, because the device is capable of such wide band operation, a single application circuit will probably not result in optimized performance across the full frequency band.

Differential circuits minimize the common mode noise and 2nd harmonic distortion issues that plague many designs. The LTC6432's differential topology matches well with the differential inputs of an ADC. However, evaluation of these differential circuits is difficult, as high resolution, high frequency, differential test equipment is lacking.

Our test circuit is designed for evaluation with standard single-ended 50Ω test equipment. Therefore, 1:2 balun transformers have been added to the input and output to transform the LTC6432-15's 100Ω differential source/load impedance to 50Ω single-ended impedance, compatible with most test equipment.

Other than the balun, the evaluation circuit requires a minimum of external components. Input and output DC blocking caps are required as this device is internally biased

for optimal operation. A frequency appropriate choke and decoupling caps provide DC bias to the RF \pm OUT nodes. Only a single 5V supply is necessary to either of the V_{CC} pins on the device. Both V_{CC} pins are connected inside the package. Two V_{CC} pins are provided for the convenience of supply routing on the PCB. An optional parallel $1\mu F$, 350Ω input network has been added to ensure low frequency stability.

The particular element values shown in Test Circuit A are chosen for wide bandwidth operation. Depending on the desired frequency, performance may be improved by proper selection of these supporting components.

Choosing the Right RF Choke

Not all choke inductors are created equal. It is always important to select an inductor with low R_{LOSS} as this will drop the available voltage to the device. Also look for an inductor with high self resonant frequency (SRF) as this will limit the upper frequency where the choke is useful. Above the SRF, the parasitic capacitance dominates and the choke's impedance will drop. For these reasons, wire wound inductors are preferred, while multilayer ceramic chip inductors should be avoided for an RF choke if possible. Since the LTC6432-15 is capable of such wideband operation, a single choke value will not result in optimized performance across its full frequency band. Table 1 list common frequency bands and suggested corresponding inductor values

APPLICATIONS INFORMATION

Table 1. Target Frequency and Suggested Inductor Values

FREQUENCY BAND (MHz)	INDUCTOR VALUE (H)	SRF (MHz)	MODEL NUMBER	MANUFACTURER
0.1 to 20	470 μ H	4	LPS5030	Coilcraft www.coilcraft.com
20 to 100	1500nH	100	0603LS	
100 to 500	560nH	525	0603LS	
500 to 1000	100nH	1150	0603LS	

Designing a Wideband Output Network

Often a single choke will not work over a wide bandwidth due to a low SRF or low inductance value. Using multiple choke stages, it is possible to extend the frequency range of the output network. This is best done using a circuit simulator and S parameters provided by the inductor manufacturer or measured by the user. Please refer to the output network in Figure 1 Test circuit A. Starting at OUT we connect two chokes in series, a 240nH RF choke and follow that with a 470 μ H choke to provide high AC impedance at 100kHz. It is important to place the lower valued (higher SRF) choke closer to the signal line for best performance. De-Qing resistors 250 Ω and 280 Ω respectively have been placed in parallel with the chokes. This flattens the loss of the output network and gives an overall flat gain response for the amplifier application circuit. With proper care selecting chokes, wideband performance is possible. In this case circuit A works over 13 octaves.

DC Blocking Capacitor

The role of a DC blocking capacitor is straightforward: block the path of DC current and allow a low series impedance path for the AC signal. Lower frequencies require a higher value of DC blocking capacitance. Generally, 1 μ F will suffice for operation down to 100kHz.

RF Bypass Capacitor

RF bypass capacitors act to shunt the AC signals to ground with a low impedance path. They prevent the AC signal from getting into the DC bias supply. It is best to place the bypass capacitor as close as possible to the DC supply pins of the amplifier. Any extra distance translates into additional series inductance which lowers the effective-

ness of the bypass capacitor network. The suggested bypass capacitor network consists of two capacitors; a low value 1000pF capacitor to shunt high frequencies and a larger 1 μ F capacitor to handle lower frequencies. Use ceramic capacitors of appropriate physical size for each capacitance value (e.g. 0402 for the 1000pF, 0805 for the 0.1 μ F) to minimize the equivalent series resistance (ESR) of the capacitor.

High Valued Capacitors and Linearity degradation

One might not expect a passive element to create signal distortions. However, high value capacitors can create nonlinear responses at frequencies below 1MHz. Typically lower quality materials are used to create high density capacitors. High quality NPO and film capacitors have low capacitance density and become unmanageably large at 1 μ F values. Typical low quality capacitors have high voltage coefficients that deviate from their expected linear response, creating IM products and harmonics. We have found that automotive grade X8R capacitors have reasonable voltage coefficients at high capacitance densities and will not degrade the linearity of the LTC6432-15. We highly suggest their use in the 6 DC blocking capacitors and the 2 feedback capacitors shown in the application circuit.

