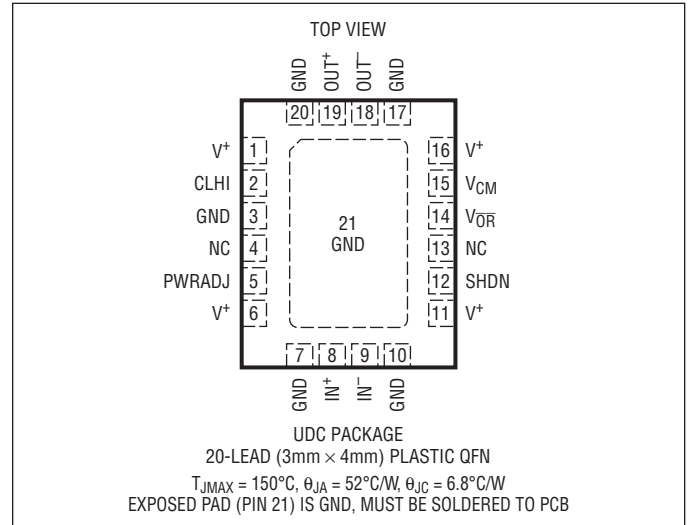


ABSOLUTE MAXIMUM RATINGS

(Note 1)

| | |
|--------------------------------------|--|
| Total Supply Voltage (V^+ to GND) | 5.5V |
| Input Current (CLHI, V_{CM}) | $\pm 10\text{mA}$ |
| Input Current (IN^+ , IN^-) | $\pm 30\text{mA}$ |
| Output Current (OUT^+ , OUT^-) | $\pm 100\text{mA}$ |
| Output Current (V_{OR}) | $\pm 10\text{mA}$ |
| Operating Temperature Range | |
| (T_C) (Note 2) | -40°C to 105°C |
| Specified Temperature Range | |
| (T_C) (Note 3) | -40°C to 105°C |
| Storage Temperature Range | -65°C to 150°C |
| Junction Temperature (T_{JMAX}) | 150°C |

PIN CONFIGURATION



ORDER INFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING* | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
|------------------|-------------------|---------------|---------------------------------|--|
| LTC6417CUDC#PBF | LTC6417CUDC#TRPBF | LFVN | 20-Lead (3mm × 4mm) Plastic QFN | 0°C to 70°C |
| LTC6417IUDC#PBF | LTC6417IUDC#TRPBF | LFVN | 20-Lead (3mm × 4mm) Plastic QFN | -40°C to 105°C (T_C) |

*Temperature grades are identified by a label on the shipping container.

Consult LTC Marketing for parts specified with wider operating temperature ranges.

Consult LTC Marketing for information on lead based finish parts.

For more information on lead free part marking, go to: <http://www.linear.com/leadfree/>

For more information on tape and reel specifications, go to: <http://www.linear.com/tapeandree/>

DC ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$, $GND = 0\text{V}$, No R_{LOAD} , $C_{LOAD} = 6\text{pF}$. $V_{CM} = 1.25\text{V}$, $CLHI = V^+$, $PWRADJ = V^+$, $SHDN = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(IN^+ + IN^-)/2$. V_{OUTCM} is defined as $(OUT^+ + OUT^-)/2$. V_{INDIFF} is defined as $(IN^+ - IN^-)$. $V_{OUTDIFF}$ is defined as $(OUT^+ - OUT^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|-------------------------------------|---|---|--------------------|--------|-------------|------------------------|
| Input/Output Characteristics | | | | | | |
| G_{DIFF} | Differential Gain | $V_{INDIFF} = \pm 1.2\text{V}$ Differential | ● -0.15 -0.2 | -0.1 | 0 0 | dB dB |
| TCG_{DIFF} | Differential Gain Temperature Coefficient | | ● | 0.0002 | | dB/ $^\circ\text{C}$ |
| $V_{SWINGDIFF}$ | Differential Output Voltage Swing | $V_{OUTDIFF}$, $V_{INDIFF} = \pm 2.3\text{V}$ | ● 4 3.3 | 4.28 | | V_{P-P} V_{P-P} |
| $V_{SWINGMIN}$ | Output Voltage Swing Low | Single-Ended Measurement of OUT^+ , OUT^- $V_{INDIFF} = \pm 2.3\text{V}$ | ● | 0.19 | 0.28 0.4 | V V |
| $V_{SWINGMAX}$ | Output Voltage Swing High | Single-Ended Measurement of OUT^+ , OUT^- $V_{INDIFF} = \pm 2.3\text{V}$ | ● 2.25 2.05 | 2.33 | | V V |

