

### DESCRIPTION

The MP6924A is a dual, fast turn-off, intelligent rectifier for synchronous rectification in LLC resonant converters.

The IC drives two N-channel MOSFETs, regulates their forward voltage drop to  $V_{fwd}$  (about 29mV), and turns the MOSFETs off before the switching current goes negative.

The MP6924A has a light-load function to latch off the gate driver under light-load conditions, limiting the current to 175µA.

The MP6924A's fast turn-off enables both continuous conduction mode (CCM) and discontinuous conduction mode (DCM).

The MP6924A requires a minimal number of readily available, standard, external components and is available in a SOIC-8 package.

### FEATURES

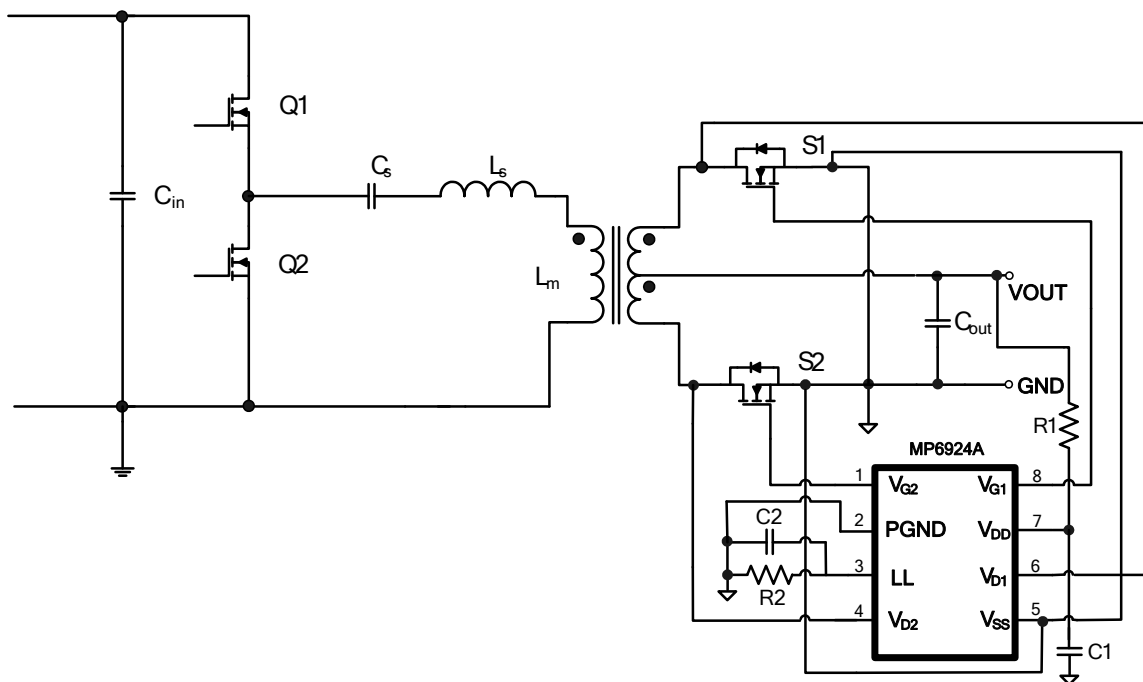
- Works with Standard and Logic Level MOSFETs
- Compatible with Energy Star
- Fast Turn-Off Total Delay of 35ns
- Wide 4.2V ~ 35V  $V_{DD}$  Operating Range
- 175µA Low Quiescent Current in Light-Load Mode
- Supports CCM, CrCM, and DCM Operation
- Supports High-Side and Low-Side Rectification
- Available in a SOIC-8 Package

### APPLICATIONS

- AC/DC Adapters
- PC Power Supplies
- LCD and LED TVs
- Isolated DC/DC Power Converters

All MPS parts are lead-free, halogen-free, and adhere to the RoHS directive. For MPS green status, please visit the MPS website under Quality Assurance. "MPS" and "The Future of Analog IC Technology" are registered trademarks of Monolithic Power Systems, Inc.

### TYPICAL APPLICATION



## ORDERING INFORMATION

Part Number*	Package	Top Marketing
MP6924AGS	SOIC-8	See Below

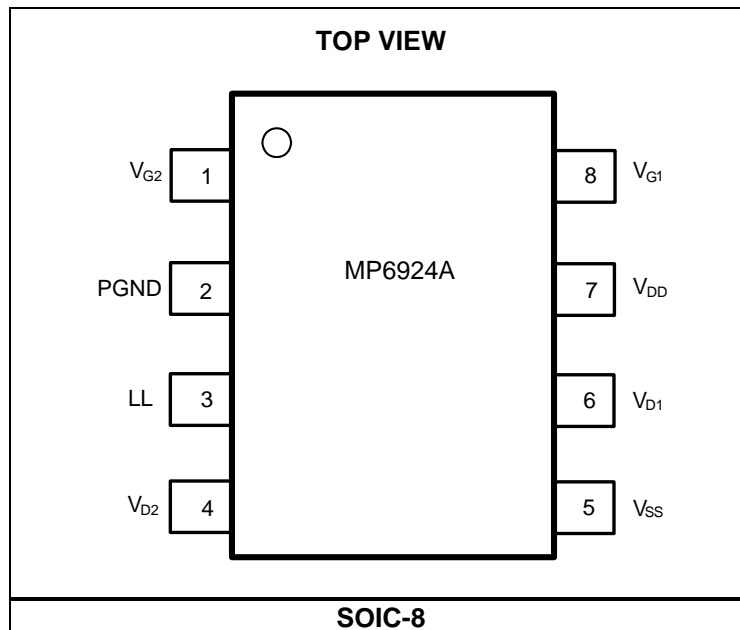
\* For Tape & Reel, add suffix -Z (e.g. MP6924AGS-Z)

## TOP MARKING

**MP6924A**  
**LLLLLLLLL**  
**MPSYWW**

MP6924A: Part number  
 LLLLLLLL: Lot number  
 MPS: MPS prefix  
 Y: Year code  
 WW: Week code