Low Frequency Stability

Most RF gain blocks suffer from low frequency instability. To avoid stability issues, the LTC6432-15, contains an on-chip feedback network that lowers the gain and matches the input and output impedance of the intrinsic amplifier. This feedback network contains a series capacitor, whose value is limited by physical size. So at some low frequency, this feedback capacitor looks like an open circuit; the feedback fails, gain increases and gross impedance mismatches occur which can create instability. This situation is easily resolved with a parallel capacitor and a resistor network on the input. This is shown in Figure 1. This network provides resistive loss at low frequencies and is bypassed by the capacitor at the desired band of operation. However, if the LTC6432-15 is preceded by a low frequency termination such as a choke or balun transformer, the input stability network is not required.

APPLICATIONS INFORMATION

Exposed Pad and Ground Plane Considerations

As with any RF device, minimizing the ground inductance is critical. Care should be taken with PC board layouts using exposed pad packages, as the exposed pad provides the lowest inductive path to ground. The maximum allowable number of minimum diameter via holes should be placed underneath the exposed pad and connect to as many ground plane layers as possible. This will provide good RF ground and low thermal impedance. Maximizing the copper ground plane at the signal and microstrip ground will also improve the heat spreading and lower inductance. It is a good idea to cover the via holes with solder mask on the backside of the PCB to prevent the solder from wicking away from the critical PCB to exposed pad interface. One to two ounces of copper plating is suggested to improve heat spreading from the device.

Frequency limitations

The LTC6432-15 is a wide bandwidth amplifier but it is not intended for operation down to DC. The lower frequency cutoff is limited by on-chip matching elements. The cutoff may be arbitrarily pushed lower with off chip elements. However, the translation between the low fixed DC common mode input voltage and the higher open collector DC common mode output bias point make DC-coupled operation impractical.

Test Circuit A

Test Circuit A shown in Figure 1 is designed to allow for the evaluation of the LTC6432-15 with standard single-ended 50Ω test equipment. This allows the designer to verify the performance when the device is operated differentially. This evaluation circuit requires a minimum of external components. Since the LTC6432-15 operates over a very wide bandwidth, the evaluation test circuit is optimized for wideband operation. Obviously, for narrowband operation, the circuit can be further optimized.

Input and output DC blocking capacitors are required, as this device is internally DC biased for optimal performance. A frequency appropriate choke and decoupling capacitors are required to provide DC bias to the RF output nodes (+OUT and -OUT). A 5V supply should also be applied

to one of the V_{CC} pins on the device. Two noise filtering capacitors should be tied to ground at NFILT1 and NFILT2 to suppress noise below 20MHz. In addition 1μF capacitors should be tied between +FDBK and +OUT and between -FDBK and -OUT to provide impedance matching below 20MHz.

Components for a suggested parallel 1μF, 350Ω stability network have been added to ensure low frequency stability. The 1μF capacitance can be increased to improve low frequency (<100kHz) performance, however the designer needs to be sure that the impedance presented at low frequency will not create an instability.

As mentioned earlier, the LTC6432-15 is extremely wide-band. Its bandwidth is most often limited by the passive components surrounding it. The DC2496A evaluation board has provisions to allow characterization over the full bandwidth of the LTC6432-15 by substituting baluns and output networks. This balanced amplifier circuit is a replica of the Test Circuit A. It is useful for single-ended 50Ω amplifier requirements and is surprisingly wide band. Using this balanced arrangement and the frequency appropriate baluns, one can achieve the intermodulation and harmonic performance listed in the AC Electrical Characteristics of this data sheet. Besides its impressive intermodulation performance; the LTC6432-15 has impressive 2nd harmonic suppression as well. This makes it particularly well suited for multi-octave applications where the 2nd harmonic cannot be filtered.

This balanced circuit example uses two mini-circuits 1:2 baluns. The baluns were chosen for their bandwidth and frequency options. See Table 2. A pair of these baluns, back to back has less than 1.5dB of loss, so the penalty for this level of performance is minimal. Any 1:2 balun may be used to create a balanced amplifier with the LTC6432-15, but one must be careful that the balun does not degrade the linearity of the circuit.

The optional input stability network is only required when the balun's bandwidth reaches below 100kHz. It is included in the circuit as a comprehensive protection for any passive element placed at the LTC6432-15 input. Its performance degradation at low frequencies can be mitigated by increasing the 1μF capacitor's value.