DC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$, $\text{GND} = 0\text{V}$, No R_{LOAD} , $C_{\text{LOAD}} = 6\text{pF}$. $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWADJ} = V^+$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | | MIN | TYP | MAX | UNITS |
|--|---|--|---|--------------|------|--------------|--------------------------------------|
| I_{OUT} | Output Current Drive (Notes 1, 4) | Single-Ended Measurement of OUT^+ , OUT^- | ● | ± 100 | | | mA |
| V_{OS} | Differential Input Offset Voltage | $\text{IN}^+ = \text{IN}^- = 1.25\text{V}$, $V_{\text{OS}} = V_{\text{OUTDIFF}}/G_{\text{DIFF}}$ | ● | -3.2 -4 | -0.1 | 3.2 4 | mV mV |
| TCV_{OS} | Differential Input Offset Voltage Drift | | ● | | 1 | | $\mu\text{V}/^\circ\text{C}$ |
| V_{IOCM} | Common Mode Offset Voltage, Input to Output | $V_{\text{OUTCM}} - V_{\text{INCM}}$ | ● | -120 -140 | -60 | -10 0 | mV mV |
| IVR_{MIN} | Input Voltage Range, IN^+ , IN^- (Minimum) (Single-Ended) | Defined by Output Voltage Swing Test | ● | | | 0.1 | V |
| IVR_{MAX} | Input Voltage Range IN^+ , IN^- (Maximum) (Single-Ended) | Defined by Output Voltage Swing Test | ● | 2.4 | | | V |
| I_{B} | Input Bias Current, IN^+ , IN^- | $\text{IN}^+ = \text{IN}^- = 1.25\text{V}$ | ● | -13 -18 | 2 | 13 18 | μA μA |
| R_{INDIFF} | Differential Input Resistance | $V_{\text{INDIFF}} = \pm 1.2\text{V}$ | ● | 12 11 | 18.5 | 25 27.5 | $\text{k}\Omega$ $\text{k}\Omega$ |
| C_{INDIFF} | Differential Input Capacitance | | | | 1 | | pF |
| R_{INCM} | Input Common Mode Resistance | $\text{IN}^+ = \text{IN}^- = 0.65\text{V}$ to 1.85V | ● | 5.8 5 | 9.25 | 13 15 | $\text{k}\Omega$ $\text{k}\Omega$ |
| CMRR | Common Mode Rejection Ratio | $\text{IN}^+ = \text{IN}^- = 0.65\text{V}$ to 1.85V , $\text{CMRR} = (V_{\text{OUTDIFF}}/G_{\text{DIFF}}/1.2\text{V})$ | ● | 63 60 | 91 | | dB dB |
| R_{OUTDIFF} | Differential Output Resistance | | | | 3 | | Ω |
| e_{N} | Input Noise Voltage Density | $f = 100\text{kHz}$ | | | 1.5 | | $\text{nV}/\sqrt{\text{Hz}}$ |
| i_{N} | Input Noise Current Density | $f = 100\text{kHz}$ | | | 4.3 | | $\text{pA}/\sqrt{\text{Hz}}$ |
| Output Common Mode Voltage Control | | | | | | | |
| G_{CM} | V_{CM} Pin Common Mode Gain | $V_{\text{CM}} = 0.65\text{V}$ to 1.85V | ● | 0.82 0.8 | 0.92 | | V/V V/V |
| $V_{\text{INCMDEFAULT}}$ | Default Input Common Mode Voltage | V_{INCM} . IN^+ , IN^- , V_{CM} Pin Floating | ● | 1.15 1.1 | 1.25 | 1.35 1.4 | V V |
| $V_{\text{OS}} (V_{\text{CM}} - V_{\text{INCM}})$ | Offset Voltage, V_{CM} to V_{INCM} | $V_{\text{CM}} - V_{\text{INCM}}$, $V_{\text{CM}} = 1.25\text{V}$ | ● | -85 -90 | 15 | 115 135 | mV mV |
| $V_{\text{OUTCMDEFAULT}}$ | Default Output Common Mode Voltage | Inputs Floating, V_{CM} Pin Floating | ● | 1.1 1 | 1.2 | 1.3 1.35 | V V |
| $V_{\text{OS}} (V_{\text{CM}} - V_{\text{OUTCM}})$ | Offset Voltage, V_{CM} to V_{OUTCM} | $V_{\text{CM}} - V_{\text{OUTCM}}$, $V_{\text{CM}} = 1.25\text{V}$ | ● | -50 -45 | 75 | 200 230 | mV mV |
| V_{OUTCMMIN} | Output Common Mode Voltage Range (Minimum) | $V_{\text{CM}} = 0.1\text{V}$ | ● | | 0.29 | 0.63 0.65 | V V |
| V_{OUTCMMAX} | Output Common Mode Voltage Range (Maximum) | $V_{\text{CM}} = 2.4\text{V}$ | ● | 2 1.85 | 2.25 | | V V |
| $V_{\text{CMDEFAULT}}$ | V_{CM} Pin Default Voltage | | ● | 1.15 1.1 | 1.25 | 1.35 1.4 | V V |
| R_{VCM} | V_{CM} Pin Input Resistance | $V_{\text{CM}} = 0.65\text{V}$ to 1.85V | ● | 2 1.9 | 2.7 | 3.4 3.7 | $\text{k}\Omega$ $\text{k}\Omega$ |
| C_{VCM} | V_{CM} Pin Input Capacitance | | | | 1 | | pF |
| I_{BVCM} | V_{CM} Pin Bias Current | $V_{\text{CM}} = 1.25\text{V}$ | ● | -15 -27.5 | 1 | 15 27.5 | μA μA |

