



www.ti.com

125 W STEREO DIGITAL AMPLIFIER POWER STAGE

FEATURES

- Total Power Output (Bridge Tied Load)
 - 2 × 125 W at 10% THD+N Into 4 Ω
 - 2 × 100 W at 10% THD+N Into 6 Ω
- Total Power Output (Single Ended)
 - 4 × 45 W at 10% THD+N Into 3 Ω
 - 4 × 35 W at 10% THD+N Into 4 Ω
- Total Power Output (Parallel Mode)
 - 1 × 250 W at 10% THD+N Into 2 Ω
 - 1 × 195 W at 10% THD+N Into 3 Ω
- >110 dB SNR (A-Weighted With TAS5518 Modulator)
- <0.1% THD+N (1 W, 1 kHz)
- Supports PWM Frame Rates of 192 kHz to 432 kHz
- Resistor-Programmable Current Limit
- Integrated Self-Protection Circuitry, Including:
 - Under Voltage Protection
 - Overtemperature Warning and Error
 - Overload Protection
 - Short-Circuit Protection
 - PWM Activity Detector
- Standalone Protection Recovery
- Power-On Reset (POR) to Eliminate System Power-Supply Sequencing
- High-Efficiency Power Stage (>90%) With 80-mΩ Output MOSFETs
- Thermally Enhanced 44-Pin HTSSOP Package (DDV)
- Error Reporting, 3.3-V and 5.0-V Compliant
- EMI Compliant When Used With Recommended System Design

APPLICATIONS

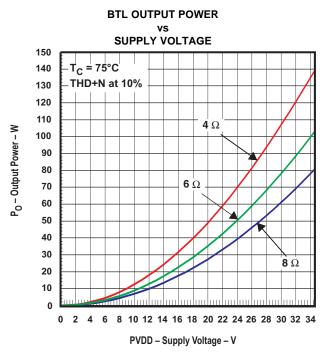
- Mini/Micro Audio System
- DVD Receiver
- Home Theater

DESCRIPTION

The TAS5352A is a high-performance, integrated stereo digital amplifier power stage designed to drive a 4- Ω bridge-tied load (BTL) at up to 125 W per channel with low harmonic distortion, low integrated noise, and low idle current.

The TAS5352A has a complete protection system integrated on-chip, safeguarding the device against a wide range of fault conditions that could damage the system. These protection features are short-circuit protection, over-current protection, under voltage protection, over temperature protection, and a loss of PWM signal (PWM activity detector).

A power-on-reset (POR) circuit is used to eliminate power-supply sequencing that is required for most power-stage designs.



A

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

PurePath Digital, PowerPad are trademarks of Texas Instruments. All other trademarks are the property of their respective owners.

TAS5352A

SLES239-NOVEMBER 2008



www.ti.com



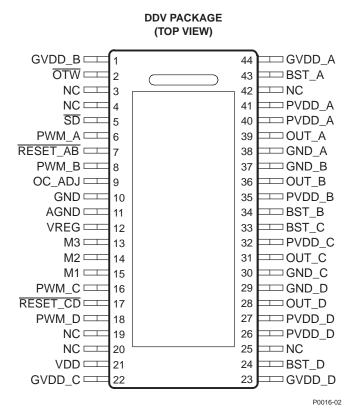
These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

GENERAL INFORMATION

Terminal Assignment

The TAS5352A is available in a thermally enhanced 44-pin HTSSOP PowerPad[™] package (DDV)

This package contains a thermal pad that is located on the top side of the device for convenient thermal coupling to the heatsink.





www.ti.com

Protection MODE Selection Pins

Protection modes are selected by shorting M1, M2, and M3 to VREG or GND.

Ν	ODE PIN	IS	Mada Nama	D14/64 (mm.) + (1)	Description		
М3	M2	M1	Mode Name	PWM Input ⁽¹⁾	Description		
0	0	0	BTL mode 1	2N	All protection systems enabled		
0	0	1	BTL mode 2	2N	Latching shutdown on, PWM activity detector and OLP disabled		
0	1	0	BTL mode 3	1N	All protection systems enabled		
0	1	1	PBTL mode	1N / 2N ⁽²⁾	All protection systems enabled All protection systems enabled		
1	0	0	SE mode 1	1N	All protection systems enabled ⁽³⁾		
1	0	1	SE mode 2	1N	Latching shutdown on, PWM activity detector and OLP disabled ⁽³⁾		
1	1	0			Deserved		
1	1	1			Reserved		

The 1N and 2N naming convention is used to indicate the number of PWM lines to the power stage per channel in a specific mode.
PWM_D is used to select between the 1N and 2N interface in PBTL mode (Low = 1N; High = 2N). PWM_D is internally pulled low in

PBTL mode. PWM_A is used as the PWM input in 1N mode and PWM_A and PWM_B are used as inputs for the 2N mode.

(3) PPSC detection system disabled.

Package Heat Dissipation Ratings⁽¹⁾

PARAMETER	TAS5352ADDV
R _{0JC} (°C/W)—2 BTL or 4 SE channels	1.3
R _{0JC} (°C/W)—1 BTL or 2 SE channel(s)	2.6
R _{0JC} (°C/W)—1 SE channel	5.0
Power Pad area ⁽²⁾	36 mm ²

(1) JC is junction-to-case, CH is case-to-heatsink.

(2) $R_{\theta CH}$ is an important consideration. Assume a 2-mil thickness of high performance grease with a thermal conductivity at 2.5W/m-K between the pad area and the heat sink. The $R_{\theta CH}$ with this condition is 0.6°C/W for the DDV package.



SLES239-NOVEMBER 2008

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range unless otherwise noted ⁽¹⁾

TAS5352A	
VDD to AGND	–0.3 V to 13.2 V
GVDD_X to AGND	–0.3 V to 13.2 V
PVDD_X to GND_X (2)	–0.3 V to 53 V
OUT_X to GND_X ⁽²⁾	–0.3 V to 53 V
BST_X to GND_X ⁽²⁾	-0.3 V to 66.2 V
BST_X to GVDD_X ⁽²⁾	–0.3 V to 53 V
VREG to AGND	-0.3 V to 4.2 V
GND_X to GND	-0.3 V to 0.3 V
GND_X to AGND	-0.3 V to 0.3 V
GND to AGND	-0.3 V to 0.3 V
PWM_X, OC_ADJ, M1, M2, M3 to AGND	-0.3 V to 4.2 V
RESET_X, SD, OTW to AGND	–0.3 V to 7 V
Maximum continuous sink current (SD, OTW)	9 mA
Maximum operating junction temperature range, T _J	0°C to 125°C
Storage temperature	-40°C to 125°C
Lead temperature, 1,6 mm (1/16 inch) from case for 10 seconds	260°C
Minimum pulse duration, low	30 ns

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) These voltages represent the dc voltage + peak ac waveform measured at the terminal of the device in all conditions.

ORDERING INFORMATION⁽¹⁾

T _A	PACKAGE	DESCRIPTION
0°C to 70°C	TAS5352ADDV	44-pin HTSSOP

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.