APPLICATIONS INFORMATION

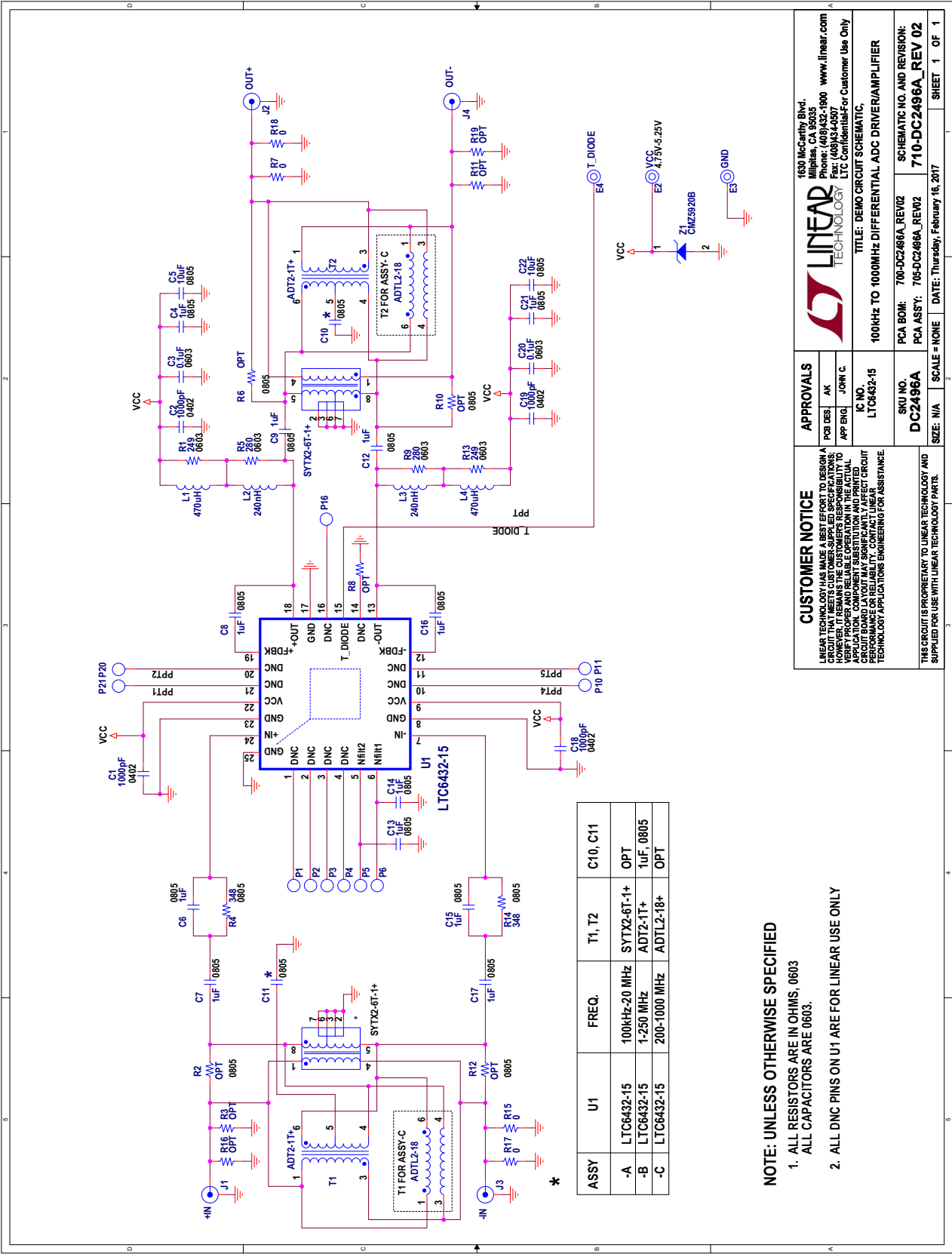


Figure 2. DC2496A Balanced Amplifier Circuit – 50Ω Input and 50Ω Output

APPLICATIONS INFORMATION

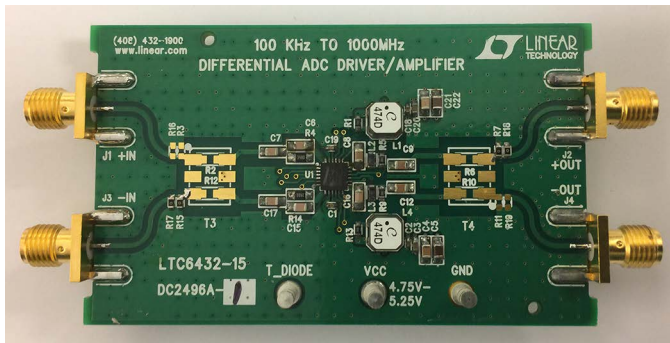


Figure 3. DC2496A Topside No Baluns Installed

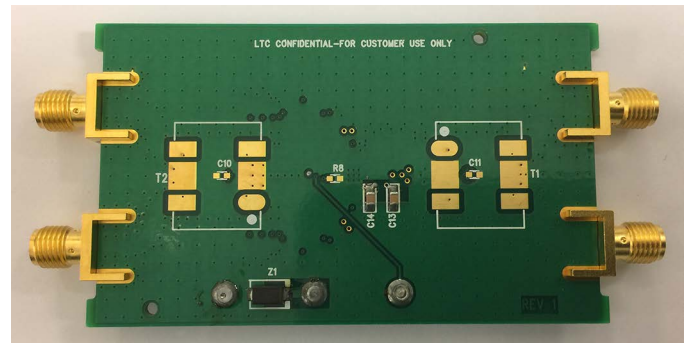


Figure 4. DC2496A Backside No Baluns Installed

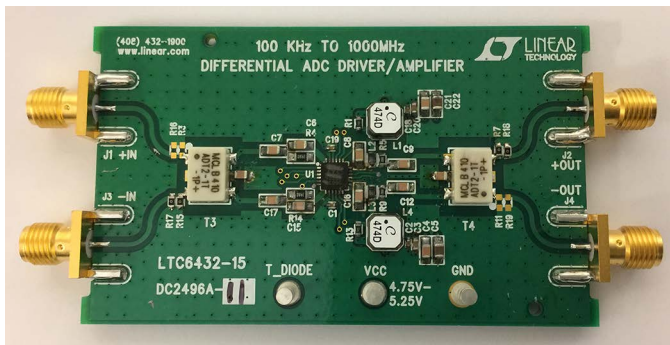


Figure 5. DC2496A Topside with Balun Installed

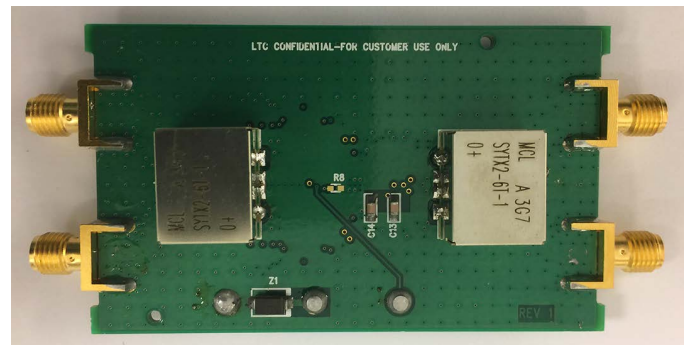


Figure 6. DC2496A Backside with Baluns Installed

Table 2. Target Frequency and Suggested 2:1 Balun

FREQUENCY BAND (MHz)	MODEL NUMBER	MANUFACTURER
0.1 to 20	SYTX2-6T-1+	Mini-Circuits www.minicircuits.com
1 to 250	ADT2-1T+	
20 to 400	ADT2-1T-1P+	
200 to 950	ADTL2-18+	

The DC2496A is designed for versatility to cover a wide range of applications. There are provisions for baluns on both the topside and backside of the DC2496A PCB. Please see Figures 3 through 6 for details. The smaller footprint ADTX2-X baluns can be mounted on the front while the larger SYTX2-6T balun can be mounted on the back. Table 2 lists the recommended Balun for each frequency range. Alternatively, the circuit can be operated differentially by using zero ohm jumpers across T3 and T4.

The plots below show the resulting small signal performance for each balun choice. More detailed results and operation details can be found in the DC2496A Quick Start Guide.

The LTC6432-15's differential output and high linearity make it the ideal solution to drive the demanding differential inputs of a high resolution ADC. In Figure 11 we show suggested circuit to drive an ADC. Both input and output are AC-coupled. A 1:2 Balun has been inserted at the input allowing a single-ended 50Ω input. The output impedance is 100Ω differential. However, a 1:1 Balun has been added to the output to suppress common mode signals. This is followed by a low pass filter to limit the noise presented to the ADC.



DIFFERENTIAL S PARAMETERS

5V, $Z_{\text{DIFF}} = 100\Omega$, $T_{\text{CASE}} = 30^\circ\text{C}$, de-embedded to package pins, 1 μF capacitor +FDBK to OUT+ and 1 μF capacitor -FDBK to OUT- DD: Differential in to differential out.

