

## FEATURES

### High speed

- 80 MHz typical  $-3$  dB bandwidth ( $G = +1$ )
- 75 MHz typical  $-3$  dB bandwidth ( $G = +2$ )
- 1000 V/ $\mu$ s typical slew rate
- 50 ns typical settling time to 0.1% ( $V_{OUT} = 10$  V step)

### Ideal for video applications

- 30 MHz typical 0.1 dB bandwidth ( $G = +2$ ,  $V_S = \pm 15$  V)
- 0.02% typical differential gain ( $V_S = \pm 15$  V)
- 0.04° typical differential phase ( $V_S = \pm 15$  V)

### Low noise

- 2.9 nV/ $\sqrt{\text{Hz}}$  typical input voltage noise
- 13 pA/ $\sqrt{\text{Hz}}$  typical inverting input current noise

### Low power

- 8.0 mA maximum supply current (quiescent)
- 2.1 mA typical supply current (power-down mode)

### High performance disable function

- Turn off time: 100 ns typical
- Break before make guaranteed
- Input to output isolation of 64 dB (off state)

### Flexible operation

- Specified for  $\pm 5$  V and  $\pm 15$  V operation
- $\pm 2.9$  V typical output swing into a 150  $\Omega$  load ( $V_S = \pm 5$  V)

## APPLICATIONS

Professional video cameras

Multimedia systems

NTSC-, PAL-, and SECAM-compatible systems

Video line drivers

ADC or DAC buffers

DC restoration circuits

## GENERAL DESCRIPTION

The AD810 is a composite and HDTV-compatible, current feedback, video operational amplifier, ideal for use in systems such as multimedia, digital tape recorders, and video cameras. The 0.1 dB flatness specification at a bandwidth of 30 MHz ( $G = +2$ ) and the differential gain and phase of 0.02% and 0.04° (NTSC) make the AD810 ideal for any broadcast quality video system. All these specifications are under load conditions of 150  $\Omega$  (one 75  $\Omega$  back terminated cable).

The AD810 is ideal for power sensitive applications such as video cameras, offering a low power supply current of 8.0 mA

## CONNECTION DIAGRAM

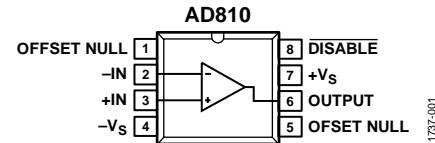


Figure 1.

maximum. The disable feature reduces the power supply current to only 2.1 mA, while the amplifier is not in use, to conserve power. Furthermore, the AD810 is specified over a power supply range of  $\pm 5$  V to  $\pm 15$  V.

The AD810 works well as an ADC or DAC buffer in video systems due to its unity gain ( $G = +1$ )  $-3$  dB bandwidth of 80 MHz. Because the AD810 is a transimpedance amplifier, this bandwidth can be maintained over a wide range of gains while featuring a low noise of 2.9 nV/ $\sqrt{\text{Hz}}$  for wide dynamic range applications.

Rev. B

[Document Feedback](#)

Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties that may result from its use. Specifications subject to change without notice. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices. Trademarks and registered trademarks are the property of their respective owners.

## TABLE OF CONTENTS

Features .....	1	Choice of Feedback Resistor .....	15
Applications .....	1	Printed Circuit Board Layout .....	15
Connection Diagram .....	1	Quality of Coaxial Cable .....	15
General Description .....	1	Power Supply Bypassing .....	15
Revision History .....	2	Power Supply Operating Range.....	15
Specifications.....	3	Offset Nulling .....	16
Absolute Maximum Ratings.....	5	Disable Mode .....	16
Thermal Resistance .....	5	Applications Information .....	17
Maximum Power Dissipation .....	5	Capacitive Loads.....	17
ESD Caution.....	5	Operation As a Video Line Driver .....	18
Pin Configurations and Function Descriptions .....	6	2:1 Video Multiplexer .....	19
Typical Performance Characteristics .....	7	4:1 Multiplexer.....	20
Test Circuits.....	14	Outline Dimensions .....	21
Theory of Operation .....	15	Ordering Guide .....	22
General Design Considerations.....	15		
Achieving Very Flat Gain Response at High Frequency .....	15		

## REVISION HISTORY

### 5/2019—Rev. A to Rev. B

Updated Format.....	Universal
Changed $V_O$ to $V_{OUT}$ and AD810S to 5962-9313201MPA.....	Throughout
Deleted Closed-Loop Gain and Phase vs. Frequency Plot and Differential Gain and Phase vs. Supply Voltage Plot .....	1
Changes to General Description Section .....	1
Changes to Table 1 .....	3
Deleted Figure 2; Renumbered Sequentially.....	4
Changes to Table 2, Maximum Power Dissipation Section .....	5
Added Thermal Resistance Section and Table 3; Renumbered Sequentially .....	5
Added Pin Configurations and Function Descriptions Section, Figure 3, Figure 4, Figure 5, and Table 4; Renumbered Sequentially .....	6
Changes to Figure 6 Caption and Figure 7 Caption.....	7
Changes to Figure 14 Caption and Figure 16 .....	8
Changes to Figure 19.....	9
Added Test Circuits Section.....	14
Moved Figure 45 and Figure 46 .....	14
Changed Choice of Feedback and Gain Resistor Section to Choice of Feedback Resistor Section .....	15

Changes to Achieving Very Flat Gain Response at High Frequency Section, Choice of Feedback Resistor Section, and Power Supply Bypassing Section .....	15
Moved Figure 45 .....	16
Changes to Disable Mode Section.....	16
Added Applications Information Section .....	17
Moved Capacitive Loads Section and Figure 48 to Figure 51 ..	17
Changes to Figure 48 and Figure 50.....	17
Moved Operation As a Video Line Driver Section and Figure 52 to Figure 56.....	18
Change to Figure 54 .....	18
Moved 2:1 Video Multiplexer Section and Figure 57 to Figure 60 .....	19
Changes to Figure 58.....	19
Moved 4:1 Multiplexer Section and Figure 61 to Figure 63 .....	20
Changes to 4:1 Multiplexer Section .....	20
Updated Outline Dimensions .....	21
Changes to Ordering Guide .....	22

### 10/1992—Rev. 0 to Rev. A

## SPECIFICATIONS

$T_A = 25^\circ\text{C}$ , supply voltage ( $V_S$ ) =  $\pm 15\text{ V}$  dc, load resistance ( $R_L$ ) =  $150\ \Omega$ , unless otherwise noted.

Table 1.

Parameter	Test Conditions/Comments	AD810A			5962-9313201MPA <sup>1</sup>			Unit
		Min	Typ	Max	Min	Typ	Max	
DYNAMIC PERFORMANCE	-3 dB Bandwidth	G = +2, feedback resistor ( $R_F$ ) = $715\ \Omega$ , $V_S = \pm 5\text{ V}$	40	50		40	50	MHz
		G = +2, $R_F = 715\ \Omega$ , $V_S = \pm 15\text{ V}$	55	75		55	75	MHz
		G = +1, $R_F = 1000\ \Omega$ , $V_S = \pm 15\text{ V}$	40	80		40	80	MHz
	0.1 dB Bandwidth	G = +10, $R_F = 270\ \Omega$ , $V_S = \pm 15\text{ V}$	50	65		50	65	MHz
		G = +2, $R_F = 715\ \Omega$ , $V_S = \pm 5\text{ V}$	13	22		13	22	MHz
	Full Power Bandwidth	G = +2, $R_F = 715\ \Omega$ , $V_S = \pm 15\text{ V}$	15	30		15	30	MHz
		Output voltage ( $V_{OUT}$ ) = $20\text{ V p-p}$ $R_L = 400\ \Omega$		16		8	16	MHz
	Slew Rate <sup>2</sup>	$R_L = 150\ \Omega$ , $V_S = \pm 5\text{ V}$		350		175	350	V/ $\mu\text{s}$
		$R_L = 400\ \Omega$ , $V_S = \pm 15\text{ V}$		1000		500	1000	V/ $\mu\text{s}$
	Settling Time to 0.1%	10 V step, G = -1		50			50	ns
Settling Time to 0.01%	10 V step, G = -1		125			125	ns	
Differential Gain	f = 3.58 MHz, $V_S = \pm 15\text{ V}$		0.02	0.05		0.02	0.05	%
	f = 3.58 MHz, $V_S = \pm 5\text{ V}$		0.04	0.07		0.04	0.07	%
Differential Phase	f = 3.58 MHz, $V_S = \pm 15\text{ V}$		0.04	0.07		0.04	0.07	Degrees
	f = 3.58 MHz, $V_S = \pm 5\text{ V}$		0.045	0.08		0.045	0.08	Degrees
Total Harmonic Distortion	f = 10 MHz, $V_{OUT} = 2\text{ V p-p}$							
	$R_L = 400\ \Omega$ , G = +2		-61			-61		dBc
INPUT OFFSET VOLTAGE	$V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		1.5	6		1.5	6	mV
	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		2	7.5		4	15	mV
Offset Voltage Drift			7			15	$\mu\text{V}/^\circ\text{C}$	
INPUT BIAS CURRENT								
Negative Input	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		0.7	5		0.8	5	$\mu\text{A}$
Positive Input	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		2	7.5		2	10	$\mu\text{A}$
OPEN-LOOP TRANSRESISTANCE	$T_{MIN}$ to $T_{MAX}$							
	$V_{OUT} = \pm 10\text{ V}$ , $R_L = 400\ \Omega$ , $V_S = \pm 15\text{ V}$	1.0	3.5		1.0	3.5		M $\Omega$
	$V_{OUT} = \pm 2.5\text{ V}$ , $R_L = 100\ \Omega$ , $V_S = \pm 5\text{ V}$	0.3	1.2		0.2	1.0		M $\Omega$
OPEN-LOOP DC VOLTAGE GAIN	$T_{MIN}$ to $T_{MAX}$							
	$V_{OUT} = \pm 10\text{ V}$ , $R_L = 400\ \Omega$ , $V_S = \pm 15\text{ V}$	86	100		80	100		dB
	$V_{OUT} = \pm 2.5\text{ V}$ , $R_L = 100\ \Omega$ , $V_S = \pm 5\text{ V}$	76	88		72	88		dB
COMMON-MODE REJECTION	$T_{MIN}$ to $T_{MAX}$							
Offset Voltage ( $V_{OS}$ )	Common-mode voltage ( $V_{CM}$ ) = $\pm 12\text{ V}$ , $V_S = \pm 15\text{ V}$	56	64		56	64		dB
	$V_{CM} = \pm 2.5\text{ V}$ , $V_S = \pm 5\text{ V}$	52	60		50	60		dB
Input Bias Current	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		0.1	0.4	-0.4	0.1	+0.4	$\mu\text{A/V}$
POWER SUPPLY REJECTION								
$V_{OS}$	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 4.5\text{ V}$ to $\pm 18\text{ V}$	65	72		60	72		dB
	$T_{MIN}$ to $T_{MAX}$		0.05	0.3	-0.3	0.05	+0.3	$\mu\text{A/V}$
INPUT VOLTAGE NOISE	f = 1 kHz, $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		2.9			2.9		nV/ $\sqrt{\text{Hz}}$
INPUT CURRENT NOISE	Negative input current ( $-I_{IN}$ ), f = 1 kHz, $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		13			13		pA/ $\sqrt{\text{Hz}}$
	Positive input current ( $+I_{IN}$ ), f = 1 kHz, $V_S = \pm 5\text{ V}$ and $\pm 15\text{ V}$		1.5			1.5		pA/ $\sqrt{\text{Hz}}$
INPUT COMMON-MODE VOLTAGE RANGE	$V_S = \pm 5\text{ V}$	$\pm 2.5$	$\pm 3.0$		$\pm 2.5$	$\pm 3$		V
	$V_S = \pm 15\text{ V}$	$\pm 12$	$\pm 13$		$\pm 12$	$\pm 13$		V