Terminal Functions

TAS5352A

SLES239-NOVEMBER 2008

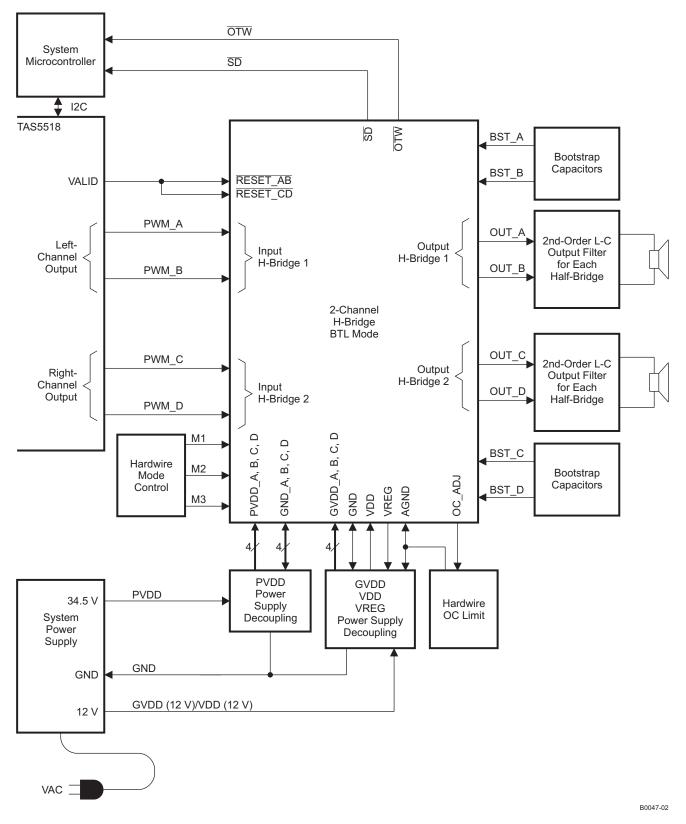
TE	RMINAL		DEGODISTICU
NAME	DDV NO.	FUNCTION ⁽¹⁾	DESCRIPTION
AGND	11	Р	Analog ground
BST_A	43	Р	Bootstrap pin, A-Side
BST_B	34	Р	Bootstrap pin, B-Side
BST_C	33	Р	Bootstrap pin, C-Side
BST_D	24	Р	Bootstrap pin, D-Side
GND	10	Р	Ground
GND_A	38	Р	Power ground for half-bridge A
GND_B	37	Р	Power ground for half-bridge B
GND_C	30	Р	Power ground for half-bridge C
GND_D	29	Р	Power ground for half-bridge D
GVDD_A	44	Р	Gate-drive voltage supply; A-Side
GVDD_B	1	Р	Gate-drive voltage supply; B-Side
GVDD_C	22	Р	Gate-drive voltage supply; C-Side
GVDD_D	23	Р	Gate-drive voltage supply; D-Side
M1	15	I	Mode selection pin (LSB)
M2	14	l	Mode selection pin
M3	13	I	Mode selection pin (MSB)
NC	3, 4, 19, 20, 25, 42	_	No connect. Pins may be grounded.
OC_ADJ	9	0	Analog overcurrent programming pin
OTW	2	0	Overtemperature warning signal, open-drain, active-low
OUT_A	39	0	Output, half-bridge A
OUT_B	36	0	Output, half-bridge B
OUT_C	31	0	Output, half-bridge C
OUT_D	28	0	Output, half-bridge D
PVDD_A	40, 41	Р	Power supply input for half-bridge A
PVDD_B	35	Р	Power supply input for half-bridge B
PVDD_C	32	Р	Power supply input for half-bridge C
PVDD_D	26, 27	Р	Power supply input for half-bridge D
PWM_A	6	I	PWM Input signal for half-bridge A
PWM_B	8	I	PWM Input signal for half-bridge B
PWM_C	16	I	PWM Input signal for half-bridge C
PWM_D	18	I	PWM Input signal for half-bridge D
RESET_AB	7	I	Reset signal for half-bridge A and half-bridge B, active-low
RESET_CD	17	I	Reset signal for half-bridge C and half-bridge D, active-low
SD	5	0	Shutdown signal, open-drain, active-low
VDD	21	Р	Input power supply
VREG	12	Р	Internal voltage regulator

(1) I = input, O = output, P = power

INSTRUMENTS www.ti.com

Texas

TYPICAL SYSTEM BLOCK DIAGRAM



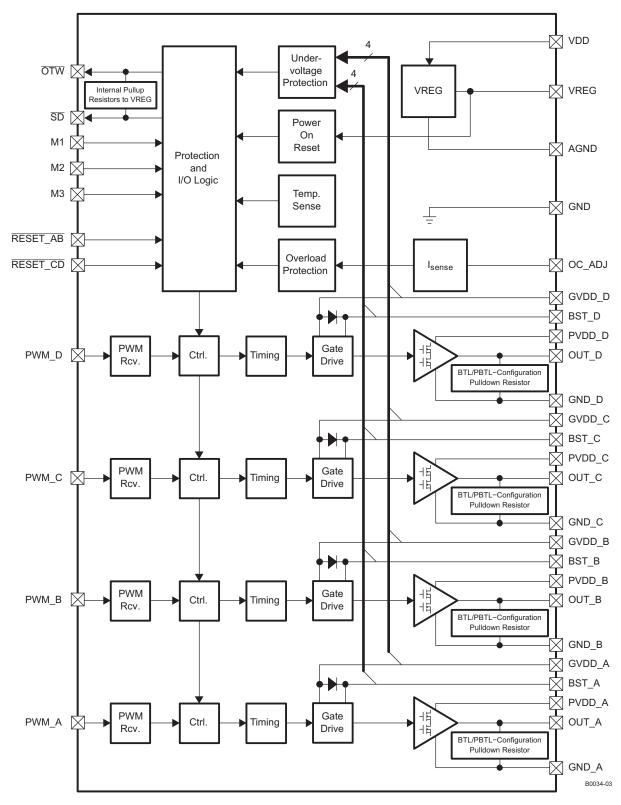


TAS5352A

www.ti.com

SLES239-NOVEMBER 2008

FUNCTIONAL BLOCK DIAGRAM





RECOMMENDED OPERATING CONDITIONS

			MIN	TYP	MAX	UNIT
PVDD_X	Half-bridge supply voltage		0	34.5	37	V
GVDD_X	Supply voltage for logic regulators and gate-drive circuitry		10.8	12	13.2	V
VDD	Digital regulator supply voltage		10.8	12	13.2	V
R _L (BTL)	Resistive load impedance (no Cycle-by_Cycle		3	4		
R _L (SE)	current control), recommended demodulation		2.25	3		Ω
R _L (PBTL)	filter		1.5	34.5 37 12 13.2 12 13.2 12 13.2 12 13.2 4 3 2 10 10 10 384 432 0.1 33 22 47 4.7		
L _{Output} (BTL)			5	10		
L _{Output} (SE)	Output-filter inductance	Minimum output inductance under short-circuit condition	5	10		μH
L _{Output} (PBTL)			5	10	2 10 10 10 384 432	
f _S	PWM frame rate		192	384	432	kHz
t _{LOW}	Minimum low-state pulse duration per PWM Frame, noise shaper enabled		30			nS
C _{PVDD}	PVDD close decoupling capacitors			0.1		μF
C _{BST}	Bootstrap capacitor, selected value supports PWM frame rates from 192 kHz to 432 kHz			33		nF
R _{OC}	Over-current programming resistor	Resistor tolerance = 5%	22	22	47	kΩ
R _{EXT-PULLUP}	External pull-up resistor to +3.3V to +5.0V for SD or OTW		3.3	4.7		kΩ
TJ	Junction temperature		0		125	°C

AUDIO SPECIFICATIONS (BTL)

Audio performance is recorded as a chipset consisting of a TAS5518 pwm processor (modulation index limited to 97.7%) and a TAS5352A power stage. PCB and system configuration are in accordance with recommended guidelines. Audio frequency = 1kHz, PVDD_x = 34.5 V, GVDD_x = 12 V, R_L = 4 Ω , f_S = 384 kHz, R_{OC} = 22 k Ω , T_C = 75°C, Output Filter: L_{DEM} = 10 μ H, C_{DEM} = 470 nF, unless otherwise noted.