## PACKAGE REFERENCE



**ABSOLUTE MAXIMUM RATINGS (1)**

V <sub>DD</sub> to V <sub>SS</sub> .....	-0.3V to +38V
PGND to V <sub>SS</sub> .....	-0.3V to +0.3V
V <sub>G</sub> to V <sub>SS</sub> .....	-0.3V to +20V
V <sub>D</sub> to V <sub>SS</sub> .....	-1V to +180V
LL to V <sub>SS</sub> .....	-0.3V to +6.5V
Continuous power dissipation (T <sub>A</sub> = +25°C) (2)	
SOIC-8.....	1.4W
Junction temperature.....	150°C
Lead temperature (solder).....	260°C
Storage temperature.....	-55°C to +150°C

**Recommended Operation Conditions (3)**

V <sub>DD</sub> to V <sub>SS</sub> .....	4.2V to 35V
Operating junction temp. (T <sub>J</sub> )...	-40°C to +125°C

<b>Thermal Resistance (4)</b>	<b>θ<sub>JA</sub></b>	<b>θ<sub>JC</sub></b>	
SOIC-8.....	90.....	45...	°C/W

**NOTES:**

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature T<sub>J</sub>(MAX), the junction-to-ambient thermal resistance θ<sub>JA</sub>, and the ambient temperature T<sub>A</sub>. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P<sub>D</sub>(MAX)=(T<sub>J</sub>(MAX)-T<sub>A</sub>)/θ<sub>JA</sub>. Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.

## ELECTRICAL CHARACTERISTICS

$V_{DD} = 12V$ ,  $-40^{\circ}C \leq T_J \leq +125^{\circ}C$ , unless otherwise noted.

Parameter	Symbol	Conditions	Min	Typ	Max	Units
$V_{DD}$ voltage range			4.2		35	V
$V_{DD}$ UVLO rising			3.7	3.95	4.2	V
$V_{DD}$ UVLO hysteresis			0.13	0.185	0.24	V
Operating current	$I_{CC}$	$C_{LOAD} = 4.7nF$ , $F_{SW} = 100kHz$		16	20	mA
Quiescent current	$I_Q$	$V_{SS} - V_D = 0.5V$		4.6	6	mA
Shutdown current		$V_{DD} = 4V$ , $LL = 0V$		135	190	$\mu A$
		$V_{DD} = 20V$ , $LL = 0V$		155	210	
Light-load mode current				175	225	$\mu A$
Thermal shutdown <sup>(5)</sup>				175		$^{\circ}C$
Thermal shutdown hysteresis <sup>(5)</sup>				10		$^{\circ}C$
<b>Control Circuitry Section</b>						
$V_{SS} - V_D$ forward voltage	$V_{fwd}$		17	29	41	mV
Turn-off threshold ( $V_{SS} - V_D$ )				0		mV
Turn-on delay	$t_{Don}$	$C_{LOAD} = 4.7nF$ , $V_{GS} = 2V$		190	300	ns
	$t_{Don}$	$C_{LOAD} = 10nF$ , $V_{GS} = 2V$		270	410	
Input bias current on $V_D$		$V_D = 180V$			1	$\mu A$
Turn-on blanking time	$t_{B\_ON}$	$C_{LOAD} = 4.7nF$	0.75	1.1	1.65	$\mu s$
Turn-off blanking time <sup>(5)</sup>	$t_{B\_OFF}$	$C_{LOAD} = 4.7nF$		1750		ns
Light-load enter pulse width	$T_{LL}$	$R_{LL} = 100k\Omega$	1.7	2.3	3	$\mu s$
Light-load turn-on pulse width hysteresis	$T_{LL-H}$	$R_{LL} = 100k\Omega$		0.45		$\mu s$
Light-load enter delay	$T_{LL-D}$		45	78	121	$\mu s$
Gate disable threshold on LL	$V_{LL\_DIS}$		0.1	0.2	0.3	V
Turn-on threshold ( $V_{DS}$ )	$V_{LL\_DS}$	$V_{DD} = 12V$	-330	-230	-130	mV
<b>Gate Driver Section</b>						
$V_G$ (low)	$V_{G\_L}$	$I_{LOAD} = 1mA$			0.1	V
$V_G$ (high)	$V_{G\_H}$	$V_{DD} > 10V$		11.5	13	V
		$V_{DD} \leq 10V$		$V_{DD}$		
Turn-off propagation delay		$V_D = V_{SS}$		15		ns
Turn-off total delay	$t_{Doff}$	$V_D = V_{SS}$ , $C_{LOAD} = 4.7nF$ , $R_{GATE} = 0\Omega$ , $V_{GS} = 2V$		35	80	ns
	$t_{Doff}$	$V_D = V_{SS}$ , $C_{LOAD} = 10nF$ , $R_{GATE} = 0\Omega$ , $V_{GS} = 2V$		45	100	
Pull-down impedance				0.6	1.5	$\Omega$

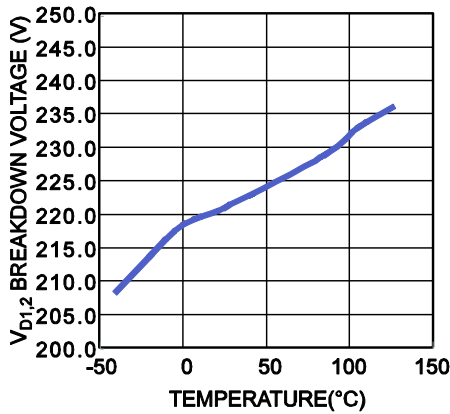
**NOTE:**

5) Guaranteed by characterization.

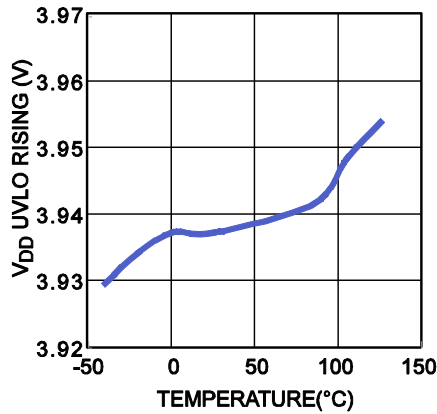
## TYPICAL PERFORMANCE CHARACTERISTICS

$V_{DD} = 12V$ , unless otherwise noted.