FREQUENCY (Hz)	S11 _{DD} (Mag)	S11 _{DD} (Ph)	S21 _{DD} (Mag)	S21 _{DD} (Ph)	S12 _{DD} (Mag)	S12 _{DD} (Ph)	S22 _{DD} (Mag)	S22 _{DD} (Ph)	GTU (Max)	STABILITY (k)
1.00E+05	-24.65	213.98	16.01	181.44	-18.97	1.08	-33.32	108.18	16.03	1.05
1.16E+05	-24.79	207.23	16.02	181.17	-18.89	1.05	-33.33	111.81	16.04	1.05
1.32E+05	-25.2	204.3	16.01	180.97	-18.89	1.53	-35.44	114.82	16.03	1.05
1.53E+05	-25.39	202.21	16.02	180.79	-18.74	1.31	-35.78	107.24	16.03	1.05
1.75E+05	-25.57	196.89	16	180.63	-18.97	2.09	-35.36	105.24	16.02	1.06
2.00E+05	-25.79	195.49	16.01	180.6	-18.86	1.12	-36.06	105.2	16.02	1.05
2.31E+05	-26.17	190.78	16	180.36	-18.92	1.28	-39.79	108.96	16.01	1.05
2.62E+05	-25.82	190.86	16	180.36	-18.94	0.73	-39.71	110.15	16.01	1.06
3.05E+05	-25.98	190.11	16.01	180.23	-18.85	0.79	-38.61	109.37	16.02	1.05
3.47E+05	-26.23	190.65	15.99	180.21	-18.98	0.85	-40.21	103.4	16	1.06
4.01E+05	-26.45	185.6	16	180.09	-18.84	0.86	-42.42	119.95	16.01	1.05
4.59E+05	-26.45	188.23	16	179.95	-18.91	0.84	-39.93	116.1	16.01	1.05
5.25E+05	-26.58	185.06	15.98	179.99	-18.79	-0.13	-41.67	99.54	15.99	1.05
6.06E+05	-26.29	183.94	15.98	179.93	-18.77	0.66	-46.44	115.06	15.99	1.05
6.88E+05	-26.23	181.89	15.98	179.89	-18.91	0.03	-42.61	121.63	15.99	1.06
7.99E+05	-26.37	181.41	15.98	179.92	-18.98	0.55	-43.66	121.57	15.99	1.06
9.10E+05	-26.08	180.72	15.97	179.86	-18.92	0.1	-43.9	107.29	15.98	1.06
1.05E+06	-26.42	180.43	15.96	179.75	-18.81	0.74	-44.98	111.22	15.97	1.05
1.20E+06	-26.64	182.6	15.96	179.82	-18.87	1.49	-48.41	89.98	15.97	1.06
1.38E+06	-26.64	179.74	15.96	179.8	-18.92	0.32	-45.69	70.77	15.97	1.06
1.59E+06	-26.27	180.38	15.96	179.62	-18.99	0.92	-46.98	70.78	15.97	1.06
1.80E+06	-26.84	178.66	15.94	179.67	-18.81	0.58	-46.36	39.09	15.95	1.05
2.10E+06	-27.03	179.86	15.94	179.66	-18.83	-0.31	-47.02	79.31	15.95	1.05
2.39E+06	-26.96	179.61	15.95	179.56	-18.68	0.06	-48.54	104.5	15.96	1.05
2.76E+06	-26.59	176.02	15.93	179.6	-18.82	-0.07	-45.61	39.58	15.94	1.05
3.16E+06	-27.18	175.48	15.95	179.52	-18.82	0.47	-50.75	6.16	15.95	1.05
3.62E+06	-27.27	176.96	15.93	179.52	-18.88	-1.04	-51.57	45.5	15.94	1.06
4.17E+06	-27.17	180.85	15.92	179.31	-18.78	-0.91	-47.24	56.08	15.93	1.05
4.73E+06	-27.01	177.52	15.93	179.38	-18.85	0.12	-51.03	-31.55	15.93	1.06
5.50E+06	-27.27	176.8	15.91	179.34	-18.87	0.02	-55.12	2.13	15.92	1.06
6.26E+06	-27.18	178.74	15.92	179.25	-18.75	-0.77	-63.87	-30.58	15.93	1.05
7.23E+06	-26.73	178.6	15.92	179.23	-18.89	-1.44	-50.17	-9.92	15.92	1.06
8.29E+06	-27.28	178.11	15.91	179.03	-18.78	-0.48	-51.41	12.11	15.92	1.05
9.48E+06	-27.26	179.63	15.92	179.01	-18.88	-0.56	-52.35	-41.82	15.93	1.06
1.09E+07	-27.26	179.73	15.91	178.89	-18.86	-0.95	-49.86	-24.68	15.92	1.06
1.24E+07	-27.21	180.03	15.92	178.77	-18.88	-1	-50.43	-51.11	15.92	1.06
1.44E+07	-27.13	181.01	15.91	178.58	-18.88	-1.13	-48.02	-52.74	15.92	1.06
1.64E+07	-27.37	179.77	15.91	178.43	-18.87	-1.23	-45.4	-49.5	15.92	1.06
1.90E+07	-27.4	180.64	15.91	178.21	-18.87	-1.36	-44.79	-59.22	15.91	1.06