	PARAMETER	TEST CONDITIONS	TAS5352A			UNIT
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
		$R_L = 4 \Omega$, 10% THD+N, clipped input signal		125		
P _{OMAX}	Maximum Power Output	R_L = 6 Ω , 10% THD+N, clipped input signal		100		
		R_L = 8 Ω, 10% THD+N, clipped input signal		76		W
		$R_L = 4 \ \Omega$, 0 dBFS, unclipped input signal		96		
Po	o Unclipped Power Output	$R_L = 6 \ \Omega$, 0 dBFS, unclipped input signal		72		
		$R_L = 8 \Omega$, 0 dBFS, unclipped input signal		57		
THD+N	Total harmonic distortion + noise	0 dBFS; AES17 filter		0.4%		
I TD+N	Total harmonic distortion + hoise	1 W; AES17 filter		0.09%		
V _n	Output integrated noise	A-weighted, AES17 filter, Auto mute disabled		50		μV
SNR	Signal-to-noise ratio ⁽¹⁾	A-weighted, AES17 filter, Auto mute disabled		110		dB
DNR	Dynamic range	A-weighted, input level = -60 dBFS, AES17 filter		110		dB
DC Offset	Output offset voltage			+/- 15		mV
P _{idle}	Power dissipation due to idle losses (IPVDD_X)	$P_O = 0$ W, all halfbridges switching ⁽²⁾		2.6		W

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.



www.ti.com

AUDIO SPECIFICATIONS (Single-Ended Output)

Audio performance is recorded as a chipset consisting of a TAS5086 pwm processor (modulation index limited to 97.7%) and a TAS5352A power stage. PCB and system configuration are in accordance with recommended guidelines. Audio frequency = 1kHz, PVDD_x = 34.5 V, GVDD_x = 12 V, R_L = 4 Ω , f_s = 384 kHz, R_{OC} = 22 k Ω , T_c = 75°C, Output Filter: L_{DEM} = 20 μ H, C_{DEM} = 1.0 μ F, unless otherwise noted.

	PARAMETER	TEST CONDITIONS	TA	S5352A	۱	UNIT
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
D	Maximum Dawar Outaut	$R_L = 3 \Omega$, 10% THD+N, clipped input signal		45		
P _{OMAX}	Maximum Power Output	$R_L = 4 \Omega$, 10% THD+N, clipped input signal		35		W
D	Unclipped Power Output	R_L = 3 Ω , 0 dBFS, unclipped input signal		35		vv
Po	Unclipped Power Output	$R_L = 4 \Omega$, 0 dBFS, unclipped input signal		25		
	Total harmonia distartion + paisa	0 dBFS; AES17 filter		0.4%		
THD+N	Total harmonic distortion + noise	1 W; AES17 filter		0.09%		
V _n	Output integrated noise	A-weighted, AES17 filter, Auto mute disabled		40		μV
SNR	Signal-to-noise ratio ⁽¹⁾	A-weighted, AES17 filter, Auto mute disabled		109		dB
DNR	Dynamic range	A-weighted, input level = -60 dBFS AES17 filter		109		dB
P _{idle}	Power dissipation due to idle losses (IPVDD_X)	$P_O = 0$ W, all halfbridges switching ⁽²⁾		2.6		W

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.

AUDIO SPECIFICATIONS (PBTL)

Audio performance is recorded as a chipset consisting of a TAS5518 pwm processor (modulation index limited to 97.7%) and a TAS5352A power stage. PCB and system configuration are in accordance with recommended guidelines. Audio frequency = 1kHz, PVDD_x = 34.5 V, GVDD_x = 12 V, R_L = 3 Ω , f_s = 384 kHz, R_{OC} = 22 k Ω , T_c = 75°C, Output Filter: L_{DEM} = 10 μ H, C_{DEM} = 1 μ F, unless otherwise noted.

	DADAMETED		ТА	S5352A		
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
P	Maximum Power Output	R_L = 3 Ω , 10% THD+N, clipped input signal		195		
P _{OMAX}	Maximum Power Output	$R_L = 2 \Omega$, 10% THD+N, clipped input signal		250		W
P	Unclipped Power Output	$R_L = 3 \Omega$, 0 dBFS, unclipped input signal		145		vv
Po	Unclipped Fower Output	$R_L = 2 \Omega$, 0 dBFS, unclipped input signal		190		
THD+N	Total bases also distantian a solar	0 dBFS; AES17 filter		0.4%		
I HD+N	Total harmonic distortion + noise	1 W; AES17 filter		0.09%		
V _n	Output integrated noise	A-weighted, AES17 filter, Auto mute disabled		50		μV
SNR	Signal-to-noise ratio ⁽¹⁾	A-weighted, AES17 filter, Auto mute disabled		110		dB
DNR	Dynamic range	A-weighted, input level = -60 dBFS AES17 filter		110		dB
DC Offset	Output offset voltage			+/- 15		mV
P _{idle}	Power dissipation due to idle losses (IPVDD_X)	$P_{O} = 0$ W, all halfbridges switching ⁽²⁾		2.6		W

(1) SNR is calculated relative to 0-dBFS input level.

(2) Actual system idle losses are affected by core losses of output inductors.

SLES239-NOVEMBER 2008

ELECTRICAL CHARACTERISTICS

 $PVDD_x = 34.5 V, GVDD_X = 12 V, VDD = 12 V, T_C$ (Case temperature) = 25°C, f_S = 384 kHz, unless otherwise specified.