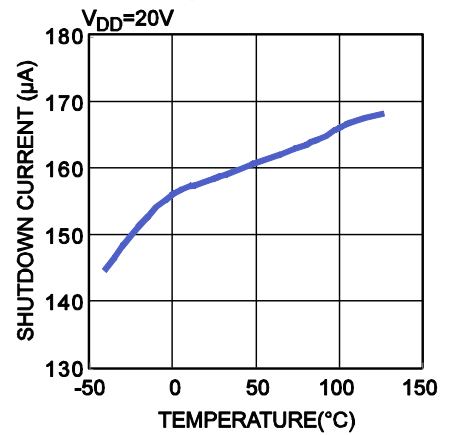
**$V_{D1,2}$  Breakdown Voltage vs. Temperature**



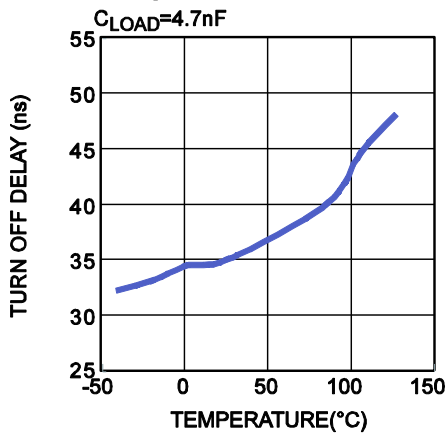
**$V_{DD}$  UVLO Rising vs. Temperature**



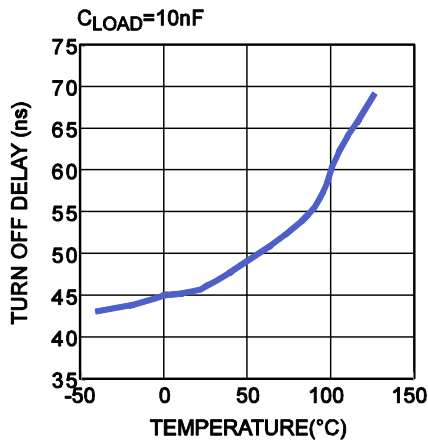
**Shutdown Current vs. Temperature**



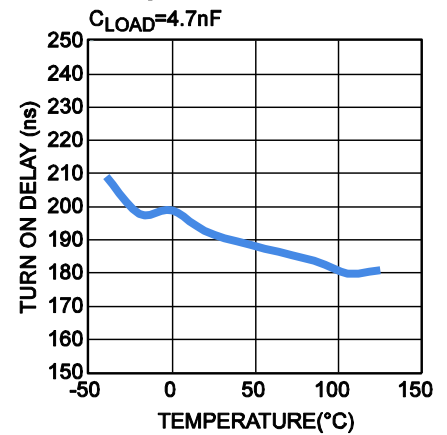
**Turn-Off Delay vs. Temperature**



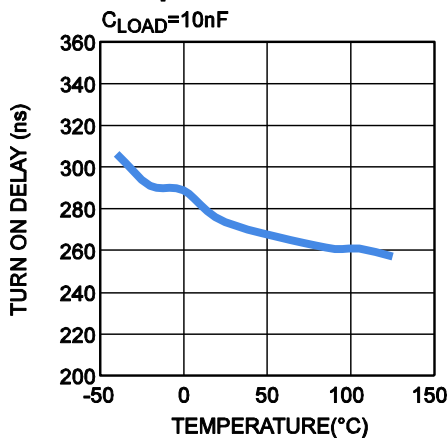
**Turn-Off Delay vs. Temperature**



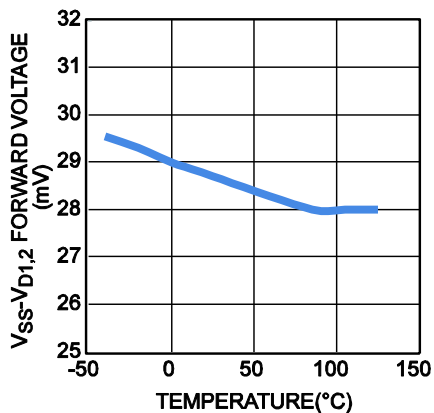
**Turn-On Delay vs. Temperature**



**Turn-On Delay vs. Temperature**



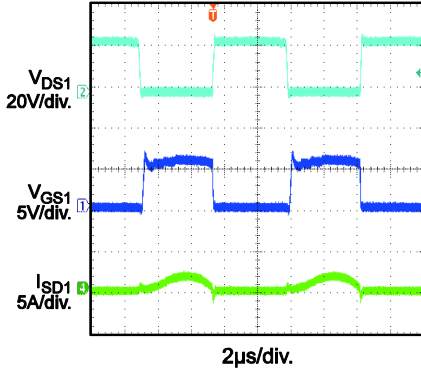
**$V_{SS}-V_{D1,2}$  Forward Voltage vs. Temperature**



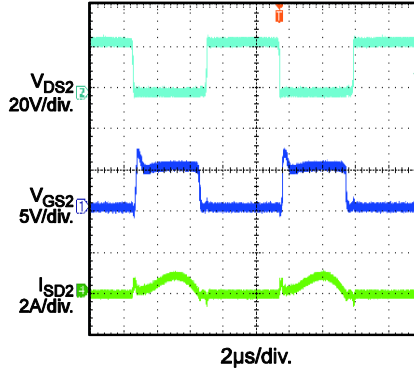
**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**

$V_{DD} = 12V$ , unless otherwise noted.