Parameter	Test Conditions/Comments	AD810A			5962-9313201MPA <sup>1</sup>			Unit
		Min	Typ	Max	Min	Typ	Max	
OUTPUT CHARACTERISTICS								
Output Voltage Swing <sup>3</sup>	$R_L = 150 \Omega$ , $T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5 V$	$\pm 2.5$	$\pm 2.9$		$\pm 2.5$	$\pm 2.9$		V
	$R_L = 400 \Omega$ , $V_S = \pm 15 V$	$\pm 12.5$	$\pm 12.9$		$\pm 12.5$	$\pm 12.9$		V
	$R_L = 400 \Omega$ , $T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 15 V$	$\pm 12$			$\pm 12$			V
Short-Circuit Current			150			150		mA
Output Current	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5 V$ and $\pm 15 V$	40	60		30	60		mA
OUTPUT RESISTANCE	Open loop (5 MHz)		15			15		$\Omega$
INPUT CHARACTERISTICS								
Input Resistance	Positive input	2.5	10		2.5	10		M $\Omega$
	Negative input		40			40		$\Omega$
Input Capacitance	Positive input		2			2		pF
DISABLE CHARACTERISTICS <sup>4</sup>								
Off Isolation	$f = 5 \text{ MHz}$ , see Figure 59		64			64		dB
Off Output Resistance	See Figure 15, $R_G$ is gain resistor		$(R_F + R_G)    13 \text{ pF}$			$(R_F + R_G)    13 \text{ pF}$		$\Omega$
Turn On Time <sup>5</sup>	Output impedance ( $Z_{OUT}$ ) = low, see Figure 59		170			170		ns
Turn Off Time	$Z_{OUT} = \text{high}$		100			100		ns
$\overline{\text{DISABLE}}$ Pin Current	$\overline{\text{DISABLE}}$ pin = 0 V, $V_S = \pm 5 V$		50	75		50	75	$\mu\text{A}$
	$\overline{\text{DISABLE}}$ pin = 0 V, $V_S = \pm 15 V$		290	400		290	400	$\mu\text{A}$
Minimum $\overline{\text{DISABLE}}$ Pin Current to Disable	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5 V$ and $\pm 15 V$		30		10	30	40	$\mu\text{A}$
POWER SUPPLY								
Operating Range	$25^\circ\text{C}$ to $T_{MAX}$	$\pm 2.5$		$\pm 18$	$\pm 2.5$		$\pm 18$	V
	$T_{MIN}$	$\pm 3.0$		$\pm 18$	$\pm 3.5$		$\pm 18$	V
Quiescent Current	$V_S = \pm 5 V$		6.7	7.5		6.7	7.5	mA
	$V_S = \pm 15 V$		6.8	8.0		6.8	8.0	mA
	$T_{MIN}$ to $T_{MAX}$ , $V_S = \pm 5 V$ and $\pm 15 V$		8.3	10.0		9	11.0	mA
Power-Down Current	$V_S = \pm 5 V$		1.8	2.3		1.8	2.3	mA
	$V_S = \pm 15 V$		2.1	2.8		2.1	2.8	mA
TEMPERATURE								
Operating Range ( $T_{MIN}$ to $T_{MAX}$ )		-40		+85	-55		+125	$^\circ\text{C}$

<sup>1</sup> See the Analog Devices military data sheet for 883B specifications.

<sup>2</sup> Slew rate measurement is based on 10% to 90% rise time with the amplifier configured for a gain of -10.

<sup>3</sup> Voltage swing is defined as useful operating range, not the saturation range.

<sup>4</sup> Disable guaranteed break before make.

<sup>5</sup> Turn on time is defined with  $\pm 5 V$  supplies using complementary output CMOS to drive the disable pin.

## ABSOLUTE MAXIMUM RATINGS

Table 2.

Parameter	Rating
Supply Voltage	±18 V
Internal Power Dissipation	See Figure 2
Output Short-Circuit Duration <sup>1</sup>	See Figure 2
Common-Mode Input Voltage	±V <sub>S</sub>
Differential Input Voltage	±6 V
Storage Temperature Range	
PDIP	−65°C to +125°C
CERDIP	−65°C to +150°C
SOIC_N	−65°C to +125°C
Operating Temperature Range	
AD810A	−40°C to +85°C
5962-9313201MPA	−55°C to +125°C
Junction Temperature	
AD810A	145°C
5962-9313201MPA	175°C
Lead Temperature Range (Soldering 60 sec)	300°C

<sup>1</sup> Internal short-circuit protection may not be sufficient to guarantee that the maximum junction temperature is not exceeded under all conditions.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

### THERMAL RESISTANCE

Thermal performance is directly linked to printed circuit board (PCB) design and operating environment. Careful attention to PCB thermal design is required.

$\theta_{JA}$  is the natural convection junction to ambient thermal resistance measured in a one-cubic foot sealed enclosure.

Table 3. Thermal Resistance

Package Type	$\theta_{JA}$	Unit
N-8	90	°C/W
Q-8	110	°C/W
R-8	150	°C/W

### MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD810 is limited by the associated rise in junction temperature. To ensure proper operation, it is important to observe the derating curves in Figure 2.

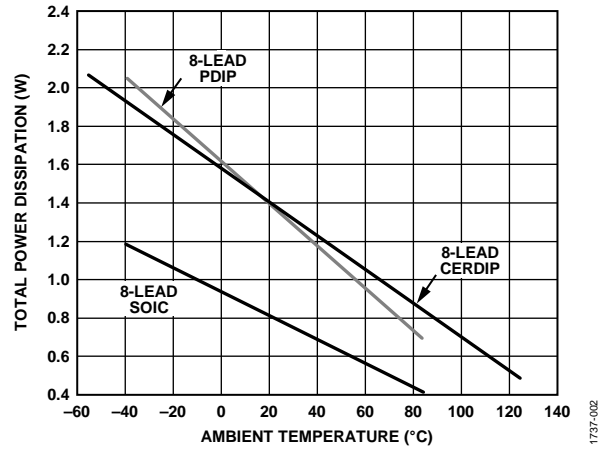


Figure 2. Total Power Dissipation vs. Ambient Temperature

### ESD CAUTION



**ESD (electrostatic discharge) sensitive device.** Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

# PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

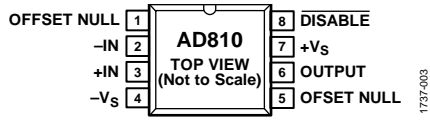


Figure 3. 8-Lead PDIP Pin Configuration

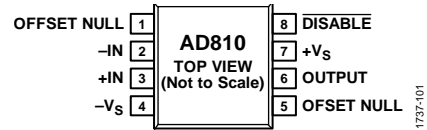


Figure 5. 8-Lead SOIC Pin Configuration

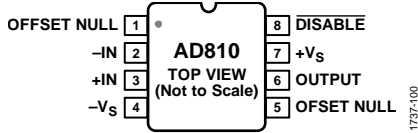


Figure 4. 8-Lead CERDIP Pin Configuration

Table 4. Pin Function Descriptions

Pin No.	Mnemonic	Description
1, 5	OFFSET NULL	Inverting Input Offset Null Connection. See Figure 47.
2	-IN	Inverting Input.
3	+IN	Noninverting Input.
4	-Vs	Negative Supply Voltage.
6	OUTPUT	Output.
7	+Vs	Positive Supply Voltage.
8	DISABLE	Disable (Active Low).