PARAMETER		TEST CONDITIONS	TAS5352A			UNIT
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Internal Voltage	Regulator and Current Consumption					
VREG	Voltage regulator, only used as a reference node	VDD = 12 V	3	3.3	3.6	V
IVDD	VDD supply current	Operating, 50% duty cycle		7.2	17	mA
	VDD supply current	Idle, reset mode		5.5	11	ША
IGVDD_X	Gate supply current per half-bridge	50% duty cycle		8	16	mA
IGVDD_X	Gate supply current per nall-blidge	Reset mode		1	1.8	ША
IPVDD_X	Half-bridge idle current	50% duty cycle, with 10 μH and 470 nF output filter.		19.0	25	mA
		Reset mode, no switching		525	630	μΑ
Output Stage M	OSFETs					
R _{DSon,LS}	Drain-to-source resistance, Low Side	$T_J = 25^{\circ}C$, excludes metalization resistance,		80	89	mΩ
R _{DSon,HS}	Drain-to-source resistance, High Side	$T_J = 25^{\circ}C$, excludes metalization resistance,		80	89	mΩ
I/O Protection						
V _{uvp,G}	Undervoltage protection limit, GVDD_X			9.5		V
V _{uvp,hyst} ⁽¹⁾	Undervoltage protection limit, GVDD_X			250		mV
BST _{uvpF}	Puts device into RESET when BST voltage falls below limit			5.9		V
BST _{uvpR}	Brings device out of RESET when BST voltage rises above limit			7		V
OTW ⁽¹⁾	Overtemperature warning		115	125	135	°C
OTW _{HYST} ⁽¹⁾	Temperature drop needed below OTW temp. for OTW to be inactive after the OTW event			25		°C
OTE ⁽¹⁾	Overtemperature error threshold		145	155	165	°C
OTE- OTW _{differential} ⁽¹⁾	OTE - OTW differential, temperature delta between OTW and OTE			30		°C
OLPC	Overload protection counter	f _S = 384 kHz		1.25		ms
I _{oc}	Overcurrent limit protection	Resistor—programmable, high-end, R _{OC} = 22 k Ω with 1 mS pulse		10.9		А
I _{OCT}	Overcurrent response time			150		ns
t _{ACTIVITY} DETECTOR	Time for PWM activity detector to activate when no PWM is present	Lack of transition of any PWM input		13.2		μS
I _{PD}	Output pulldown current of each half-bridge	Connected when RESET is active to provide bootstrap capacitor charge. Not used in SE mode.		3		mA
Static Digital Sp	pecifications	· ·				
V _{IH}	High-level input voltage	PWM_A, PWM_B, PWM_C, PWM_D, M1,	2			V
V _{IL}	Low-level input voltage	M2, M3, RESET_AB, RESET_CD			0.8	V
I _{Leakage}	Input leakage current				100	μA
OTW/SHUTDOV	VN (SD)					
R _{INT_PU}	Internal <u>pul</u> lup resistance, OTW to VREG, SD to VREG		20	26	32	kΩ
V _{OH}	High-level output voltage	Internal pullup resistor	3	3.3	3.6	V
		External pullup of 4.7 k Ω to 5 V	4.5		5	

(1) Specified by design

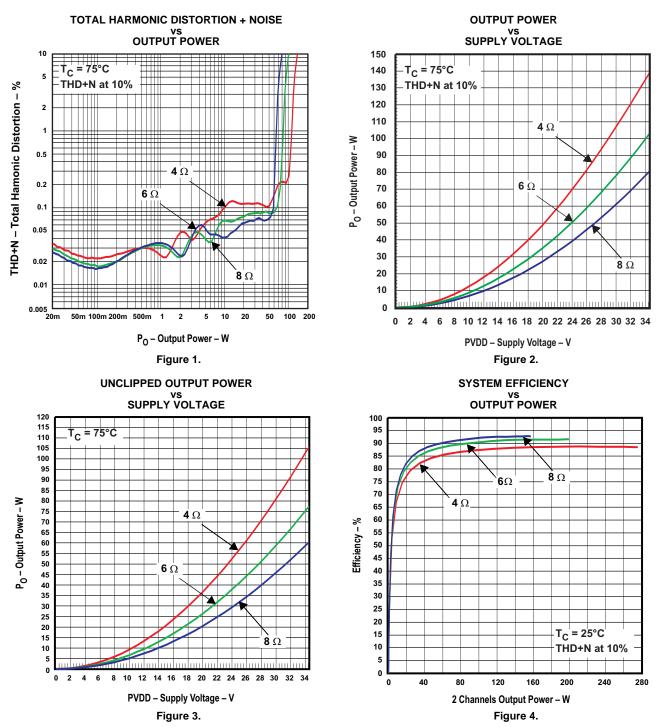


ELECTRICAL CHARACTERISTICS (continued)

PVDD_x = 34.5 V, GVDD_X = 12 V, VDD = 12 V, T_C (Case temperature) = 25°C, f_S = 384 kHz, unless otherwise specified.

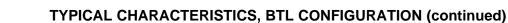
PARAMETER		TEST CONDITIONS	TAS5352A			UNIT
	FARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
V _{OL}	Low-level output voltage	I _O = 4 mA		0.2	0.4	V
FANOUT	Device fanout OTW, SD	No external pullup		30		Devices

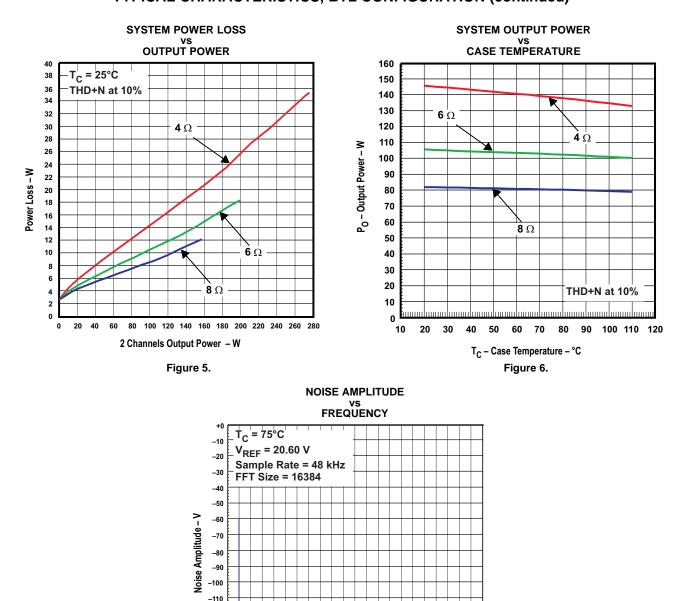
TYPICAL CHARACTERISTICS, BTL CONFIGURATION



Copyright © 2008, Texas Instruments Incorporated

www.ti.com





-120 -130 -140 -150

-160

0

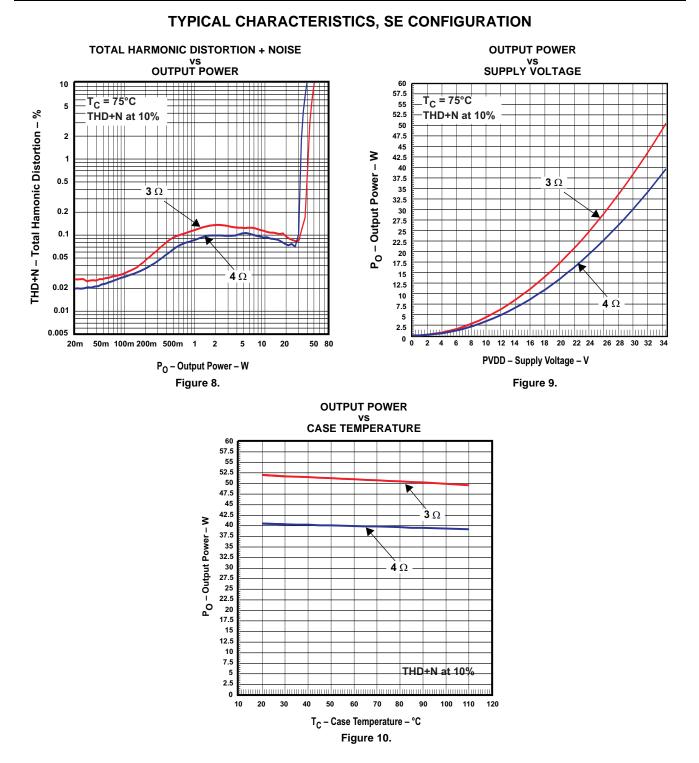
والمترار بتبعد وتندر والمراجعة والمراجعة والمتراجعة فالتنا التبار التترابطي والتراجعة والمراجع والمراجع المترا

f – Frequency – kHz Figure 7.