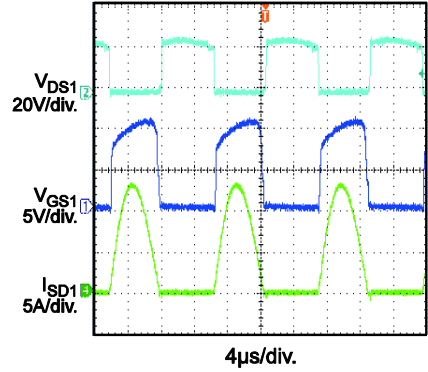
**Operation in 90W LLC Converter**  
 $V_{IN}=240VAC, V_{OUT}=12V, I_{OUT}=0.75A$



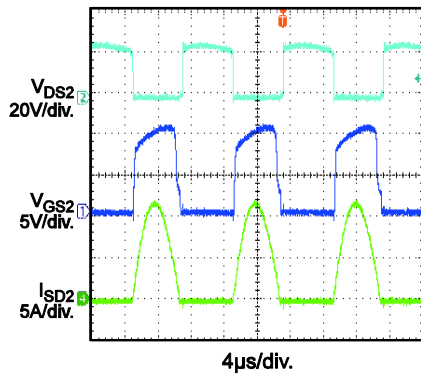
**Operation in 90W LLC Converter**  
 $V_{IN}=240VAC, V_{OUT}=12V, I_{OUT}=0.75A$



**Operation in 90W LLC Converter**  
 $V_{IN}=240VAC, V_{OUT}=12V, I_{OUT}=7.5A$



**Operation in 90W LLC Converter**  
 $V_{IN}=240VAC, V_{OUT}=12V, I_{OUT}=7.5A$



## PIN FUNCTIONS

Pin # (SOIC-8)	Name	Description
1	V <sub>G2</sub>	<b>MOSFET 2 gate driver output.</b>
2	PGND	<b>Power ground.</b> PGND is the power switch return.
3	LL	<b>Light-load timing setting.</b> Connect a resistor to LL to set the light-load timing. Leave LL open to prevent the IC from entering light-load mode. Pull LL low to disable the gate driver.
4	V <sub>D2</sub>	<b>MOSFET 2 drain voltage sense.</b>
5	V <sub>SS</sub>	<b>Source pin used as reference for V<sub>D1</sub> and V<sub>D2</sub>.</b>
6	V <sub>D1</sub>	<b>MOSFET 1 drain voltage sense.</b>
7	V <sub>DD</sub>	<b>Supply voltage.</b>
8	V <sub>G1</sub>	<b>MOSFET 1 gate driver output.</b>

## BLOCK DIAGRAM

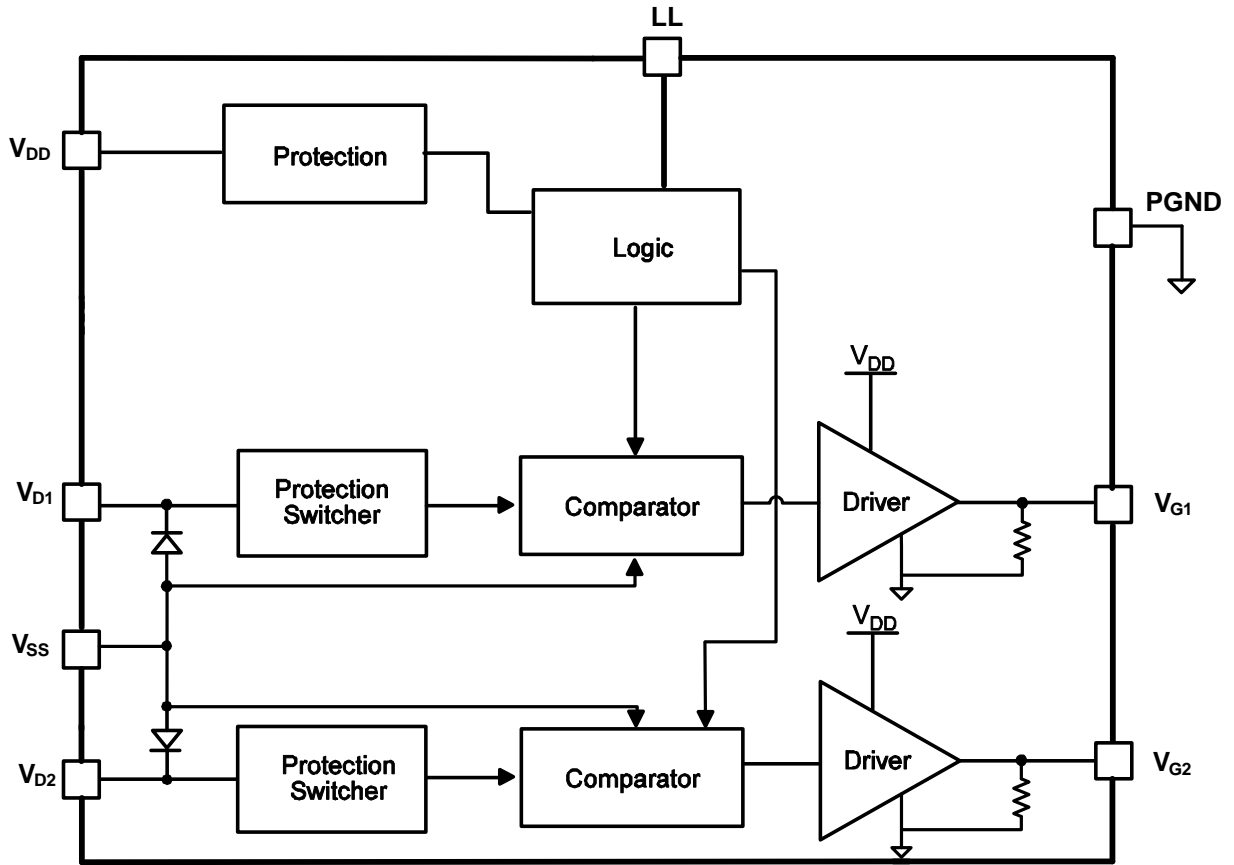


Figure 1: Functional Block Diagram



## OPERATION

The MP6924A operates in discontinuous conduction mode (DCM), continuous conduction mode (CCM), and critical conduction mode (CrCM). When the MP6924A operates in either DCM or CrCM, the control circuitry controls the gate in forward mode. The gate turns off when the MOSFET current is low. In CCM, the control circuitry turns off the gate during very fast transients.