DIFFERENTIAL S PARAMETERS

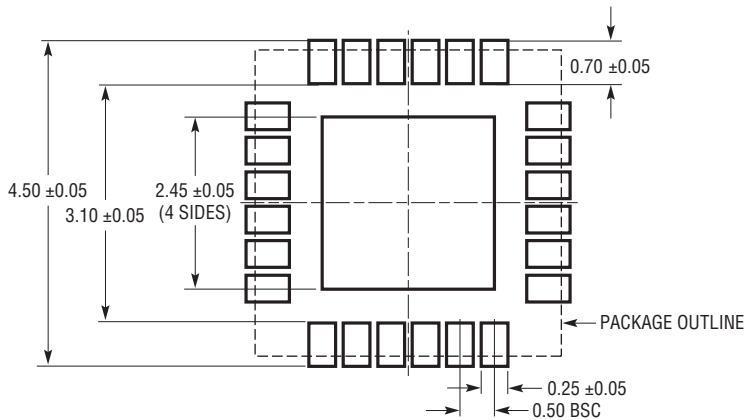
5V, $Z_{DIFF} = 100\Omega$, $T_{CASE} = 30^\circ\text{C}$, de-embedded to package pins, 1 μF capacitor +FDBK to OUT+ and 1 μF capacitor -FDBK to OUT- DD: Differential in to differential out.

FREQUENCY (MHz)	S11 _{DD} (Mag)	S11 _{DD} (Ph)	S21 _{DD} (Mag)	S21 _{DD} (Ph)	S12 _{DD} (Mag)	S12 _{DD} (Ph)	S22 _{DD} (Mag)	S22 _{DD} (Ph)	GTU (Max)	STABILITY (k)
2.17E+07	-27.32	181.3	15.9	177.93	-18.88	-1.67	-42.22	-52.54	15.91	1.06
2.49E+07	-27.12	181.43	15.9	177.69	-18.85	-1.99	-41.72	-64.62	15.91	1.06
2.87E+07	-26.96	181.05	15.9	177.36	-18.86	-2.43	-40.84	-61.81	15.91	1.06
3.26E+07	-27.24	182.44	15.89	177.04	-18.86	-2.53	-39.61	-70.18	15.9	1.06
3.78E+07	-26.86	183.1	15.89	176.6	-18.89	-3.1	-38.18	-68.88	15.9	1.06
4.31E+07	-26.76	182.65	15.9	176.13	-18.86	-3.54	-37.65	-74.32	15.91	1.06
4.98E+07	-26.62	181.26	15.89	175.61	-18.91	-3.78	-35.95	-76.76	15.9	1.06
5.70E+07	-26.75	181.06	15.89	175	-18.91	-4.63	-34.6	-83.01	15.9	1.06
6.52E+07	-26.95	182.92	15.9	174.31	-18.9	-5.13	-33.59	-87.34	15.91	1.06
7.53E+07	-26.88	179.75	15.9	173.46	-18.92	-6.03	-32.99	-86.88	15.91	1.06
8.54E+07	-26.47	180.29	15.9	172.59	-18.95	-6.61	-31.62	-89.71	15.91	1.06
9.92E+07	-26.82	179.69	15.91	171.39	-18.92	-7.57	-30.3	-97.21	15.92	1.06
1.13E+08	-26.63	178.99	15.92	170.17	-18.95	-8.7	-29.22	-95.47	15.93	1.06
1.31E+08	-26.88	176.87	15.92	168.6	-18.96	-9.88	-28.31	-100.54	15.94	1.06
1.50E+08	-26.83	177.15	15.94	166.88	-18.96	-11.16	-27.4	-104.6	15.95	1.06
1.71E+08	-27	176.62	15.95	164.91	-18.96	-13.01	-26.82	-107.66	15.97	1.06
1.97E+08	-27.59	176.01	15.96	162.38	-18.96	-14.59	-26.14	-110.04	15.97	1.06
2.24E+08	-27.5	179.18	15.96	159.78	-18.94	-16.96	-25.69	-111.52	15.98	1.05
2.60E+08	-27.45	180.64	15.93	156.29	-18.97	-19.81	-25.41	-112.18	15.95	1.06
2.96E+08	-27.43	181.86	15.88	152.81	-18.97	-22.79	-24.98	-108.99	15.9	1.06
3.42E+08	-27	182.3	15.8	148.49	-19	-26.46	-24.35	-103.45	15.82	1.06
3.92E+08	-26.74	180.54	15.7	144	-19.06	-30.32	-22.82	-96.37	15.73	1.07
4.49E+08	-26.64	178.86	15.59	139.1	-19.17	-34.98	-20.83	-92.76	15.64	1.07
5.18E+08	-27.17	178.07	15.46	133.25	-19.27	-39.99	-18.56	-92.28	15.53	1.08
5.88E+08	-27.89	179.84	15.37	127.38	-19.43	-45.32	-16.49	-94.9	15.48	1.09
6.82E+08	-28.41	192.17	15.23	119.35	-19.65	-52.66	-14.25	-100.15	15.4	1.09
7.77E+08	-27.7	208.65	15.07	111.07	-19.84	-59.66	-12.39	-106.24	15.34	1.09
8.98E+08	-24.34	220.03	14.89	100.45	-20.16	-68.72	-10.43	-114.78	15.32	1.09
1.03E+09	-20.91	217.95	14.59	89.13	-20.53	-78.35	-8.69	-124.05	15.25	1.07
1.18E+09	-17.61	208.58	14.14	75.71	-21.11	-89.5	-7.1	-134.83	15.16	1.05
1.36E+09	-14.62	192.85	13.4	59.47	-21.9	-103.24	-5.56	-148.41	14.96	1.02
1.54E+09	-12.38	175.97	12.41	45.07	-22.92	-115.67	-4.41	-161.86	14.63	1.01
1.79E+09	-10.26	150.16	11.29	29.07	-24.47	-130.06	-3.34	179.45	14.42	1.01
2.04E+09	-8.89	126.71	10.6	12.81	-25.73	-143.95	-2.83	161.69	14.4	1.02
2.36E+09	-7.68	98.74	9.25	354.9	-27.3	-157.95	-2.67	139.37	13.44	1.28
2.70E+09	-6.66	71.35	8.02	336.79	-29.27	-174.25	-2.8	116.2	12.31	1.86
3.09E+09	-5.78	43.7	7.98	310.66	-30.89	166.1	-3.19	92.85	12.16	2.35
3.56E+09	-5.28	15	5.73	281.01	-34.09	137.29	-3.99	66.89	9.47	5.21