1k 2k 3k 4k 5k 6k 7k 8k 9k 10k 11k 12k 13k 14k 15k 16k 17k 18k 19k 20k 21k 22k



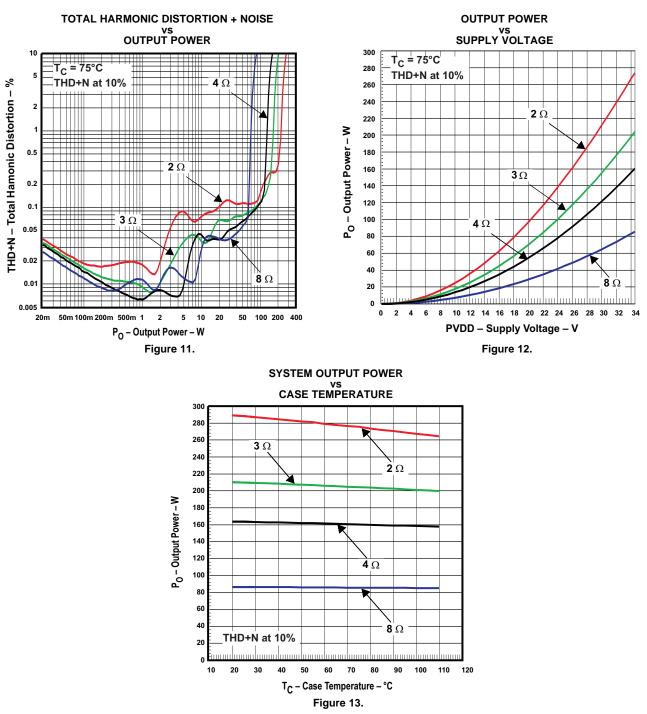
www.ti.com



Product Folder Link(s): TAS5352A







TYPICAL CHARACTERISTICS, PBTL CONFIGURATION



APPLICATION INFORMATION

PCB Material Recommendation

FR-4 Glass Epoxy material with 2 oz. (70 μ m) is recommended for use with the TAS5352A. The use of this material can provide for higher power output, improved thermal performance, and better EMI margin (due to lower PCB trace inductance.

PVDD Capacitor Recommendation

The large capacitors used in conjunction with each full-bridge, are referred to as the PVDD Capacitors. These capacitors should be selected for proper voltage margin and adequate capacitance to support the power requirements. In practice, with a well designed system power supply, 1000 μ F, 50-V will support more applications. The PVDD capacitors should be low ESR type because they are used in a circuit associated with high-speed switching.

Decoupling Capacitor Recommendations

In order to design an amplifier that has robust performance, passes regulatory requirements, and exhibits good audio performance, good quality decoupling capacitors should be used. In practice, X7R should be used in this application.

The voltage of the decoupling capacitors should be selected in accordance with good design practices. Temperature, ripple current, and voltage overshoot must be considered. This fact is particularly true in the selection of the 0.1μ F that is placed on the power supply to each half-bridge. It must withstand the voltage overshoot of the PWM switching, the heat generated by the amplifier during high power output, and the ripple current created by high power output. A minimum voltage rating of 50-V is required for use with a 34.5 V power supply.

System Design Recommendations

The following schematics and PCB layouts illustrate "best practices" in the use of the TAS5352A.

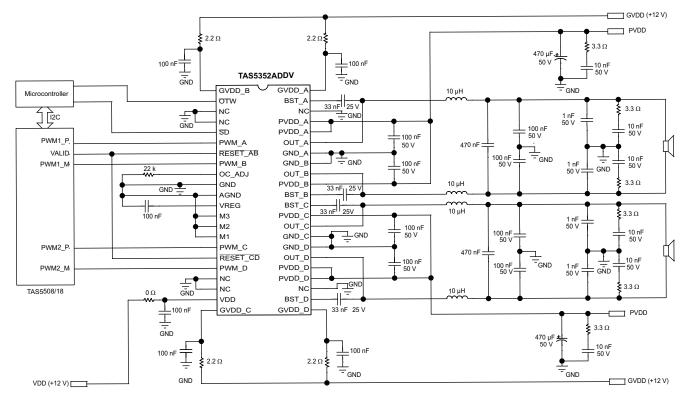


Figure 14. Typical Differential (2N) BTL Application With AD Modulation Filters



INSTRUMENTS

TEXAS

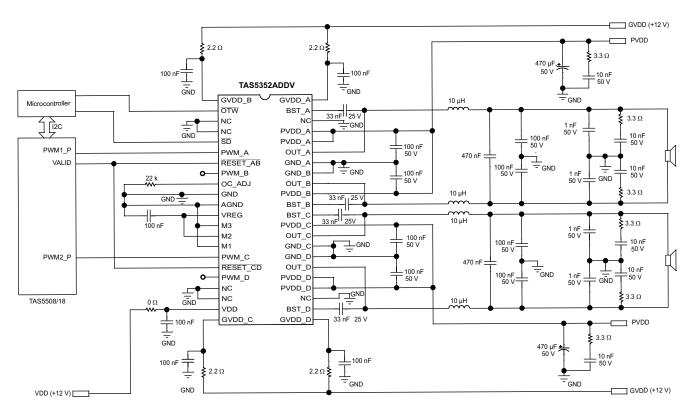


Figure 15. Typical Non-Differential (1N) BTL Application With AD Modulation Filters





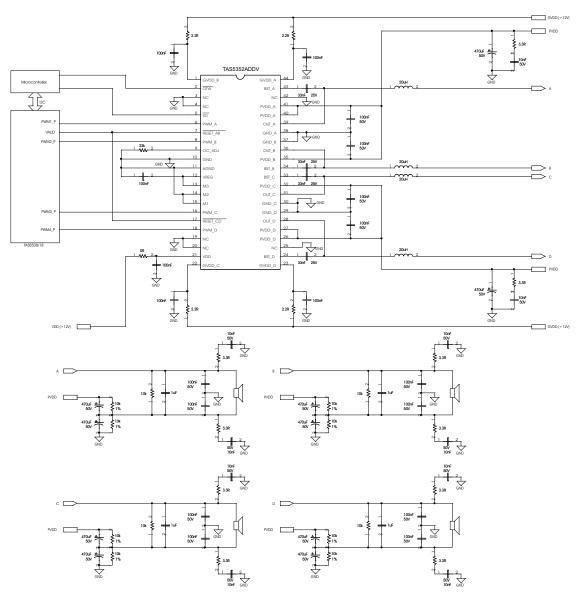
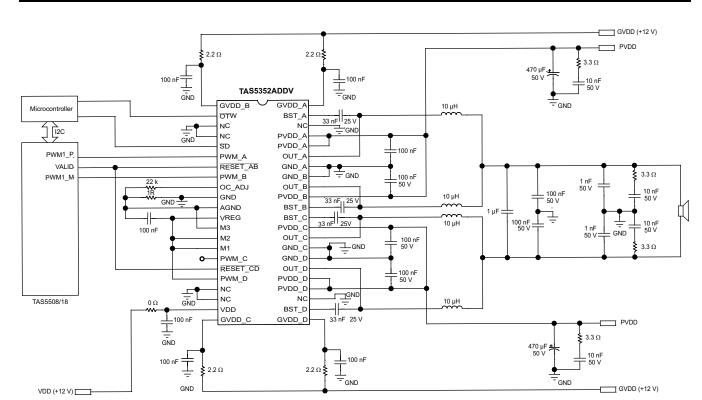