### VD Clamp

Because  $V_{D1,2}$  can rise as high as 180V, a high-voltage JFET is used at the input. To prevent excessive currents when  $V_{DS1,2}$  drops below -0.7V, a 1kΩ resistor is recommended between  $V_{D1,2}$  and the drain of the external MOSFET.

### Under-Voltage Lockout (UVLO)

When  $V_{DD}$  is below the  $V_{DD}$  UVLO threshold, the MP6924A falls into sleep mode, and  $V_{G1,2}$  remains at a low level.

### Enable

If LL is pulled low, the MP6924A is in shutdown mode, which consumes 175μA of shutdown current. If LL is pulled high during the rectification cycle, the gate driver does not appear until the next rectification cycle begins (see Figure 2).

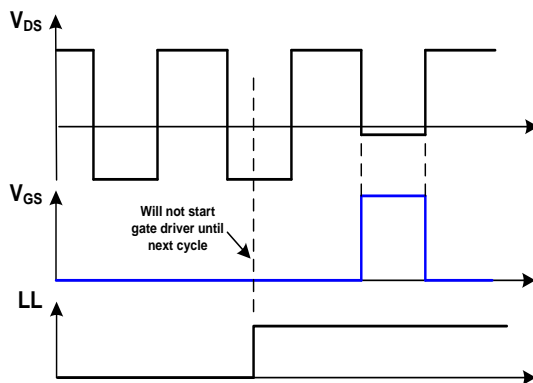


Figure 2: LL Control Scheme

### Thermal Shutdown

If the junction temperature of the chip exceeds the thermal shutdown threshold,  $V_{G1,2}$  is pulled low, and the MP6924A stops switching. The IC resumes normal function after the junction temperature drops 10°C.

### Turn-On Phase

When the switch current flows through the body diode of the MOSFET, there is a negative voltage drop ( $V_D - V_{SS}$ ) across the body diode.  $V_{DS}$  is much lower than the turn-on threshold of the control circuitry ( $V_{LL-DS}$ ), which triggers a charge current to turn on the MOSFET (see Figure 3).

### Turn-On Blanking

The control circuitry contains a blanking function that ensures that when the MOSFET turns on or off, it remains in that state for  $t_{B\_ON}$  (~1.1μs), which determines the minimum on time. During the turn-on blanking period, the turn-off threshold is not blanked completely, but changes to about +100mV (instead of 0mV). This ensures that the part can always turn off, even during the turn-on blanking period, although it does so slower. Avoid setting the synchronous period below  $t_{B\_ON}$  in CCM in the LLC converter to eliminate shoot-through.

### Conduction Phase

When  $V_{DS}$  rises above the forward voltage drop ( $-V_{fwd}$ ) according to the decrease of the switching current, the MP6924A pulls down the gate voltage level to make the on resistance of the synchronous MOSFET larger to ease the rise of  $V_{DS}$ .

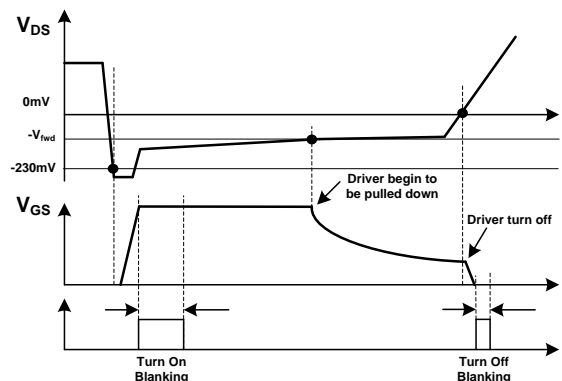


Figure 3: Turn-On/Off Timing Diagram

The control scheme in Figure 3 shows  $V_{DS}$  adjusted to be around  $-V_{fwd}$ , even when the current through the MOSFET is fairly low. This function puts the driver voltage at a very low level when the synchronous MOSFET is turning off, which boosts the turn-off speed.

**Turn-Off Phase**

When  $V_{DS}$  rises to trigger the turn-off threshold, the gate voltage is pulled to zero after a very short turn-off delay (see Figure 3).

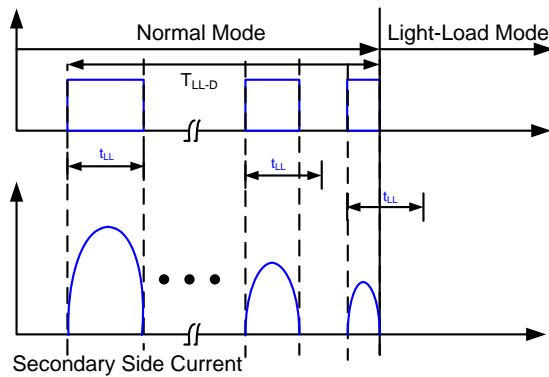
**Turn-Off Blanking**

After the gate driver is pulled to zero by  $V_{DS}$  reaching the turn-off threshold, turn-off blanking is triggered to ensure that the gate driver is off for at least  $t_{B\_ON}$  to prevent an erroneous trigger on  $V_{DS}$ .

**Light-Load Latch-Off Function**

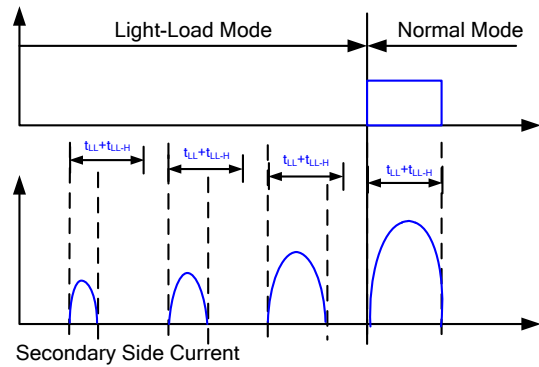
The gate driver of the MP6924A is latched off to save driver loss in light-load condition and improve efficiency.