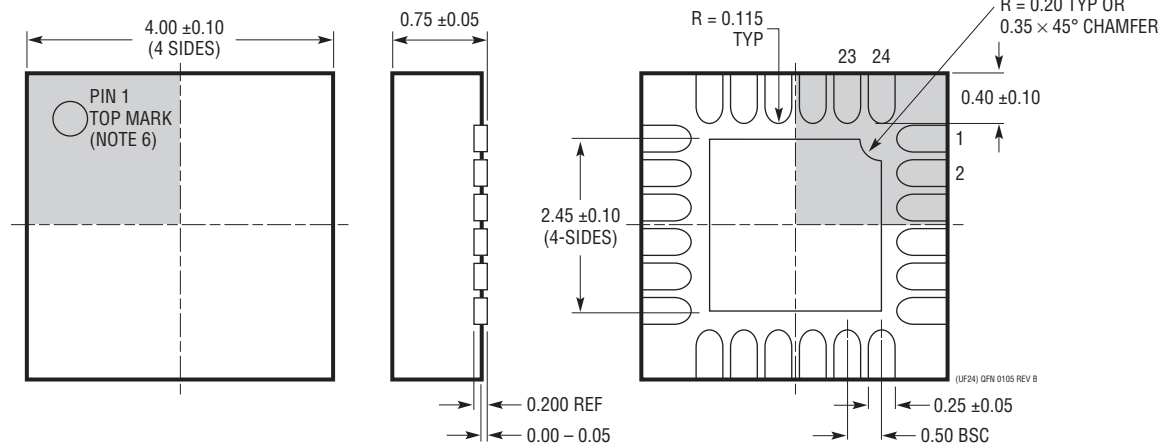
PACKAGE DESCRIPTION

Please refer to <http://www.linear.com/product/LTC6432-15#packaging> for the most recent package drawings.

UF Package
24-Lead Plastic QFN (4mm × 4mm)
 (Reference LTC DWG # 05-08-1697 Rev B)



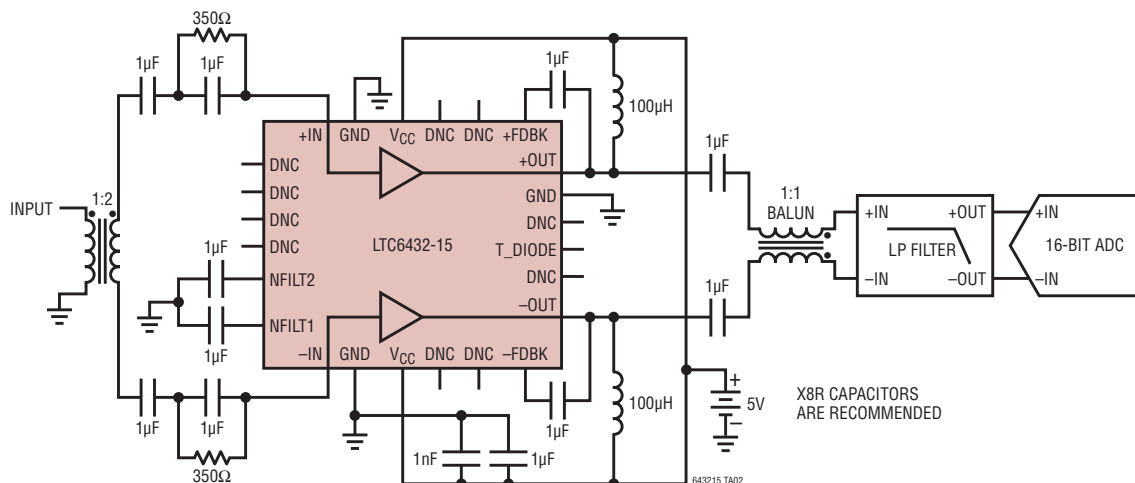
RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS



NOTE:

1. DRAWING PROPOSED TO BE MADE A JEDEC PACKAGE OUTLINE MO-220 VARIATION (WGGD-X)—TO BE APPROVED
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE
MOLD FLASH, MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE, IF PRESENT
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION
ON THE TOP AND BOTTOM OF PACKAGE

TYPICAL APPLICATION



RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
Fixed Gain IF Amplifiers/ADC Drivers		
LTC6430-20	100Ω Differential 20dB Gain Block IF Amplifier	20MHz to 2GHz 2.9dB NF 20.8dB Gain, 51dBm OIP3 at 240MHz into a 100Ω Differential Load
LTC6431-20	50Ω 20dB Gain Block IF Amplifier	Single-Ended Version of LTC6430-20, 20.8dB Gain, 46.2dBm OIP3 at 240MHz into a 50Ω Load
LTC6431-15	50Ω 15dB Gain Block IF Amplifier	Single-Ended Version of LTC6430-15, 15.5dB Gain, 47dBm OIP3 at 240MHz into a 50Ω Load
LTC6430-15	100Ω Differential 15dB Gain Block IF Amplifier	20MHz to 2GHz 3.3dB NF 15.5dB Gain, 50dBm OIP3 at 240MHz into a 100Ω Differential Load
LTC6417	1.6GHz Low Noise High Linearity Differential Buffer/ADC Driver	OIP3 = 41dBm at 300MHz, Can Drive 50Ω Differential Output High Speed Voltage Clamping Protects Subsequent Circuitry
LTC6400-8/LTC6400-14/LTC6400-20/LTC6400-26	1.8GHz Low Noise, Low Distortion Differential ADC Drivers	-71dBc IM3 at 240MHz 2V _{P-P} Composite, I _S = 90mA, A _V = 8dB, 14dB, 20dB, 26dB
LTC6401-8/LTC6401-14/LTC6401-20/LTC6401-26	1.3GHz Low Noise, Low Distortion Differential ADC Drivers	-74dBc IM3 at 140MHz 2V _{P-P} Composite, I _S = 50mA, A _V = 8dB, 14dB, 20dB, 26dB
LTC6433-15	50Ω, 15dB Low Frequency Gain Block	OIP3 = 52dBm at 1MHz, Single-Ended Version of LTC6432-15
Variable Gain IF Amplifiers/ADC Drivers		
LTC6412	800MHz, 31dB Range Analog-Controlled VGA	OIP3 = 35dBm at 240MHz, Continuously Adjustable Gain Control
Baseband Differential Amplifiers		
LTC6409	1.1nV/√Hz Single Supply Differential Amplifier/ADC Driver	88dB SFDR at 100MHz, AC- or DC-Coupled Inputs
LTC6419	3GHz Rail-to-Rail Input Differential Amplifier/ ADC Driver	-65dBc IM3 at 50MHz 2V _{P-P} Composite, Rail-to-Rail Inputs, eN = 1.6nV/√Hz, 18mA
High Speed ADCs		
LTC2208/LTC2209	16-Bit, 13Msps/160Msps ADC	74dBFS Noise Floor, SFDR > 89dB at 140MHz, 2.25V _{P-P} Input
LTC2259-16	16-Bit, 80Msps ADC, Ultralow Power	72dBFS Noise Floor, SFDR > 82dB at 140MHz, 2.00V _{P-P} Input
LTC2160/LTC2161	16-bit, 25Msps/40Msps/60Msps ADC Low Power	76.2 dBFS Noise Floor, SFDR > 84dB at 140MHz, 2.00V _{P-P} Input
LTC2155-14/LTC2156-14/LTC2157-14/LTC2158-14	14-bit, 170Msps/210Msps/250Msps/310Msps ADC 2-Channel	69dBFS Noise Floor, SFDR > 80dB at 140MHz, 1.50V _{P-P} Input, >1GHz Input BW
LTC2216	16-Bit, 80Msps ADC	79dBFS Noise Floor, SFDR > 91dB at 140MHz, 75V _{P-P} Input

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Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;
- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



JONHON

«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели,
кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



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