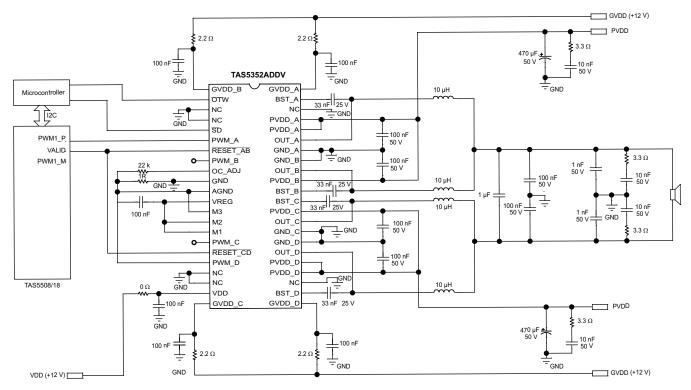
Figure 16. Typical SE Application

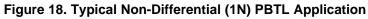
TEXAS INSTRUMENTS

www.ti.com











THEORY OF OPERATION

POWER SUPPLIES

To facilitate system design, the TAS5352A needs only a 12 V supply in addition to the (typical) 34.5 V power-stage supply. An internal voltage regulator provides suitable voltage levels for the digital and low-voltage analog circuitry. Additionally, all circuitry requiring a floating voltage supply, e.g., the high-side gate drive, is accommodated by built-in bootstrap circuitry requiring only an external capacitor for each half-bridge.

In order to provide outstanding electrical and acoustical characteristics, the PWM signal path including gate drive and output stage is designed as identical, independent half-bridges. For this reason, each half-bridge has separate gate drive supply (GVDD X), bootstrap pins (BST X), and power-stage supply pins (PVDD_X). Furthermore, an additional pin (VDD) is provided as supply for all common circuits. Although supplied from the same 12-V source, it is highly recommended to separate GVDD A. GVDD_B, GVDD_C, GVDD_D, and VDD on the printed-circuit board (PCB) by RC filters (see application diagram for details). These RC filters provide the recommended high-frequency isolation. Special attention should be paid to placing all decoupling capacitors as close to their associated pins as possible. In general, inductance between the power supply pins and decoupling capacitors must be avoided. (See reference board documentation for additional information.)

For a properly functioning bootstrap circuit, a small ceramic capacitor must be connected from each bootstrap pin (BST X) to the power-stage output pin (OUT X). When the power-stage output is low, the bootstrap capacitor is charged through an internal diode connected between the gate-drive powersupply pin (GVDD X) and the bootstrap pin. When the power-stage output is high, the bootstrap capacitor potential is shifted above the output potential and thus provides a suitable voltage supply for the high-side gate driver. In an application with PWM switching frequencies in the range from 352 kHz to 384 kHz, it is recommended to use 33-nF ceramic capacitors, size 0603 or 0805, for the bootstrap supply. These 33-nF capacitors ensure sufficient energy storage, even during minimal PWM duty cycles, to keep the high-side power stage FET (LDMOS) fully turned on during the remaining part of the PWM cycle. In an application running at a reduced switching frequency, generally 192 kHz, the bootstrap capacitor might need to be increased in value.

Special attention should be paid to the power-stage power supply; this includes component selection, PCB placement, and routing. As indicated, each half-bridge has independent power-stage supply pins (PVDD_X). For optimal electrical performance, EMI compliance, and system reliability, it is important that each PVDD_X pin is decoupled with a 100-nF ceramic capacitor placed as close as possible to each supply pin. It is recommended to follow the PCB layout of the TAS5352A reference design. For additional information on recommended power supply and required components, see the application diagrams given previously in this data sheet.

The 12 V supply should be from a low-noise, low-output-impedance voltage regulator. Likewise, the 34.5 V power-stage supply is assumed to have low output impedance and low noise. The power-supply sequence is not critical as facilitated by the internal power-on-reset circuit. Moreover, the TAS5352A is fully protected against erroneous power-stage turnon due to parasitic gate charging. Thus, voltage-supply ramp rates (dV/dt) are non-critical within the specified range (see the *Recommended Operating Conditions* section of this data sheet).

SYSTEM POWER-UP/POWER-DOWN SEQUENCE

Powering Up

The TAS5352A does not require a power-up sequence. The outputs of the H-bridges remain in a high-impedance state until the gate-drive supply voltage (GVDD_X) and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the *Electrical Characteristics* section of this data sheet). Although not specifically required, it is recommended to hold RESET_AB and RESET_CD in a low state while powering up the device. This allows an internal circuit to charge the external bootstrap capacitors by enabling a weak pulldown of the half-bridge output.

When the TAS5352A is being used with TI PWM modulators such as the TAS5518, no special attention to the state of RESET_AB and RESET_CD is required, provided that the chipset is configured as recommended.

Powering Down

The TAS5352A does not require a power-down sequence. The device remains fully operational as long as the gate-drive supply (GVDD_X) voltage and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the *Electrical*

Characteristics section of this data sheet). Although not specifically required, it is a good practice to hold RESET_AB and RESET_CD low during power down, thus preventing audible artifacts including pops or clicks.

When the TAS5352A is being used with TI PWM modulators such as the TAS5518, no special attention to the state of RESET_AB and RESET_CD is required, provided that the chipset is configured as recommended.

Mid Z Sequence Compatibility

The TAS5352A is compatible with the Mid Z sequence of the TAS5086 Modulator. The Mid Z Sequence is a series of pulses that is generated by the modulator. This sequence causes the power stage to slowly enable its outputs as it begins to switch.

By slowly starting the PWM switching, the impulse response created by the onset of switching is reduced. This impulse response is the acoustic artifact that is heard in the output transducers (loudspeakers) and is commonly termed "click" or "pop".

The low acoustic artifact noise of the TAS5352A will be further decreased when used in conjunction with the TAS5086 modulator with the Mid Z Sequence enabled.

The Mid Z sequence is primarily used for the single-ended output configuration. It facilitates a "softer" PWM output start after the split cap output configuration is charged.

ERROR REPORTING

The SD and OTW pins are both active-low, open-drain outputs. Their function is for protection-mode signaling to a PWM controller or other system-control device.

Any <u>fault</u> resulting in device shutdown is signaled by the SD pin going low. Likewise, OTW goes low when the device junction temperature exceeds 125°C (see the following table).

SD	OTW	DESCRIPTION
0	0	Overtemperature (OTE) or overload (OLP) or undervoltage (UVP)
0	1	Overload (OLP) or undervoltage (UVP)
1	0	Junction temperature higher than 125°C (overtemperature warning)
1	1	Junction temperature lower than 125°C and no OLP or UVP faults (normal operation)

Note that asserting either $\overline{\text{RESET}_{AB}}$ or $\overline{\text{RESET}_{CD}}$ low forces the $\overline{\text{SD}}$ signal high, independent of faults being present. TI recommends monitoring the $\overline{\text{OTW}}$





signal using the system microcontroller and responding to an overtemperature warning signal by, e.g., turning down the volume to prevent further heating of the device resulting in device shutdown (OTE).