When the MOSFET’s switching cycle conducting period falls below  $T_{LL}$ , the MP6924A enters light-load mode and latches off the MOSFET after a light-load enter delay ( $T_{LL-D}$ ) (see Figure 4).



**Figure 4: MP6924A Entering Light-Load Mode**

During light-load mode, the MP6924A monitors the body diode conduction time. If this time exceeds  $T_{LL} + T_{LL-H}$ , the IC exits light-load mode and initiates the gate driver in the next new switching cycle (see Figure 5 and Figure 6).

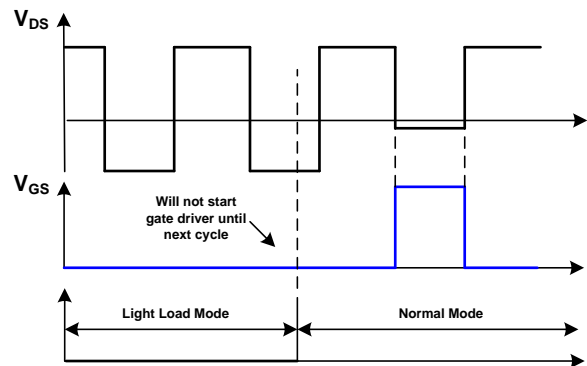


**Figure 5: MP6924A Exiting Light-Load Mode**

Light-load enter timing ( $T_{LL}$ ) is programmable by connecting a resistor ( $R_{LL}$ ) to LL. By monitoring the LL current (the LL voltage is kept at  $\sim 2V$  internally),  $T_{LL}$  can be calculated with Equation (1):

$$T_{LL} = R_{LL} (k\Omega) \cdot \frac{2.3\mu s}{100k\Omega} \quad (1)$$

If the light-load mode of the MP6924A ends during the rectification cycle, the gate driver signal does not appear until the next rectification cycle begins (see Figure 6).



**Figure 6: Gate Driver Starting after Exiting Light-Load Mode**

## APPLICATION INFORMATION

### Layout Considerations

Listed below are the main recommendations that should be taken into consideration when designing the PCB.

#### Sensing for $V_D/V_S$

1. Keep the sensing connections ( $V_{D1}/V_{SS}$ ,  $V_{D2}/V_{SS}$ ) as close to each of the MOSFETs (drain/source) as possible.
2. Keep the two channels' sensing loops separated from each other.
3. Make the sensing loop as small as possible (see Figure 7).

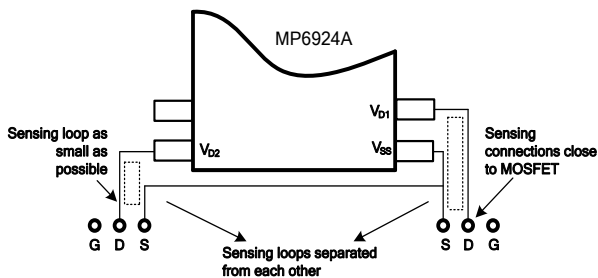


Figure 7: Sensing for  $V_D/V_S$

Figure 8 shows a layout example of the MP6924A driving PowerPAK SO8 package MOSFETs with two, separate, small sensing loops.

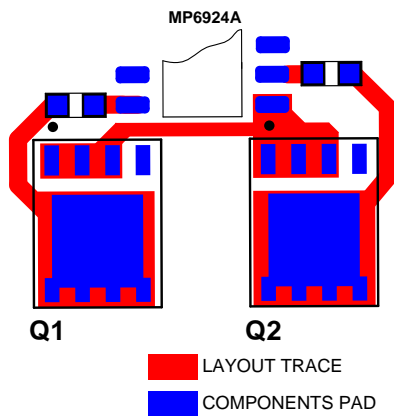


Figure 8: Layout Example for Sensing Loop and  $V_{DD}$  Decoupling

#### $V_{DD}$ Decoupling Capacitor

1. Place a decoupling capacitor no smaller than  $1\mu\text{F}$  from  $V_{DD}$  to PGND close to the IC for adequate filtering (see Figure 9).

#### System Power Loop

1. Keep the two channels' power loops separated from each other (see Figure 9).  
*This minimizes the interaction between the two channels' power loops, which may affect the voltage sensing of the IC.*
2. Make the power loop as small as possible to reduce parasitic inductance.

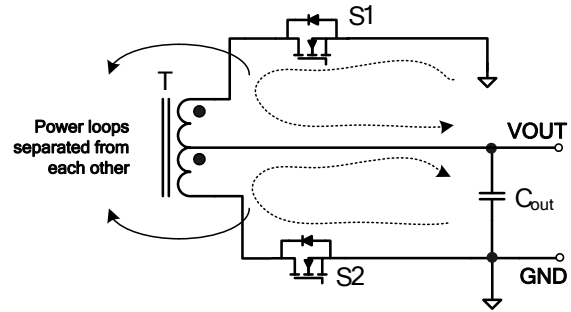


Figure 9: System Power Loop

Figure 10 shows a layout example of the power loop trace, which has a minimized loop length. The two channel power traces do not cross each other.

It is highly recommended to place the driver's sensing loop trace away from the power loop trace (see Figure 10). The sensing loop trace and power loop trace can be placed on different layers to keep them separate from each other.

Do not place the driver IC inside the power loop. This may affect MOSFET voltage sensing.