### TYPICAL PERFORMANCE CHARACTERISTICS

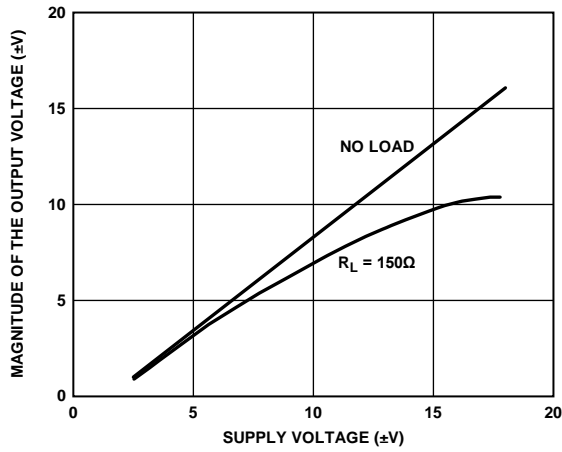


Figure 6. Magnitude of the Output Voltage vs. Supply Voltage

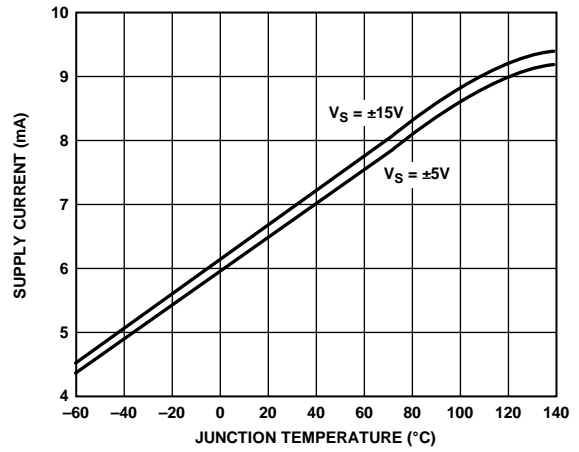


Figure 9. Supply Current vs. Junction Temperature

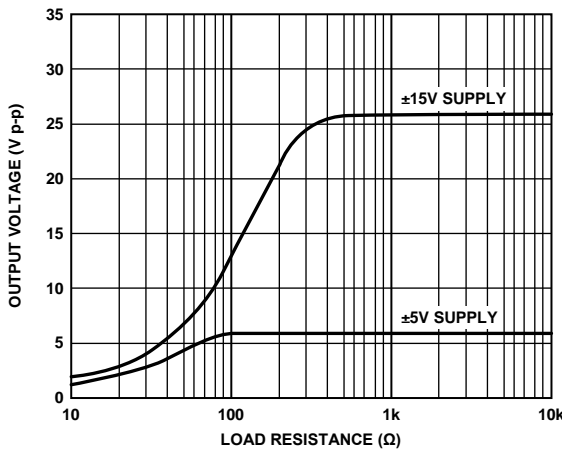


Figure 7. Output Voltage vs. Load Resistance

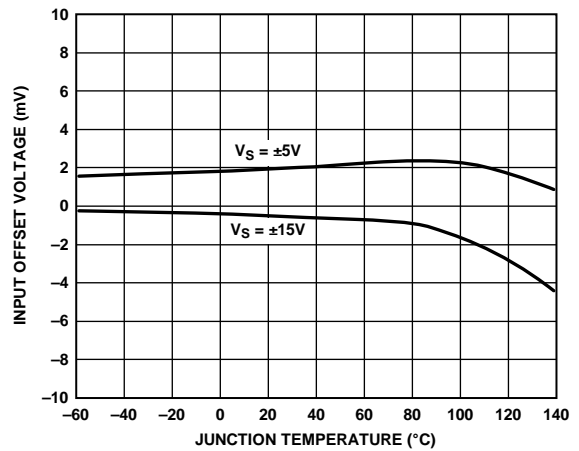


Figure 10. Input Offset Voltage vs. Junction Temperature

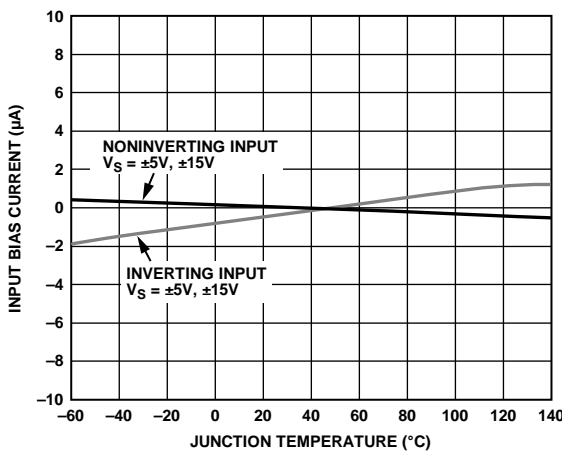


Figure 8. Input Bias Current vs. Junction Temperature

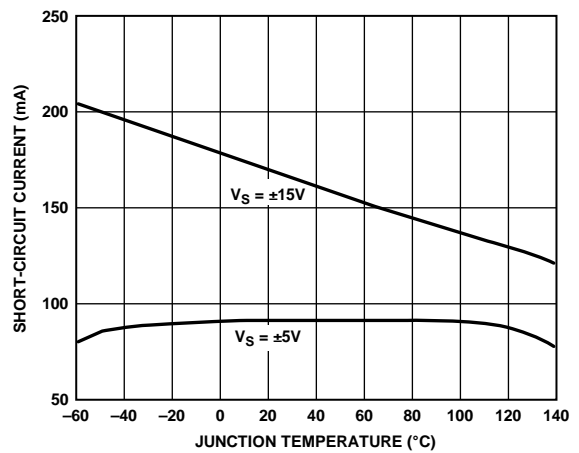


Figure 11. Short-Circuit Current vs. Junction Temperature

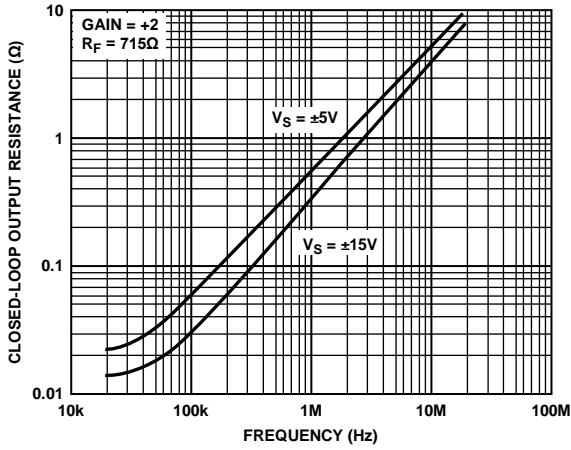


Figure 12. Closed-Loop Output Resistance vs. Frequency

1737-010

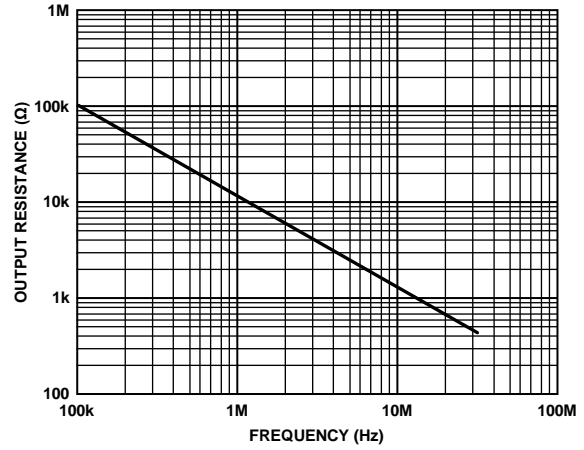


Figure 15. Output Resistance vs. Frequency, Disabled State

1737-013

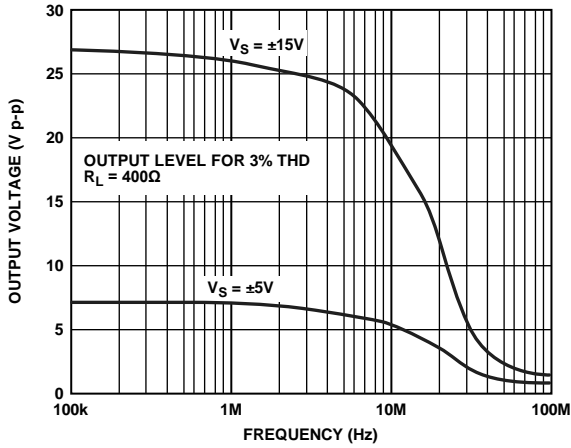


Figure 13. Large Signal Frequency Response

1737-011

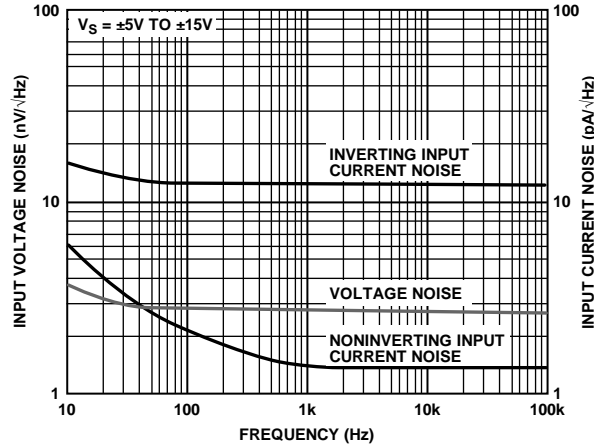


Figure 16. Input Voltage Noise and Input Current Noise vs. Frequency

1737-014

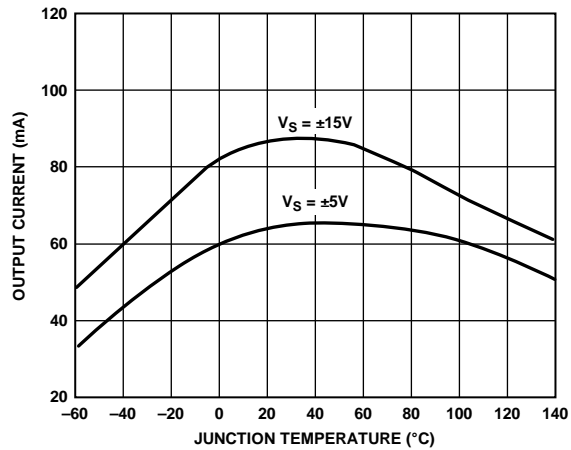


Figure 14. Output Current vs. Junction Temperature

1737-012

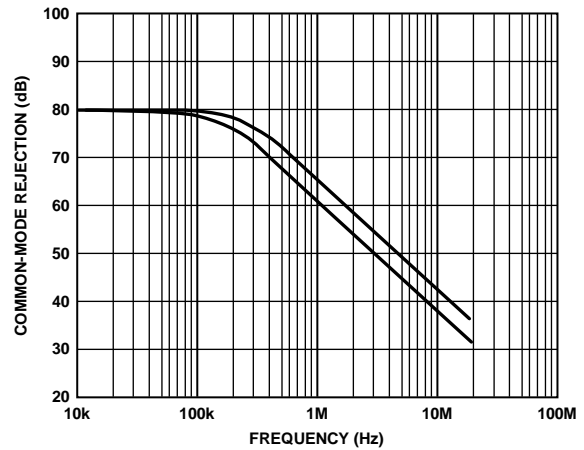


Figure 17. Common-Mode Rejection vs. Frequency

1737-015



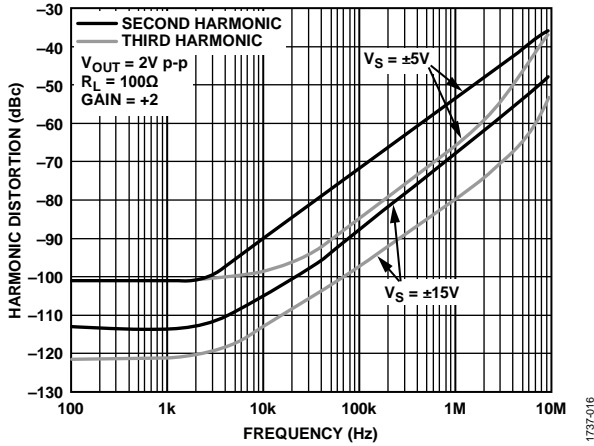


Figure 18. Harmonic Distortion vs. Frequency ( $R_L = 100\ \Omega$ )

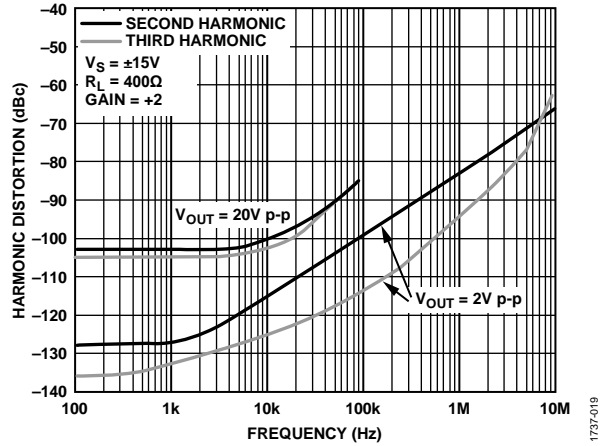


Figure 21. Harmonic Distortion vs. Frequency ( $R_L = 400\ \Omega$ )