To reduce external component count, an internal pullup resistor to 3.3 V is provided on both SD and OTW outputs. Level compliance for 5-V logic can be obtained by adding external pullup resistors to 5 V (see the *Electrical Characteristics* section of this data sheet for further specifications).

DEVICE PROTECTION SYSTEM

The TAS5352A contains advanced protection circuitry carefully designed to facilitate system integration and ease of use, as well as to safeguard the device from permanent failure due to a wide range of fault short circuits, conditions such as overload. overtemperature, and undervoltage. The TAS5352A responds to a fault by immediately setting the power stage in a high-impedance (Hi-Z) state and asserting the SD pin low. In situations other than overload and over-temperature error (OTE), the device automatically recovers when the fault condition has been removed, i.e., the supply voltage has increased.

The device will function on errors, as shown in the following table

BTL	MODE	PBT	L MODE	SE MODE		
Local Error In	Turns Off	Local Error In	Turns Off	Local Error In	Turns Off	
Α	A + B	А		А	A + B	
В	A+D	В	A + B + C	В	A+D	
С	C + D	С	+ D	С	C + D	
D	C+D	D		D	C + D	

Bootstrap UVP does not shutdown according to the table, it shuts down the respective halfbridge.

Use of TAS5352A in High-Modulation-Index Capable Systems

This device requires at least 30 ns of low time on the output per 384-kHz PWM frame rate in order to keep the bootstrap capacitors charged. As an example, if the modulation index is set to 99.2% in the TAS5508, this setting allows PWM pulse durations down to 10 ns. This signal, which does not meet the 30-ns requirement, is sent to the PWM_X pin and this low-state pulse time does not allow the bootstrap capacitor to stay charged. The TAS5352A device requires limiting the TAS5508 modulation index to 97.7% to keep the bootstrap capacitor charged under all signals and loads.

The TAS5352A contains a bootstrap capacitor under voltage protection circuit (BST_UVP) that monitors the voltage on the bootstrap capacitors. When the



voltage on the bootstrap capacitors is less than required for proper control of the High-Side MOSFETs, the device will initiate bootstrap capacitor recharge sequences until the bootstrap capacitors are properly charged for robust operation. This function may be activated with PWM pulses less than 30 nS.

Therefore, TI strongly recommends using a TI PWM processor, such as TAS5518, TAS5086 or TAS5508, with the modulation index set at 97.7% to interface with TAS5352A.

Overcurrent (OC) Protection With Current Limiting and Overload Detection

The device has independent, fast-reacting current detectors with programmable trip threshold (OC threshold) on all high-side and low-side power-stage FETs. See the following table for OC-adjust resistor values. The detector outputs are closely monitored by two protection systems. The first protection system controls the power stage in order to prevent the output current from further increasing, i.e., it performs a current-limiting function rather than prematurely shutting down during combinations of high-level music transients and extreme speaker load impedance drops. If the high-current situation persists, i.e., the power stage is being overloaded, a second protection system triggers a latching shutdown, resulting in the power stage being set in the high-impedance (Hi-Z) state. Current limiting and overload protection are independent for half-bridges A and B and, respectively, C and D. That is, if the bridge-tied load between half-bridges A and B causes an overload fault, only half-bridges A and B are shut down.

- For the lowest-cost bill of materials in terms of component selection, the OC threshold measure should be limited, considering the power output requirement and minimum load impedance. Higher-impedance loads require a lower OC threshold.
- The demodulation-filter inductor must retain at least 5 μH of inductance at twice the OC threshold setting.

Unfortunately, most inductors have decreasing inductance with increasing temperature and increasing current (saturation). To some degree, an increase in temperature naturally occurs when operating at high output currents, due to core losses and the dc resistance of the inductor's copper winding. A thorough analysis of inductor saturation and thermal properties is strongly recommended.

Setting the OC threshold too low might cause issues such as lack of enough output power and/or unexpected shutdowns due to too-sensitive overload detection. In general, it is recommended to follow closely the external component selection and PCB layout as given in the *Application* section.

For added flexibility, the OC threshold is programmable within a limited range using a single external resistor connected between the OC_ADJ pin and AGND. (See the Electrical Characteristics section of this data sheet for information on the correlation between programming-resistor value and the OC threshold.) It should be noted that a properly functioning overcurrent detector assumes the presence of a properly designed demodulation filter at the power-stage output. It is required to follow certain guidelines when selecting the OC threshold and an appropriate demodulation inductor:

OC-Adjust Resistor Values (kΩ)	Max. Current Before OC Occurs (A), T _C = 75°C				
22	10.9				
33	9.1				
47	7.1				

The reported max peak current in the table above is measured with continuous current in 1 Ω , one channel active and the other one muted.

Pin-To-Pin Short Circuit Protection (PPSC)

The PPSC detection system protects the device from permanent damage in the case that a power output pin (OUT X) is shorted to GND X or PVDD X. For comparison the OC protection system detects an over current after the demodulation filter where PPSC detects shorts directly at the pin before the filter. PPSC detection is performed at startup i.e. when VDD is supplied, consequently a short to either GND X or PVDD X after system startup will not activate the PPSC detection system. When PPSC detection is activated by a short on the output, all half bridges are kept in a Hi-Z state until the short is removed, the device then continues the startup sequence and starts switching. The detection is controlled globally by a two step sequence. The first step ensures that there are no shorts from OUT X to GND X, the second step tests that there are no shorts from OUT X to PVDD X. The total duration of this process is roughly proportional to the capacitance of the output LC filter. The typical duration is < 15ms/uF. While the PPSC detection is in progress, SD is kept low, and the device will not react to changes applied to the RESET pins. If no shorts are present the PPSC detection passes, and SD is released. A device reset will not start a new PPSC detection. PPSC detection is enabled in BTL and PBTL output configurations, the detection is not performed in SE mode. To make sure not to trip the PPSC detection system it is recommended not to insert resistive load to GND X or PVDD X.

Copyright © 2008, Texas Instruments Incorporated



www.ti.com

Overtemperature Protection

The TAS5352A has а two-level temperature-protection system that asserts an active-low warning signal (OTW) when the device junction temperature exceeds 125°C (typical) and, if the device junction temperature exceeds 155°C (typical), the device is put into thermal shutdown, resulting in all half-bridge outputs being set in the high-impedance (Hi-Z) state and SD being asserted low. OTE is latched in this case. To clear the OTE latch, either RESET_AB or RESET_CD must be asserted. Thereafter, the device resumes normal operation.

Undervoltage Protection (UVP) and Power-On Reset (POR)

The UVP and POR circuits of the TAS5352A fully protect the device in any power-up/down and brownout situation. While powering up, the POR circuit resets the overload circuit (OLP) and ensures that all circuits are fully operational when the GVDD_X and VDD supply voltages reach stated in the Electrical Characteristics Table. Although GVDD_X and VDD are independently monitored, a supply voltage drop below the UVP threshold on any VDD or GVDD_X pin results in all half-bridge outputs immediately being set in the high-impedance (Hi-Z) state and SD being asserted low. The device automatically resumes operation when all supply voltages have increased above the UVP threshold.

DEVICE RESET

Two reset pins are provided for independent control of half-bridges A/B and C/D. When RESET_AB is asserted low, all four power-stage FETs in halfbridges A and B are forced into a high-impedance (Hi-Z) state. Likewise, asserting RESET_CD low forces all four power-stage FETs in half-bridges C and D into a high-impedance state. Thus, both reset pins are well suited for hard-muting the power stage if needed.