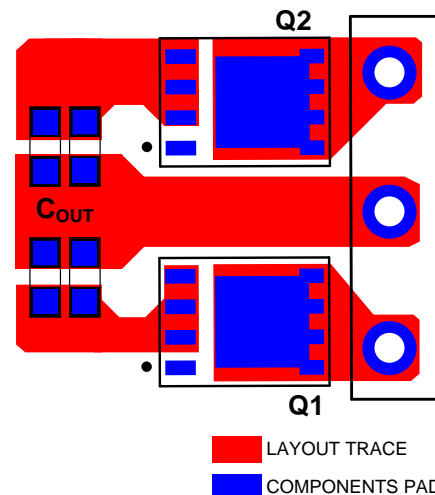


Figure 10: Layout Example for System Power Loop

**SR MOSFET Selection and Driver Ability**

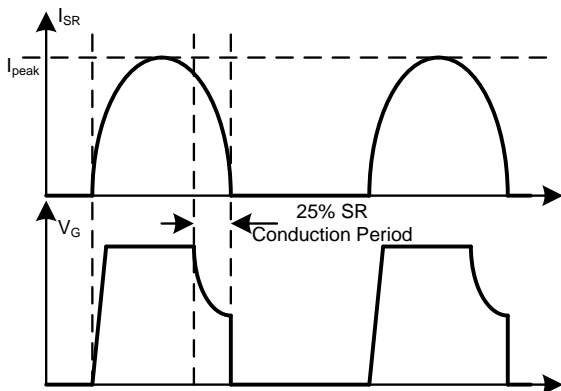
Power MOSFET selection is a trade-off between the  $R_{DS(ON)}$  and  $Q_g$ . To achieve high efficiency, a MOSFET with a smaller  $R_{DS(ON)}$  is recommended. A larger  $Q_g$  with a smaller  $R_{DS(ON)}$  makes the turn-on/-off speed lower and the power loss larger. For the MP6924A,  $V_{DS}$  is adjusted at  $V_{fwd}$  during the driving period. A MOSFET with a small  $R_{DS(ON)}$  is not recommended because the gate driver may be kept at a fairly low level with a small  $R_{DS(ON)}$ , even when the system load is high, which makes the advantage of the low  $R_{DS(ON)}$  inconspicuous.

Figure 11 shows the typical waveform of the LLC on the secondary side. To achieve a fairly high usage of the MOSFET’s  $R_{DS(ON)}$ , it is expected that the MOSFET driver voltage is kept at the maximum level until the last 25% of the SR conduction period. Calculate  $V_{DS}$  with Equation (2):

$$V_{DS} = -R_{ds(ON)} \cdot \frac{\sqrt{2}}{2} \cdot I_{peak} = -R_{ds(ON)} \cdot I_{OUT} = -V_{fwd} \quad (2)$$

Where  $V_{DS}$  is drain-source voltage of the MOSFET.

The MOSFET’s  $R_{DS(ON)}$  is recommended to be no lower than  $\sim V_{fwd}/I_{OUT}$  (mΩ). For example, in a 10A application with  $V_{fwd}$  at 29mV, the  $R_{DS(ON)}$  of the MOSFET is recommended to be no lower than 2.9mΩ.

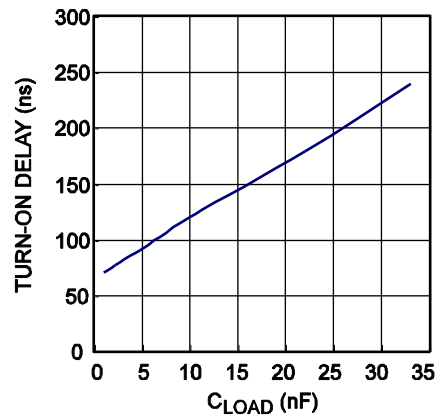


**Figure 11: Synchronous Rectification Typical Waveform in LLC**

$Q_g$  of the MOSFET affects the turn-on and turn-off delay. Figure 12 shows the turn-on delay ( $t_{Don}$ ) and the turn-off delay ( $t_{Doff}$ ).  $t_{Don}$  indicates how long the body diode conducts before the MOSFET turns on, while  $t_{Doff}$  indicates how long the driver takes to turn off the MOSFET. With a higher turn-on delay, the body diode conduction duration of the MOSFET is longer, which brings down the total efficiency. However, with a higher turn-off delay, the shoot-through risk is higher in CCM operation.

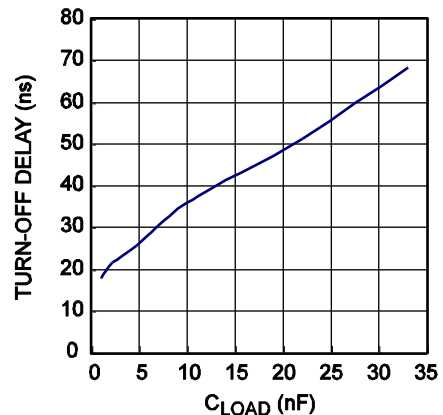
Figure 12 and Figure 13 show the  $t_{Don}$  and  $t_{Doff}$  of the MP6924A according to different  $C_{load}$  values.

**Turn-On Delay vs. C\_LOAD**

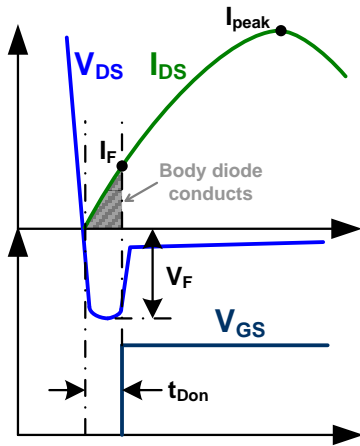


**Figure 12: Turn-On Delay vs. C<sub>load</sub>**

**Turn-Off Delay vs. C\_LOAD**



**Figure 13: Turn-Off Delay vs. C<sub>load</sub>**



**Figure 14: Turn-On Delay Effect on Efficiency**

Figure 14 shows how  $t_{Don}$  affects system efficiency. During  $t_{Don}$ , the body diode of the SR MOSFET conducts, which leads to a power loss that can be calculated with Equation (3):

$$P_{on} \approx \frac{V_F \cdot I_F}{2} \cdot 2f_s \cdot t_{Don} = V_F \cdot I_F \cdot f_s \cdot t_{Don} \quad (3)$$

Where  $V_F$  is the body diode forward voltage drop,  $I_F$  is the switching current when the turn-on delay ( $t_{Don}$ ) has ended, and  $f_s$  is the switching frequency.