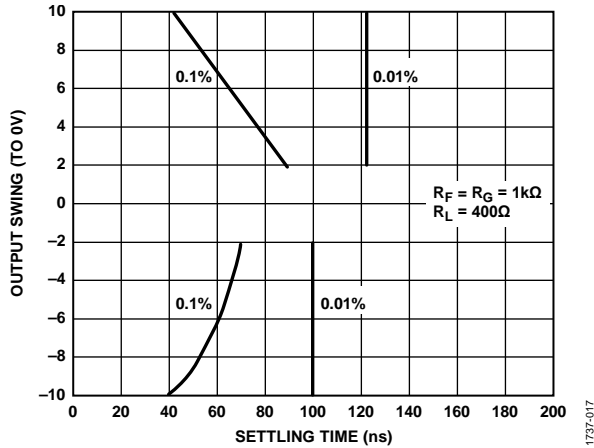


Figure 19. Output Swing (to 0 V) vs. Settling Time at Various Error Levels

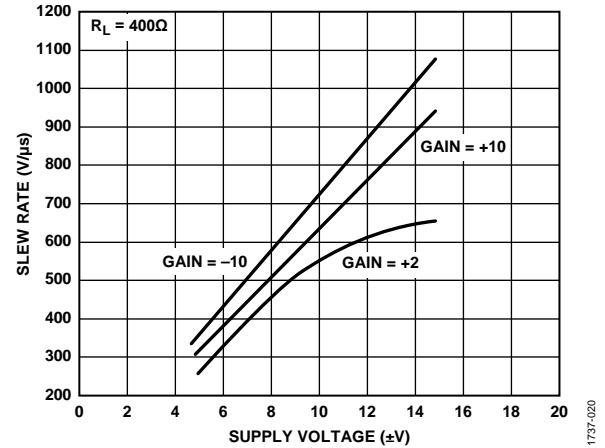


Figure 22. Slew Rate vs. Supply Voltage

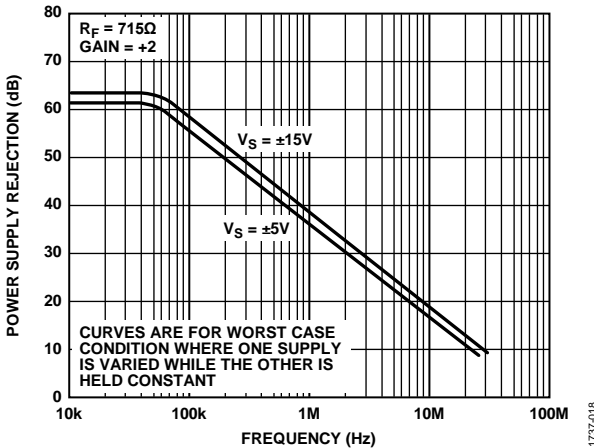


Figure 20. Power Supply Rejection vs. Frequency

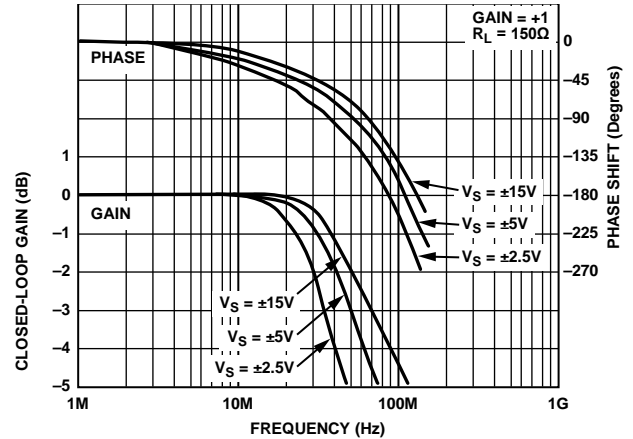


Figure 23. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = +1$ ,  $R_F = 1\text{k}\ \Omega$  for  $\pm 15\text{V}$ ,  $910\ \Omega$  for  $\pm 5\text{V}$  and  $\pm 2.5\text{V}$

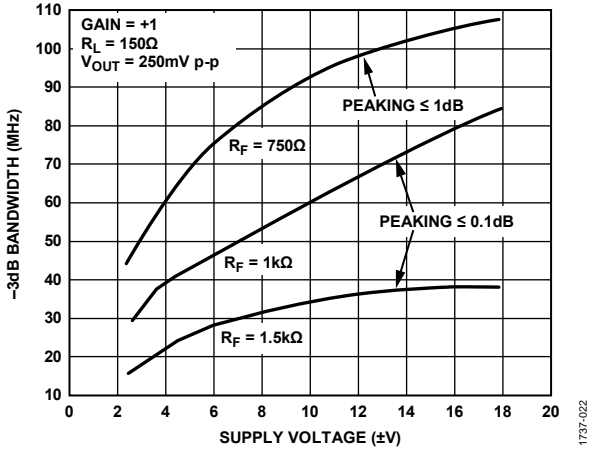


Figure 24. -3 dB Bandwidth vs. Supply Voltage, Gain = +1,  $R_L = 150 \Omega$

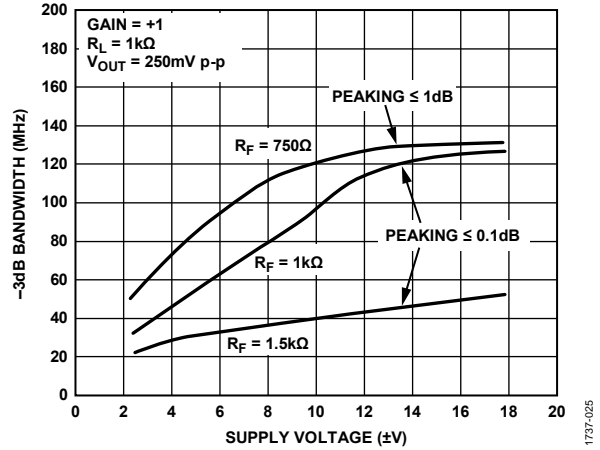


Figure 27. -3 dB Bandwidth vs. Supply Voltage,  $G = +1$ ,  $R_L = 1 k\Omega$

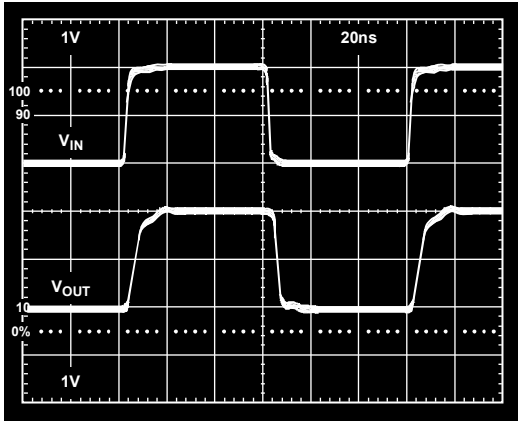


Figure 25. Small Signal Pulse Response, Gain = +1,  $R_F = 1 k\Omega$ ,  $R_L = 150 \Omega$ ,  $V_S = \pm 15 V$

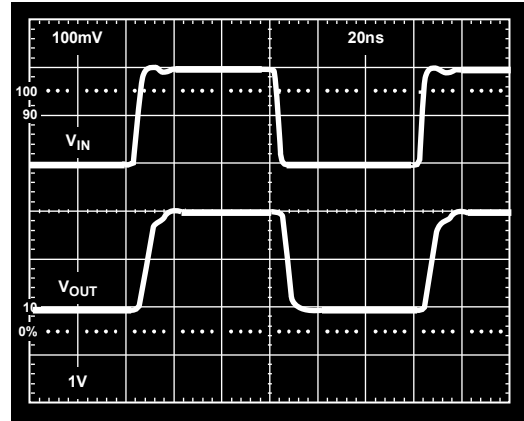


Figure 28. Small Signal Pulse Response, Gain = +10,  $R_F = 442 \Omega$ ,  $R_L = 150 \Omega$ ,  $V_S = \pm 15 V$

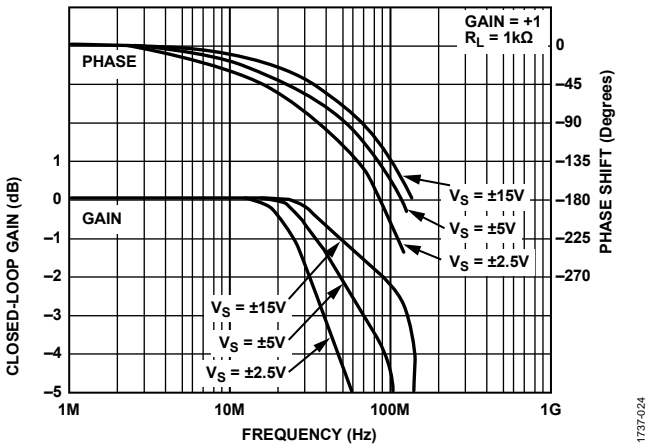


Figure 26. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = +1$ ,  $R_F = 1 k\Omega$  for  $\pm 15 V$ ,  $910 \Omega$  for  $\pm 5 V$  and  $\pm 2.5 V$

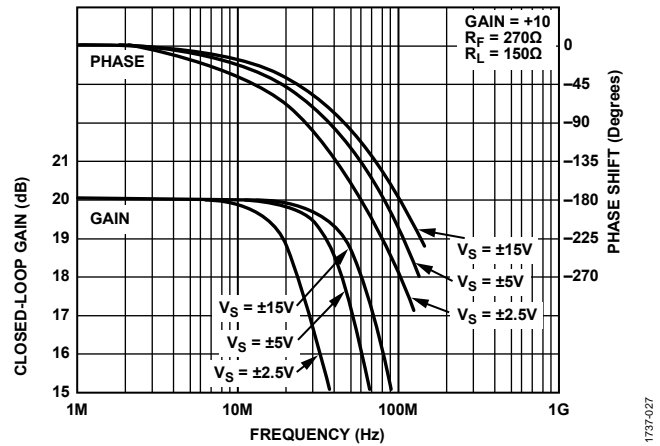


Figure 29. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = +10$ ,  $R_L = 150 \Omega$

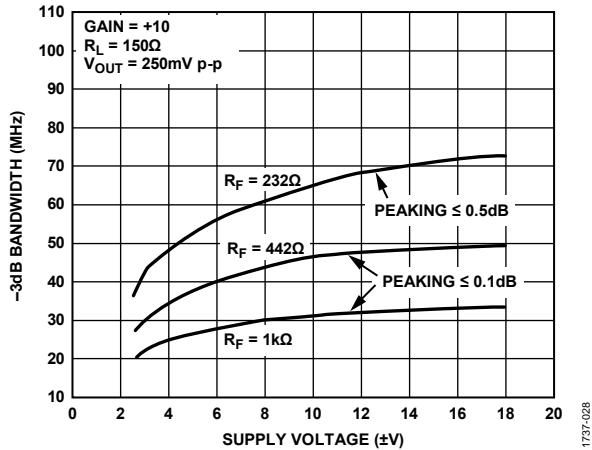


Figure 30. -3 dB Bandwidth vs. Supply Voltage, Gain = +10,  $R_L = 150\ \Omega$

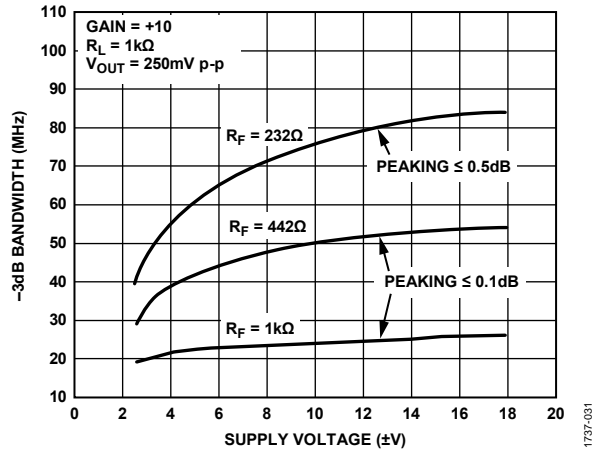


Figure 33. -3 dB Bandwidth vs. Supply Voltage, Gain = +10,  $R_L = 1\ k\Omega$

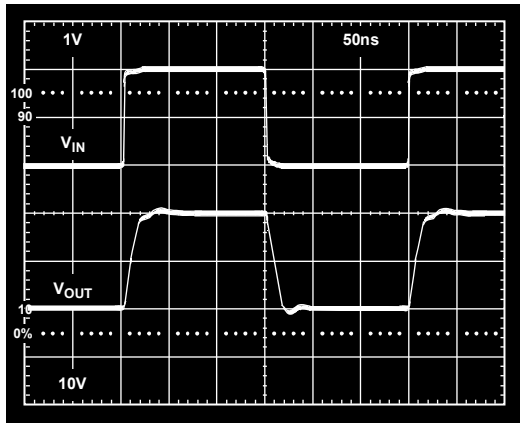


Figure 31. Large Signal Pulse Response, Gain = +10,  $R_F = 442\ \Omega$ ,  $R_L = 400\ \Omega$ ,  $V_S = \pm 15\ V$