In BTL modes, to accommodate bootstrap charging prior to switching start, asserting the reset inputs low enables weak pulldown of the half-bridge outputs. In the SE mode, the weak pulldowns are not enabled, and it is therefore recommended to ensure bootstrap capacitor charging by providing a low pulse on the PWM inputs when reset is asserted high.

Asserting either reset input low removes any fault information to be signaled on the SD output, i.e., SD is forced high.

A rising-edge transition on either reset input allows the device to resume operation after an overload fault. To ensure thermal reliability, the rising edge of reset must occur no sooner than 4 ms after the falling edge of SD.

PACKAGE MATERIALS INFORMATION

www.ti.com

TAPE AND REEL INFORMATION

REEL DIMENSIONS

TEXAS INSTRUMENTS





TAPE DIMENSIONS



A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

TAPE AND REEL INFORMATION

*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TAS5352ADDVR	HTSSOP	DDV	44	2000	330.0	24.4	8.6	15.6	1.8	12.0	24.0	Q1

TEXAS INSTRUMENTS

www.ti.com

PACKAGE MATERIALS INFORMATION

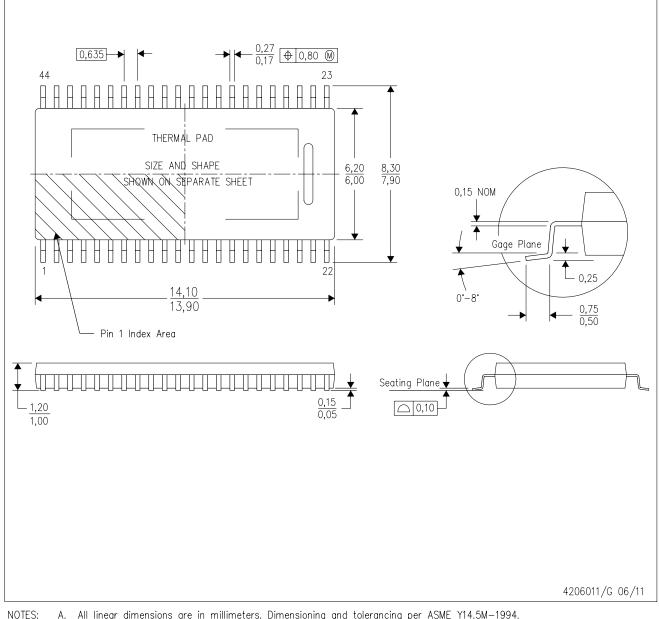
14-Jul-2012



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TAS5352ADDVR	HTSSOP	DDV	44	2000	367.0	367.0	45.0

DDV (R-PDSO-G44) PowerPAD[™] PLASTIC SMALL OUTLINE PACKAGE (DIE DOWN)



A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.

- c. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
- D. This package is designed to be attached directly to an external heatsink. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com http://www.ti.com. See the product data sheet for details regarding the exposed thermal pad dimensions.

PowerPAD is a trademark of Texas Instruments.



™SMALL OUTLINE <u>PACKAGE</u> PowerPAD DDV (R-PDSO-G44) THERMAL INFORMATION This PowerPAD[™] package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. This design optimizes the heat transfer from the integrated circuit (IC). For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com. The exposed thermal pad dimensions for this package are shown in the following illustration. 44 23 Exposed Thermal 38 Pad 4,20 3,50 2x0,60 22 1 8,30 6.90 Top View Exposed Thermal Pad Dimensions 4206975-2/D 07/11

NOTE: All linear dimensions are in millimeters



IMPORTANT NOTICE

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, enhancements, improvements and other changes to its semiconductor products and services per JESD46C and to discontinue any product or service per JESD48B. Buyers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All semiconductor products (also referred to herein as "components") are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its components to the specifications applicable at the time of sale, in accordance with the warranty in TI's terms and conditions of sale of semiconductor products. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by applicable law, testing of all parameters of each component is not necessarily performed.

TI assumes no liability for applications assistance or the design of Buyers' products. Buyers are responsible for their products and applications using TI components. To minimize the risks associated with Buyers' products and applications, Buyers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI components or services are used. Information published by TI regarding third-party products or services does not constitute a license to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of significant portions of TI information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. TI is not responsible or liable for such altered documentation. Information of third parties may be subject to additional restrictions.

Resale of TI components or services with statements different from or beyond the parameters stated by TI for that component or service voids all express and any implied warranties for the associated TI component or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Buyer acknowledges and agrees that it is solely responsible for compliance with all legal, regulatory and safety-related requirements concerning its products, and any use of TI components in its applications, notwithstanding any applications-related information or support that may be provided by TI. Buyer represents and agrees that it has all the necessary expertise to create and implement safeguards which anticipate dangerous consequences of failures, monitor failures and their consequences, lessen the likelihood of failures that might cause harm and take appropriate remedial actions. Buyer will fully indemnify TI and its representatives against any damages arising out of the use of any TI components in safety-critical applications.

In some cases, TI components may be promoted specifically to facilitate safety-related applications. With such components, TI's goal is to help enable customers to design and create their own end-product solutions that meet applicable functional safety standards and requirements. Nonetheless, such components are subject to these terms.

No TI components are authorized for use in FDA Class III (or similar life-critical medical equipment) unless authorized officers of the parties have executed a special agreement specifically governing such use.

Only those TI components which TI has specifically designated as military grade or "enhanced plastic" are designed and intended for use in military/aerospace applications or environments. Buyer acknowledges and agrees that any military or aerospace use of TI components which have *not* been so designated is solely at the Buyer's risk, and that Buyer is solely responsible for compliance with all legal and regulatory requirements in connection with such use.

TI has specifically designated certain components which meet ISO/TS16949 requirements, mainly for automotive use. Components which have not been so designated are neither designed nor intended for automotive use; and TI will not be responsible for any failure of such components to meet such requirements.

Products		Applications	
Audio	www.ti.com/audio	Automotive and Transportation	www.ti.com/automotive
Amplifiers	amplifier.ti.com	Communications and Telecom	www.ti.com/communications
Data Converters	dataconverter.ti.com	Computers and Peripherals	www.ti.com/computers
DLP® Products	www.dlp.com	Consumer Electronics	www.ti.com/consumer-apps
DSP	dsp.ti.com	Energy and Lighting	www.ti.com/energy
Clocks and Timers	www.ti.com/clocks	Industrial	www.ti.com/industrial
Interface	interface.ti.com	Medical	www.ti.com/medical
Logic	logic.ti.com	Security	www.ti.com/security
Power Mgmt	power.ti.com	Space, Avionics and Defense	www.ti.com/space-avionics-defense
Microcontrollers	microcontroller.ti.com	Video and Imaging	www.ti.com/video
RFID	www.ti-rfid.com		
OMAP Mobile Processors	www.ti.com/omap	TI E2E Community	e2e.ti.com
Wireless Connectivity	www.ti.com/wirelessconnectivity		

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2012, Texas Instruments Incorporated



Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;

- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);

- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;

- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком):

- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



Телефон: 8 (812) 309-75-97 (многоканальный) Факс: 8 (812) 320-03-32 Электронная почта: ocean@oceanchips.ru Web: http://oceanchips.ru/ Адрес: 198099, г. Санкт-Петербург, ул. Калинина, д. 2, корп. 4, лит. А