DC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$, $\text{GND} = 0\text{V}$, No R_{LOAD} , $C_{\text{LOAD}} = 6\text{pF}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWRADJ} = V^+$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | | MIN | TYP | MAX | UNITS |
|---|--|--|---|---------------|------|---------------|--------------------------------|
| DC Clamping Characteristics | | | | | | | |
| $V_{\text{CLHI}}^{\text{DEFAULT}}$ | Default Output Clamp Voltage, High | | ● | 2.4 2.35 | 2.48 | 2.55 2.6 | V V |
| $V_{\text{OS}}(\text{CLHI} - V_{\text{OUTCM}})$ | Offset Voltage, CLHI to V_{OUTCM} | | ● | -60 -85 | 20 | 80 85 | mV mV |
| $V_{\text{OS}}(\text{CLLO} - V_{\text{OUT}})$ | Offset Voltage, CLLO to V_{OUT} | $V_{\text{CLHI}} = 2.0\text{V}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 2.4\text{V}$, $\text{IN}^- = 0.1\text{V}$ | ● | -100 -110 | 10 | 100 110 | mV mV |
| G_{LOHI} | Low Side Clamp Gain with Respect to CLHI Pin | $V_{\text{CLHI}} = 2.0\text{V}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 2.4\text{V}$, $\text{IN}^- = 0.1\text{V}$ | ● | -1.2 -1.25 | -1 | -0.8 -0.75 | V/V V/V |
| G_{LOCM} | Low Side Clamp Gain with Respect to CM Pin | $V_{\text{CLHI}} = 2.0\text{V}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 2.4\text{V}$, $\text{IN}^- = 0.1\text{V}$ | ● | 1.65 1.5 | 1.9 | 2.2 2.25 | V/V V/V |
| R_{CLHI} | CLHI Pin Input Resistance | $V_{\text{CLHI}} = 1.5\text{V}$ to 2.5V | ● | 3.4 3.1 | 4.8 | 5.7 6 | k Ω k Ω |
| I_{BCLHI} | CLHI Pin Bias Current | $V_{\text{CLHI}} = 2.5\text{V}$ | ● | -12 -12.5 | 3 | 18 18.5 | μA μA |
| Power Supply | | | | | | | |
| V_{S} | Supply Voltage Range | | ● | 4.75 | | 5.25 | V |
| I_{S} | Supply Current | | ● | 100 95 | 123 | 140 145 | mA mA |
| PSRR | Power Supply Rejection Ratio | $V_{\text{S}} = 4.75\text{V}$ to 5.25V | ● | 65 63 | 72 | | dB dB |
| SHDN Pin | | | | | | | |
| I_{SHDN} | Shutdown Current | $V_{\text{SHDN}} = 5\text{V}$ | ● | 17 15 | 24 | 29 35 | mA mA |
| $V_{\text{SHDN}}^{\text{DEFAULT}}$ | Default Shutdown Voltage | | ● | | | 0.1 | V |
| $V_{\text{IL,SHDN}}$ | SHDN Input Low Voltage | | ● | | | 2 | V |
| $V_{\text{IH,SHDN}}$ | SHDN Input High Voltage | | ● | 3.5 | | | V |
| $I_{\text{IL,SHDN}}$ | SHDN Input Low Current | $\text{SHDN} = 0\text{V}$ | ● | -1.6 -2 | 0 | 1.6 2 | μA μA |
| $I_{\text{IH,SHDN}}$ | SHDN Input High Current | $\text{SHDN} = 5\text{V}$ | ● | 275 250 | 380 | 450 475 | μA μA |
| C_{SHDN} | SHDN Pin Input Capacitance | | | | 1 | | pF |
| R_{SHDN} | SHDN Pin Input Resistance | $\text{SHDN} = 2.5\text{V}$ to 5V | ● | 6 5 | 10.5 | 14 15 | k Ω k Ω |
| PWRADJ Pin | | | | | | | |
| $V_{\text{PWRADJ}}^{\text{DEFAULT}}$ | Default PWRADJ Voltage | PWRADJ Floating | | 1.5 1.45 | 1.65 | 1.8 1.85 | V V |
| $I_{\text{S,L}}$ | Supply Low Current | PWRADJ = 0V | ● | 45 40 | 74 | 105 110 | mA mA |
| $I_{\text{IL,PWRADJ}}$ | PWRADJ Input Low Current | PWRADJ = 0V | ● | -145 -165 | -120 | -80 -75 | μA μA |
| $I_{\text{IH,PWRADJ}}$ | PWRADJ Input High Current | PWRADJ = 5V | ● | 210 200 | 240 | 290 300 | μA μA |
| C_{PWRADJ} | PWRADJ Pin Input Capacitance | | | | 1 | | pF |