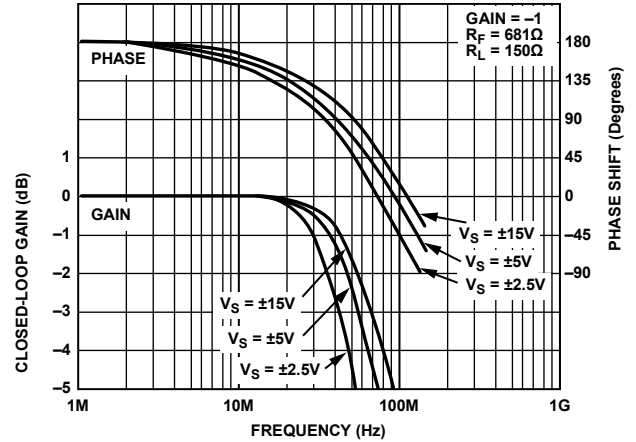


Figure 34. Closed-Loop Gain and Phase Shift vs. Frequency  $G = -1$ ,  $R_L = 150\ \Omega$ ,  $R_F = 681\ \Omega$  for  $\pm 15\ V$ ,  $620\ \Omega$  for  $\pm 5\ V$  and  $\pm 2.5\ V$

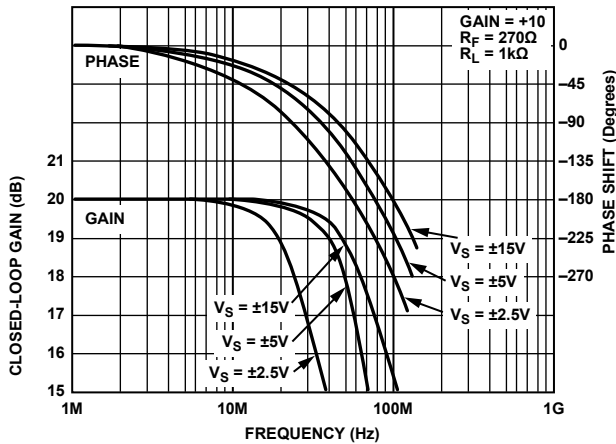


Figure 32. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = +10$ ,  $R_L = 1\ k\Omega$

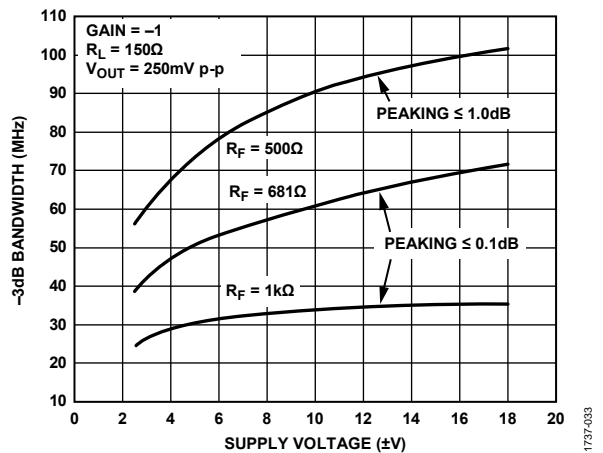


Figure 35. -3 dB Bandwidth vs. Supply Voltage, Gain = -1,  $R_L = 150\ \Omega$

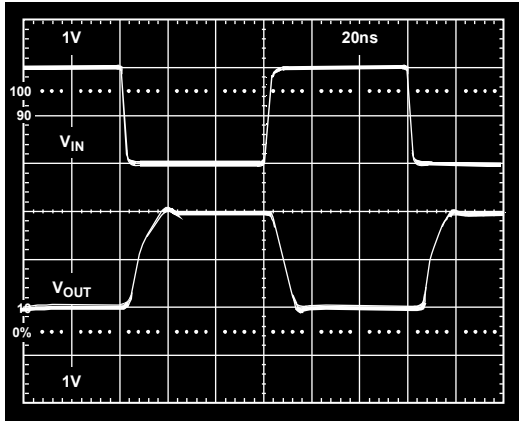


Figure 36. Small Signal Pulse Response, Gain = -1,  $R_F = 681 \Omega$ ,  $R_L = 150 \Omega$ ,  $V_S = \pm 5 V$

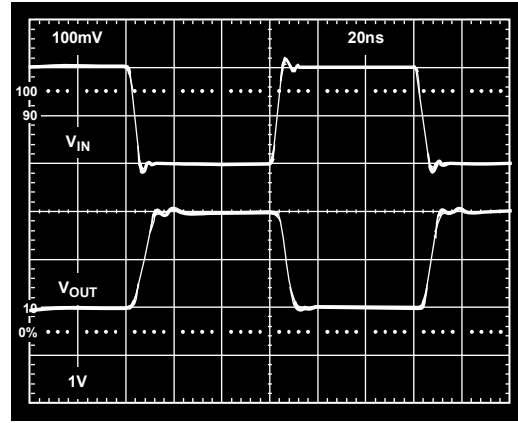


Figure 39. Small Signal Pulse Response, Gain = -10,  $R_F = 442 \Omega$ ,  $R_L = 150 \Omega$ ,  $V_S = \pm 15 V$

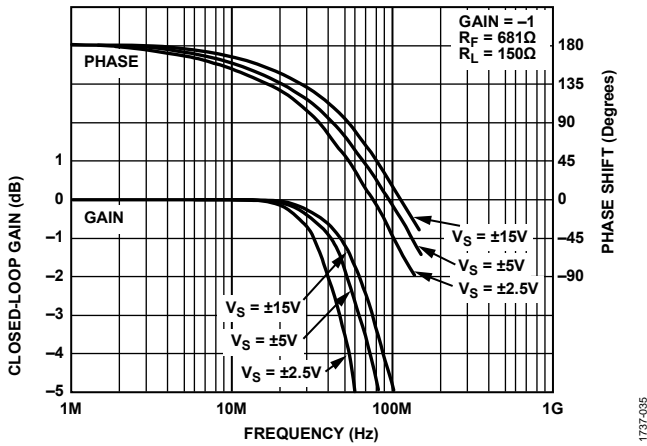


Figure 37. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = -1$ ,  $R_L = 1 k\Omega$ ,  $R_F = 681 \Omega$  for  $V_S = \pm 15 V$ ,  $620 \Omega$  for  $\pm 5 V$  and  $\pm 2.5 V$

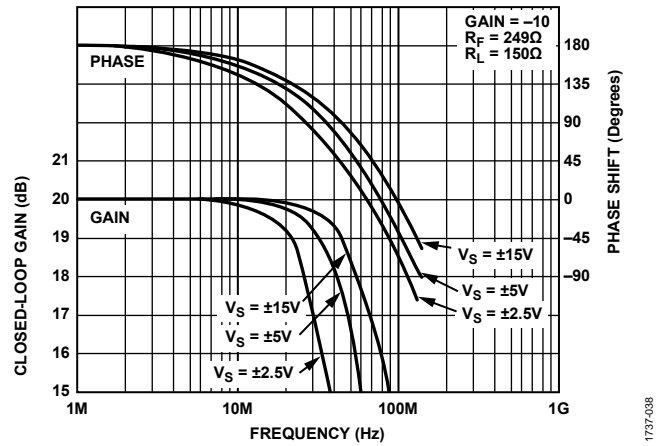


Figure 40. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = -10$ ,  $R_L = 150 \Omega$

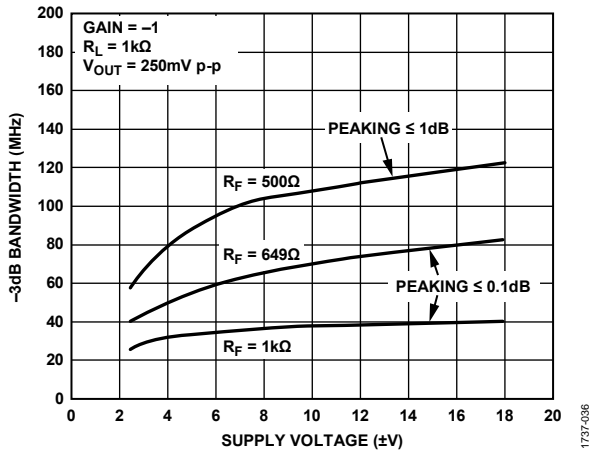


Figure 38. -3 dB Bandwidth vs. Supply Voltage, Gain = -1,  $R_L = 1 k\Omega$

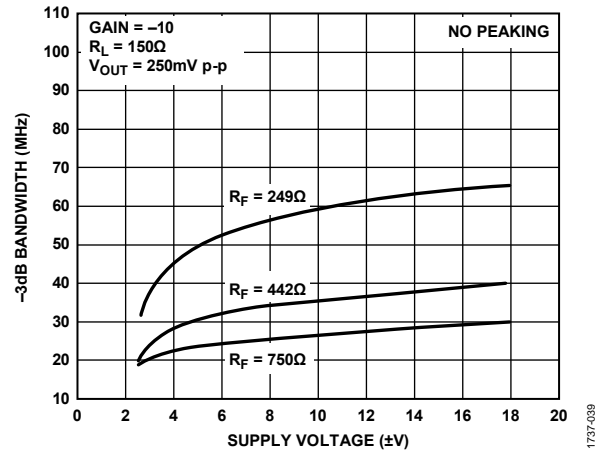


Figure 41. -3 dB Bandwidth vs. Supply Voltage,  $G = -10$ ,  $R_L = 150 \Omega$

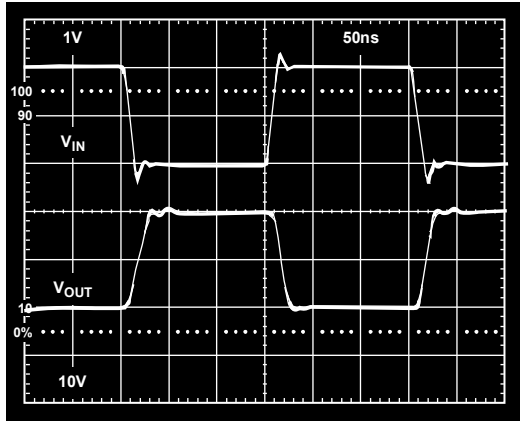


Figure 42. Large Signal Pulse Response, Gain = -10,  $R_F = 442\ \Omega$ ,  $R_L = 400\ \Omega$ ,  $V_S = \pm 15\ V$