When considering the switching current as a complete sine wave,  $I_F$  can be estimated with Equation (4) and Equation (5):

$$I_F = I_{peak} \cdot \sin(2 \cdot f_s \cdot t_{Don} \cdot \pi) \quad (4)$$

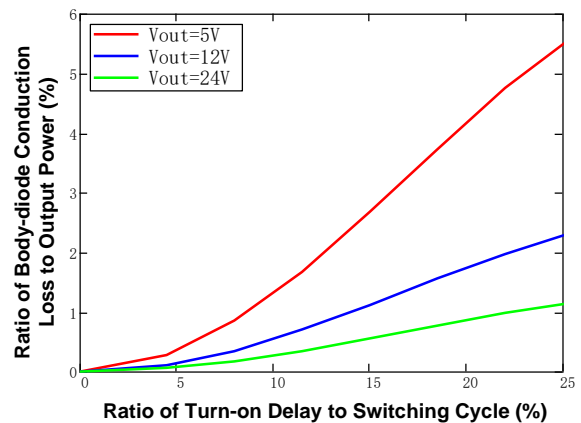
$$I_{peak} \approx \frac{\pi}{2} \cdot I_{out} \quad (5)$$

Where  $I_{peak}$  is the peak switching current through the MOSFET, and  $I_{out}$  is the system output current.

When plugging the values from Equation (4) and Equation (5) into Equation (3), the turn-on delay power loss through the SR MOSFET's body diode can be derived with Equation (6):

$$P_{on} = \frac{\pi}{2} \cdot I_{out} \cdot V_F \cdot f_s \cdot t_{Don} \cdot \sin(2 \cdot f_s \cdot t_{Don} \cdot \pi) \quad (6)$$

Figure 15 shows how different turn-on delay values affect efficiency according to different output voltages. To keep the body diode conduction loss at a fairly low level (below 0.5% of the output power), the turn-on delay is recommended to be less than 5% of the switching cycle. For example, in a  $f_{sw} = 200\text{kHz}$  LLC system, the switching cycle is  $\sim 5\mu\text{s}$ . It is recommended to select a MOSFET that makes  $t_{Don} < 250\text{ns}$ .

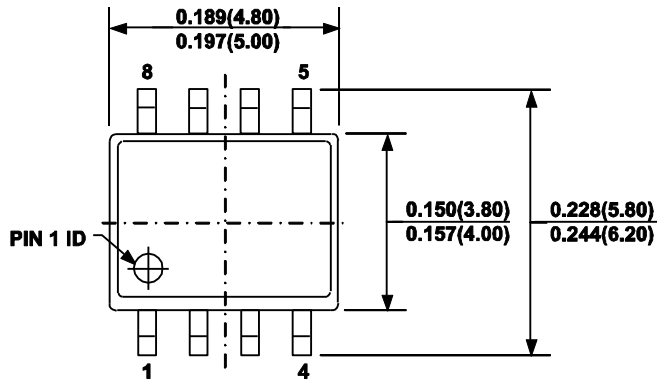


**Figure 15: Turn-On Delay vs. Power Loss**

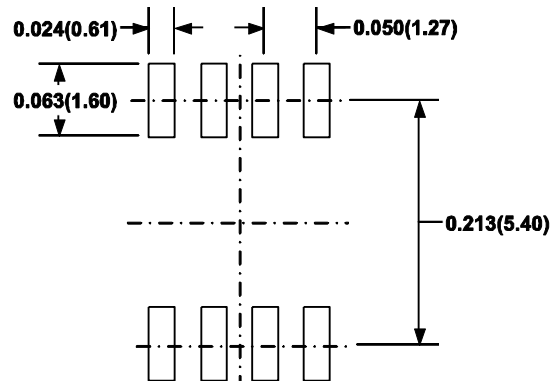
The turn-off delay ( $t_{Doff}$ ) is critical in some fast transient CCM applications. Choose the MOSFET to make  $t_{Doff}$  below the CCM current transient duration. Otherwise, the MOSFET may need to be selected with a lower  $Q_g$ , or an external totem pole driver circuit may be added to prevent shoot-through.

**PACKAGE INFORMATION**

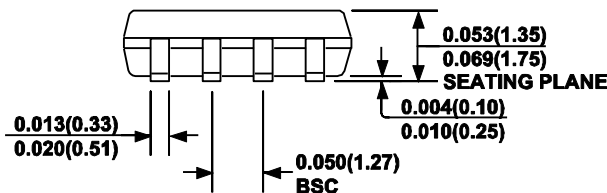
**SOIC-8**



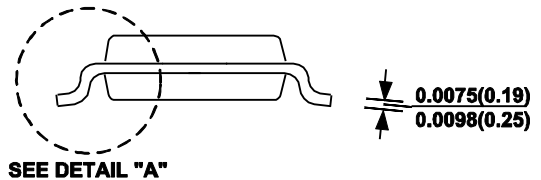
**TOP VIEW**



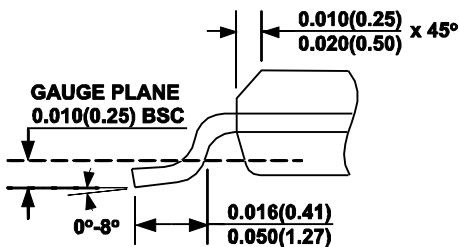
**RECOMMENDED LAND PATTERN**



**FRONT VIEW**



**SIDE VIEW**



**DETAIL "A"**

**NOTE:**

- 1) CONTROL DIMENSION IS IN INCHES. DIMENSION IN BRACKET IS IN MILLIMETERS.
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
- 4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.004" INCHES MAX.
- 5) DRAWING CONFORMS TO JEDEC MS-012, VARIATION AA.
- 6) DRAWING IS NOT TO SCALE.

**NOTICE:** The information in this document is subject to change without notice. Users should warrant and guarantee that third party Intellectual Property rights are not infringed upon when integrating MPS products into any application. MPS will not assume any legal responsibility for any said applications.

Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;
- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



## JONHON

«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



Телефон: 8 (812) 309-75-97 (многоканальный)

Факс: 8 (812) 320-03-32

Электронная почта: [ocean@oceanchips.ru](mailto:ocean@oceanchips.ru)

Web: <http://oceanchips.ru/>

Адрес: 198099, г. Санкт-Петербург, ул. Калинина, д. 2, корп. 4, лит. А