DC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$, $\text{GND} = 0\text{V}$, No R_{LOAD} , $C_{\text{LOAD}} = 6\text{pF}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWRADJ} = V^+$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|---------------------------------------|--|--|---------------|------|--------------|--------------------------------|
| R_{PWRADJ} | PWRADJ Pin Input Resistance | PWRADJ = 2.5V to 5.0V | 10.5 10 | 14.5 | 19 20 | $k\Omega$ $k\Omega$ |
| V_{OR} Pin | | | | | | |
| $V_{\text{OR(HI)}}$ | Maximum Voltage on V_{OR} Pin | $V_{\text{CL}} = 5.0\text{V}$, $V_{\text{CM}} = 1.25\text{V}$ | 3.25 3.2 | 3.35 | 3.55 3.6 | V V |
| $I_{\text{OR(DEFAULT)}}$ | Default Pull-Down Current on V_{OR} Pin | $V_{\text{CL}} = 50\text{V}$, $V_{\text{CM}} = 1.25\text{V}$ | -900 -1150 | -770 | -650 -500 | μA μA |
| $I_{\text{OR(MAX)}}$ | Maximum Pull-Down Current Both Clamps are Active | $V_{\text{CL}} = 2.0\text{V}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 2.4\text{V}$, $\text{IN}^- = 0.1\text{V}$ | | 1 | 1.5 2 | μA μA |