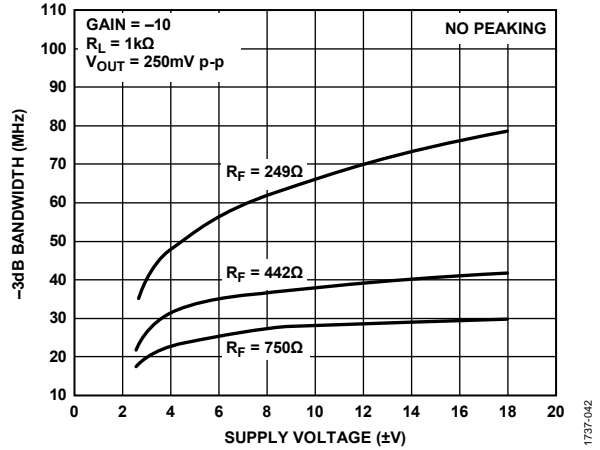


Figure 44. -3 dB Bandwidth vs. Supply Voltage,  $G = -10$ ,  $R_L = 1\ k\Omega$

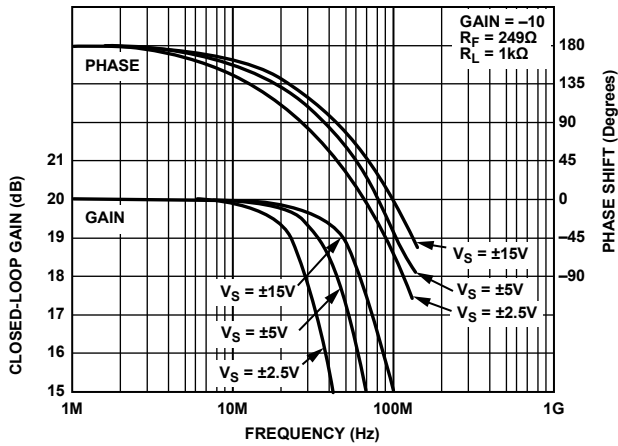


Figure 43. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = -10$ ,  $R_L = 1\ k\Omega$

TEST CIRCUITS

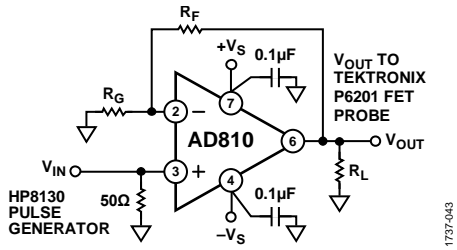


Figure 45. Noninverting Amplifier Connection

1737-043

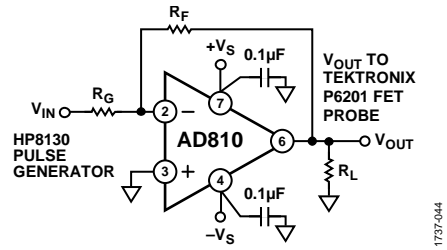


Figure 46. Inverting Amplifier Connection

1737-044

## THEORY OF OPERATION

### GENERAL DESIGN CONSIDERATIONS

The AD810 is a current feedback amplifier optimized for use in high performance video and data acquisition systems. Because the AD810 uses a current feedback architecture, its closed-loop bandwidth depends on the value of the feedback resistor. Table 5 and Table 6 list recommended resistor values for some useful closed-loop gains and supply voltages. As shown in Table 5 and Table 6, the closed-loop bandwidth is not a strong function of gain, as it is for a voltage feedback amplifier. The recommended resistor values results in maximum bandwidths with less than 0.1 dB of peaking in the gain vs. frequency response.

The  $-3$  dB bandwidth is also somewhat dependent on the power supply voltage. Lowering the supplies increases the values of internal capacitances, reducing the bandwidth. To compensate for this reduction, smaller values of feedback resistor are sometimes used at lower supply voltages. The characteristic curves in Figure 23 and Figure 24 illustrate that bandwidths of over 100 MHz on 30 V total supplies and over 50 MHz on 5 V total supplies can be achieved.

**Table 5.  $-3$  dB Bandwidth vs. Closed-Loop Gain and Resistance Values ( $R_L = 150 \Omega$ ),  $V_S = \pm 15$  V**

Closed-Loop Gain	$R_F$	$R_G$	$-3$ dB Bandwidth (MHz)
+1	1 k $\Omega$	Open	80
+2	715 $\Omega$	715 $\Omega$	75
+10	270 $\Omega$	30 $\Omega$	65
-1	681 $\Omega$	681 $\Omega$	70
-10	249 $\Omega$	24.9 $\Omega$	65

**Table 6.  $-3$  dB Bandwidth vs. Closed-Loop Gain and Resistance Values ( $R_L = 150 \Omega$ ),  $V_S = \pm 5$  V**

Closed-Loop Gain	$R_F$	$R_G$	$-3$ dB Bandwidth (MHz)
+1	910 $\Omega$	Open	50
+2	715 $\Omega$	715 $\Omega$	50
+10	270 $\Omega$	30 $\Omega$	50
-1	620 $\Omega$	620 $\Omega$	55
-10	249 $\Omega$	24.9 $\Omega$	50

### ACHIEVING VERY FLAT GAIN RESPONSE AT HIGH FREQUENCY

Achieving and maintaining gain flatness of less than 0.1 dB above 10 MHz is not difficult if the recommended resistor values are used. Additionally, consider feedback resistor selection, PCB layout, coaxial cable quality, power supply bypassing and operating range, and offset nulling to ensure consistently optimal results.

### CHOICE OF FEEDBACK RESISTOR

Because the 3 dB bandwidth depends on the feedback resistor, the fine scale flatness varies to some extent with feedback resistor tolerance. It is recommended that resistors with a 1% tolerance be used to maintain exceptional flatness through high volume production.

### PRINTED CIRCUIT BOARD LAYOUT

As with all wideband amplifiers, PCB parasitics can affect the overall closed-loop performance. Most important are stray capacitances at the output and inverting input nodes. (An added capacitance of 2 pF between the inverting input and ground adds about 0.2 dB of peaking in the gain of 2 response, and increase the bandwidth to 105 MHz). Leave space (3/16 inches is sufficient) around the signal lines to minimize coupling. Also, keep signal lines connecting the feedback and gain resistors short enough so that their associated inductance does not cause high frequency gain errors. Line lengths less than 1/4 inches are recommended.

### QUALITY OF COAXIAL CABLE

Optimum flatness when driving a coaxial cable is possible only when the driven cable is terminated at each end with a resistor matching its characteristic impedance. With an ideal coaxial cable, the resulting flatness is not affected by the length of the cable. Although outstanding results can be achieved using inexpensive cables, some variation in flatness due to varying cable lengths is to be expected.

### POWER SUPPLY BYPASSING

Adequate power supply bypassing can be critical when optimizing the performance of a high frequency circuit. Inductance in the power supply leads can contribute to resonant circuits that produce peaking in the amplifier response. Although the recommended 0.1  $\mu$ F power supply bypass capacitors are sufficient in most applications, more elaborate bypassing (such as using two paralleled capacitors) may be required in some cases. In addition, if large current transients must be delivered to the load, bypass capacitors (typically greater than 1  $\mu$ F) are required to optimize settling time and lowest distortion.

### POWER SUPPLY OPERATING RANGE

The AD810 operates with supplies from  $\pm 18$  V down to about  $\pm 2.5$  V. On  $\pm 2.5$  V supplies, the low distortion output voltage swing is greater than 1 V p-p. Single-supply operation can be achieved by biasing the input common-mode voltage at the supply midpoint.

## OFFSET NULLING

A 10 k $\Omega$  potentiometer connected between Pin 1 and Pin 5, with its wiper connected to +V<sub>S</sub> can be used to trim out the inverting input current (with about  $\pm 20$   $\mu$ A of range). For closed-loop gains above about 5, this configuration may not be sufficient to trim the output offset voltage to zero. Tie the potentiometer wiper to ground through a large value resistor (50 k $\Omega$  for  $\pm 5$  V supplies, 150 k $\Omega$  for  $\pm 15$  V supplies) to trim the output to zero at high closed-loop gains.

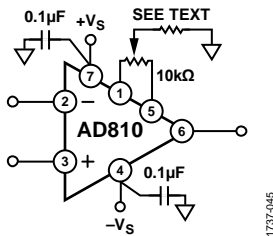


Figure 47. Offset Null Configuration

## DISABLE MODE

By pulling the voltage on Pin 8 to ground (0 V), the AD810 can be put into a disabled state. In this condition, the supply current drops to less than 2.8 mA, the output becomes high impedance, and there is a high level of isolation from input to output. In the case of a line driver, for example, the output impedance is about the same as for a 1.5 k $\Omega$  resistor (the feedback plus gain resistors) in parallel with a 13 pF capacitor (due to the output) and the input to output isolation is greater than 65 dB at 1 MHz.

Leaving the disable pin disconnected (floating) keeps the AD810 operational in the enabled state.

The input impedance of the disable pin is about 35 k $\Omega$  in parallel with a few pF. When grounded, about 50  $\mu$ A flows out of the DISABLE pin for  $\pm 5$  V supplies. If driven by complementary output CMOS logic, the disable time (until the output goes high impedance) is about 100 ns and the enable time (to low impedance output) is about 170 ns on  $\pm 5$  V supplies. The enable time can be extended to about 750 ns by using open-drain logic.

When operated on  $\pm 15$  V supplies, the AD810 disable pin can be driven by open-drain logic. In this case, adding a 10 k $\Omega$  pull-up resistor from the DISABLE pin to the positive supply decreases the enable time to about 150 ns. If there is a nonzero voltage present on the amplifier output at the time the device is switched to the disabled state, some additional decay time is required for the output voltage to decrease to zero. The total time for the output to go to zero is generally about 250 ns and is somewhat dependent on the load impedance.

In cases where the amplifier is driving a high impedance load, the input to output isolation decreases significantly if the input signal is greater than about 1.2 V p-p. The isolation can be restored back to the 65 dB level by adding an extra load (for example, 150  $\Omega$ ) at the amplifier output. This additional load attenuates the feedthrough signal. (This decreased isolation is not an issue for multiplexer applications where the outputs of multiple AD810 devices are tied together as long as at least one channel is in the on state.)



# APPLICATIONS INFORMATION

## CAPACITIVE LOADS

When used with the appropriate feedback resistor, the AD810 can drive capacitive loads exceeding 1000 pF directly without oscillation. By using the curves in Figure 50 to choose the resistor value, less than 1 dB of peaking can easily be achieved without sacrificing much bandwidth. Note that the curves in Figure 50 were generated for the case of a 10 kΩ load resistor. For smaller load resistances, the peaking is less than indicated by Figure 50.

Another method of compensating for large load capacitances is to insert a resistor in series ( $R_S$ ) with the loop output, as shown in Figure 48. In most cases, less than 50 Ω is all that is needed to achieve an extremely flat gain response.

Figure 49 to Figure 51 illustrate the outstanding performance that can be achieved when driving a 1000 pF capacitor.

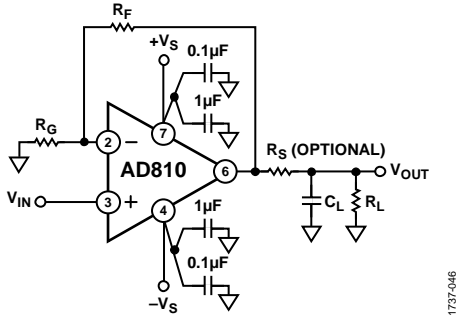


Figure 48. Circuit Options for Driving a Large Capacitive Load

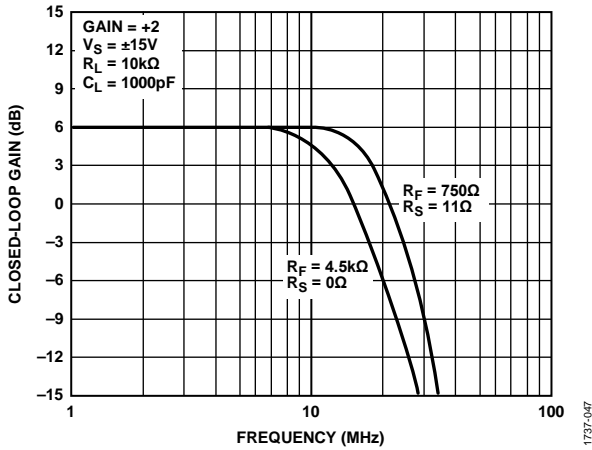


Figure 49. Performance Comparison of Two Methods for Driving a Large Capacitive Load

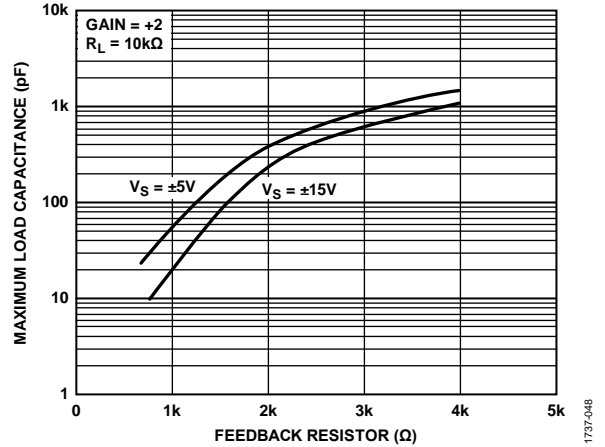


Figure 50. Maximum Load Capacitance vs. Feedback Resistor, Peaking < 1 dB

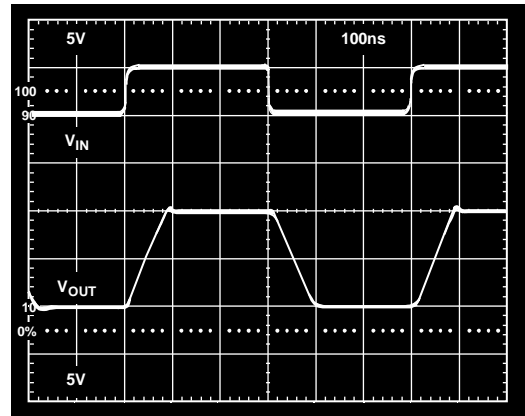


Figure 51. AD810 Driving a 1000 pF Load, Gain = +2,  $R_F = 750 \Omega$ ,  $R_S = 11 \Omega$ ,  $R_L = 10 \text{ k}\Omega$

**OPERATION AS A VIDEO LINE DRIVER**

The AD810 is designed to offer outstanding performance at closed-loop gains of 1 or greater. At a gain of 2, the low differential gain and phase errors and wide  $-0.1$  dB bandwidth are nearly independent of supply voltage and load (as shown in Figure 53 through Figure 55) making the AD810 an excellent video line driver.

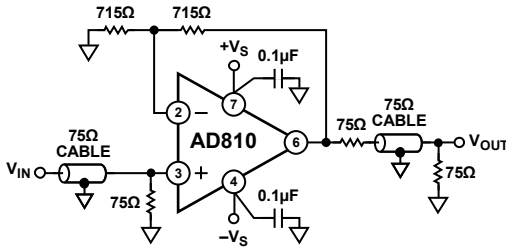


Figure 52. Video Line Driver Operating at Gain = +2

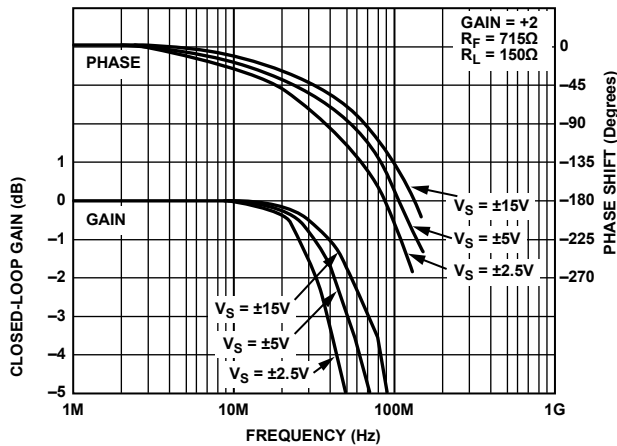


Figure 53. Closed-Loop Gain and Phase Shift vs. Frequency,  $G = +2$ ,  $R_L = 150\Omega$ ,  $R_F = 715\Omega$

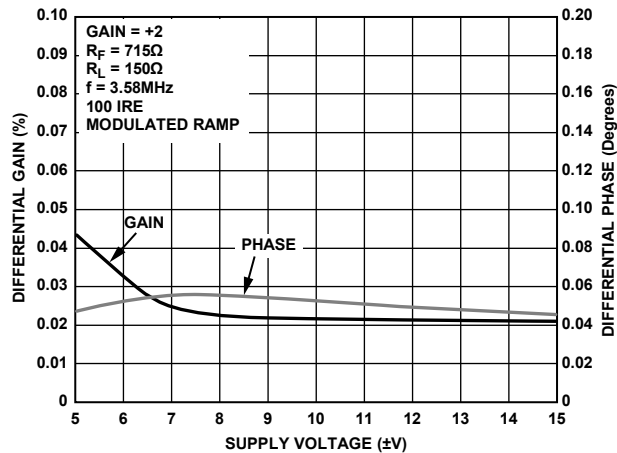


Figure 54. Differential Gain and Differential Phase vs. Supply Voltage

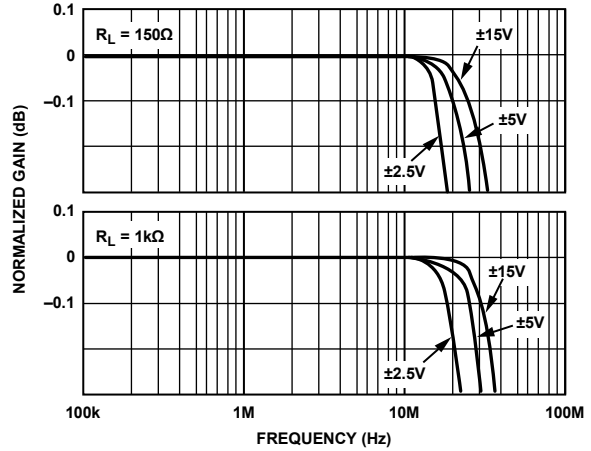


Figure 55. Normalized Gain vs. Frequency for Various Supply Voltages, Gain = +2,  $R_F = 715\Omega$

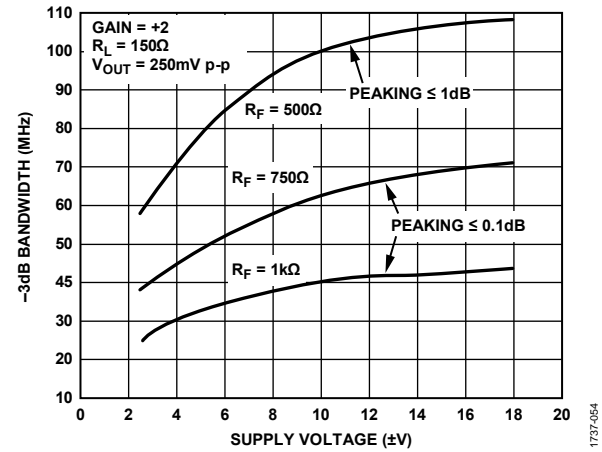


Figure 56.  $-3$  dB Bandwidth vs. Supply Voltage,  $G = +2$ ,  $R_L = 150\Omega$

### 2:1 VIDEO MULTIPLEXER

The outputs of two AD810 devices can be wired together to form a 2:1 mux without degrading the flatness of the gain response. Figure 59 shows a recommended configuration that results in  $-0.1$  dB bandwidth of 20 MHz and off channel isolation of 77 dB at 10 MHz on  $\pm 5$  V supplies. The time to switch between channels is about  $0.75 \mu\text{s}$  when the DISABLE pins are driven by open-drain output logic. Adding pull-up resistors to the logic outputs or using complementary output logic (such as the 74HC04) reduces the switching time to about 180 ns. The switching time is only slightly affected by the signal level.

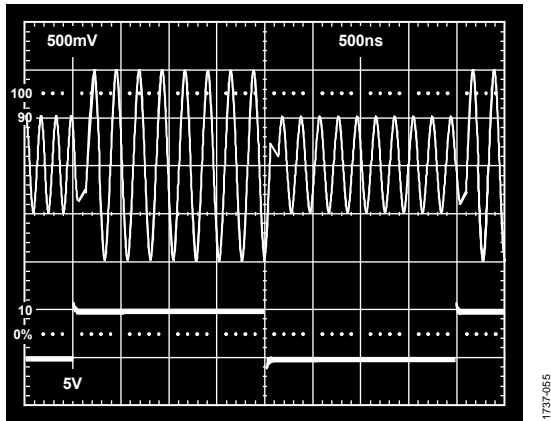


Figure 57. Channel Switching Time for the 2:1 Mux

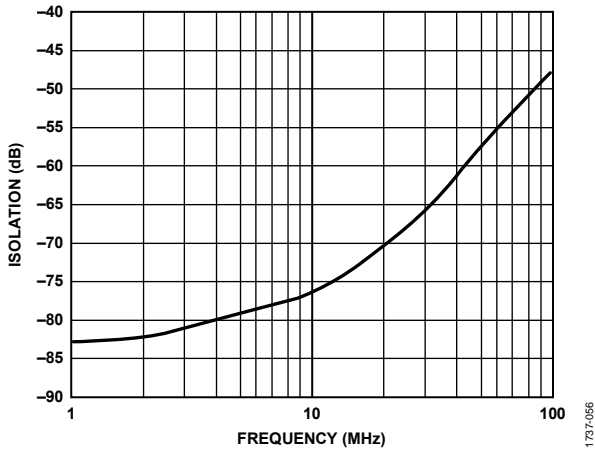


Figure 58. Isolation vs. Frequency for 2:1 Mux, Off Channel

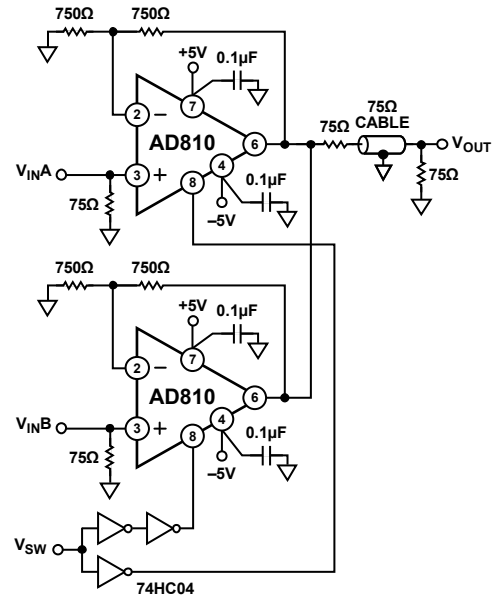


Figure 59. A Fast Switching 2:1 Video Mux

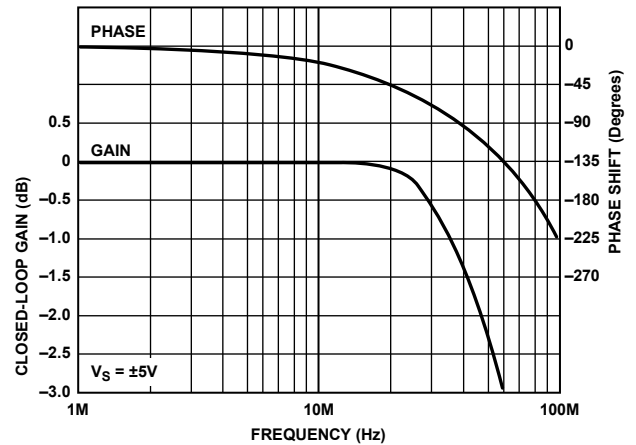


Figure 60. Closed-Loop Gain and Phase Shift vs. Frequency for 2:1 Mux, On Channel

**4:1 MULTIPLEXER**

A multiplexer of arbitrary size can be formed by combining the desired number of AD810 devices together with the appropriate selection logic. The schematic in Figure 63 shows a recommendation for a 4:1 mux, which can be useful for driving a high impedance such as the input to a video ADC. The output series resistors effectively compensate for the combined output capacitance of the off channels plus the input capacitance of the ADC while maintaining wide bandwidth. In the case illustrated in Figure 63, the  $-0.1$  dB bandwidth is about 20 MHz with no peaking. Switching time and off channel isolation (for the 4:1 mux) are about 250 ns and 60 dB at 10 MHz, respectively.

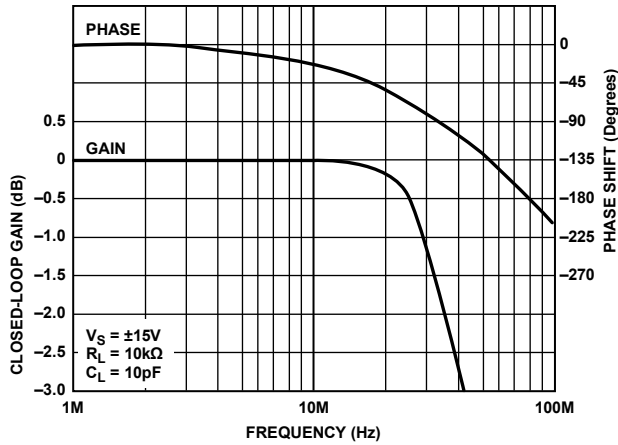


Figure 61. Closed-Loop Gain and Phase Shift vs. Frequency for 4:1 Mux, On Channel

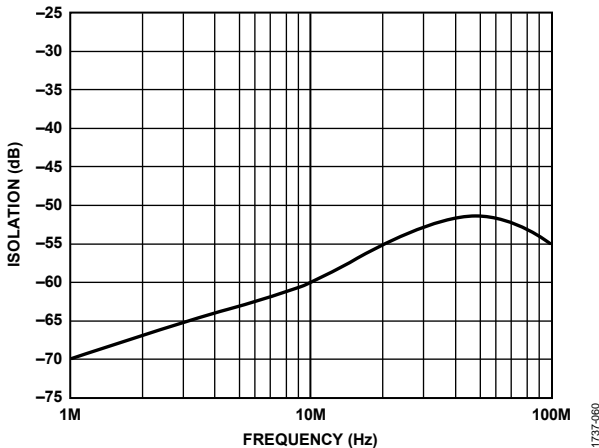


Figure 62. Isolation vs. Frequency for 4:1 Mux, Off Channel

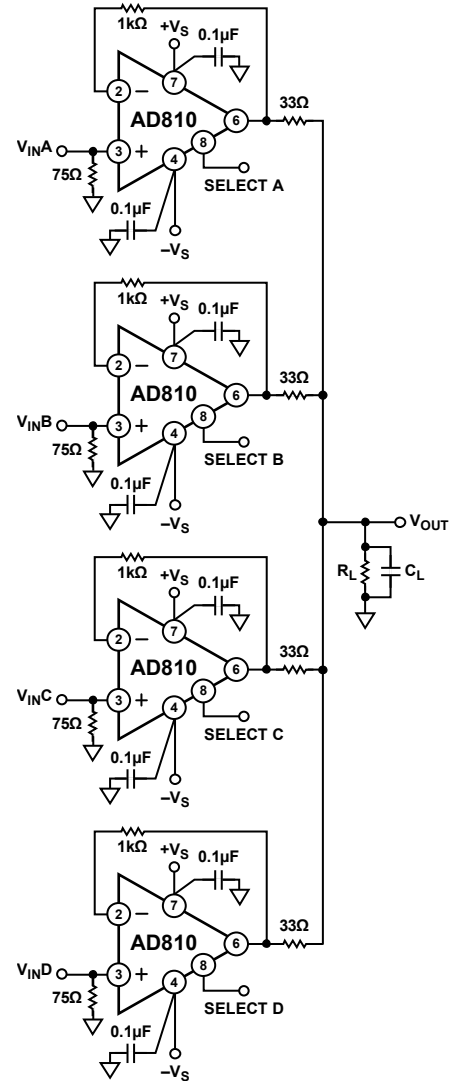
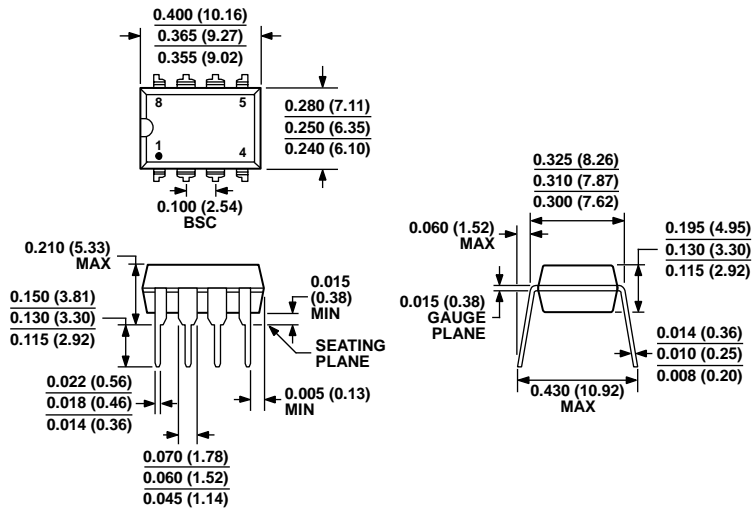


Figure 63. 4:1 Multiplexer Driving a High Impedance

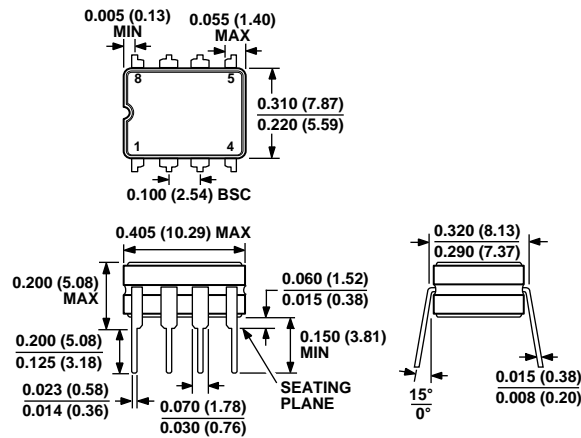
OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-001  
 CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN. CORNER LEADS MAY BE CONFIGURED AS WHOLE OR HALF LEADS.

Figure 64. 8-Lead Plastic Dual In-Line Package [PDIP]  
 Narrow Body  
 (N-8)

Dimensions shown in inches and (millimeters)

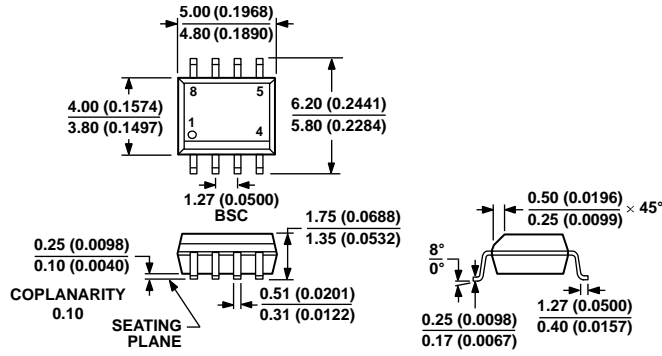


CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 65. 8-Lead Ceramic Dual In-Line Package [CERDIP]  
 (Q-8)

Dimensions shown in inches and (millimeters)

070606-A



COMPLIANT TO JEDEC STANDARDS MS-012-AA  
 CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS  
 (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR  
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

012407-A

Figure 66. 8-Lead Standard Small Outline Package [SOIC\_N]  
 Narrow Body  
 (R-8)  
 Dimensions shown in millimeters and (inches)

**ORDERING GUIDE**

Model <sup>1</sup>	Temperature Range	Package Description	Package Option
AD810ANZ	-40°C to +85°C	8-Lead Plastic Dual In-Line Package [PDIP]	N-8
AD810ARZ	-40°C to +85°C	8-Lead Plastic Standard Small Outline Package [SOIC_N]	R-8
AD810ARZ-REEL	-40°C to +85°C	8-Lead Plastic Standard Small Outline Package [SOIC_N]	R-8
AD810ARZ-REEL7	-40°C to +85°C	8-Lead Plastic Standard Small Outline Package [SOIC_N]	R-8
5962-9313201MPA	-55°C to +125°C	8-Lead Ceramic Dual In-Line Package [CERDIP]	Q-8

<sup>1</sup> Z = RoHS Compliant Part.

Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;
- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



## JONHON

«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



Телефон: 8 (812) 309-75-97 (многоканальный)

Факс: 8 (812) 320-03-32

Электронная почта: [ocean@oceanchips.ru](mailto:ocean@oceanchips.ru)

Web: <http://oceanchips.ru/>

Адрес: 198099, г. Санкт-Петербург, ул. Калинина, д. 2, корп. 4, лит. А