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$ unless otherwise noted, $\text{GND} = 0\text{V}$, $R_{\text{LOAD}} = 500\Omega$, $C_{\text{LOAD}} = 6\text{pF}$, $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWRADJ} = V_{\text{CC}}$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|--|--|--|-----|------|-----|------------------|
| Differential AC Characteristics | | | | | | |
| -3dBBW | -3dB Bandwidth | 200mV _{P-P,OUT} Differential | | 1.6 | | GHz |
| 0.1dBBW | $\pm 0.1\text{dB}$ Bandwidth | 200mV _{P-P,OUT} Differential | | 0.18 | | GHz |
| 0.5dBBW | $\pm 0.5\text{dB}$ Bandwidth | 200mV _{P-P,OUT} Differential | | 0.45 | | GHz |
| 1/f | 1/f Noise Corner | | | 25 | | kHz |
| SR | Slew Rate | Differential | | 10 | | V/ns |
| $t_{\text{S1\%}}$ | 1% Settling Time | 2V _{P-P,OUT} | | 0.8 | | ns |
| t_{OFF} | Shutdown Time | SHDN = 0V to 5V | | 40 | | ns |
| t_{ON} | Enable Time | SHDN = 5V to 0V | | 15 | | ns |
| $t_{\text{PWRADJ,OFF}}$ | PWRADJ Off Time | PWRADJ = 5V to 0V | | 10 | | ns |
| $t_{\text{PWRADJ,ON}}$ | PWRADJ On Time | PWRADJ = 0V to 5V | | 5 | | ns |
| $t_{\text{CL,OFF 10\%}}$ | Clamp Release Time | CLHI = 1.5V, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 1.625\text{V}$ to 1.25V, $\text{IN}^- = 1.25\text{V}$ to 0.875V | | 1 | | ns |
| $t_{\text{CL,ON 10\%}}$ | Clamp Engage Time | CLHI = 1.5V, $V_{\text{CM}} = 1.25\text{V}$, $\text{IN}^+ = 1.25\text{V}$ to 1.625V, $\text{IN}^- = 1.25\text{V}$ to 0.875V | | 5 | | ns |
| Common Mode AC Characteristics (V_{CM} Pin) | | | | | | |
| -3dBBW | V_{CM} Pin Small Signal -3dB BW | $V_{\text{CM}} = 0.1\text{V}_{\text{P-P}}$, Measured Single-Ended at Output | | 10 | | MHz |
| SR_{CM} | Common Mode Slew Rate | Measured Single-Ended at Output | | 2 | | V/ μs |
| Overshoot AC Characteristics (V_{OR} Pin) | | | | | | |
| -3dBBW | V_{OR} Pin Small Signal -3dB BW | $V_{\text{OR}} = 0.1\text{V}_{\text{P-P}}$, CLHI = 2V, $\text{IN}^+ = 2.4\text{V}$, $\text{IN}^- = 0.1\text{V}$, $R_{\text{VOR}} = 1\text{k}$, Measured Single-Ended at Output | | 200 | | MHz |
| SR_{VOR} | Overshoot Slew Rate | Measured Single-Ended at Output | | 40 | | V/ μs |
| AC Clamping Characteristics | | | | | | |
| t_{OVR} | Overdrive Recovery Time | 1.9V _{P-P,OUT} | | 2 | | ns |

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$ unless otherwise noted, $\text{GND} = 0\text{V}$, $R_{\text{LOAD}} = 500\Omega$, $C_{\text{LOAD}} = 6\text{pF}$. $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWRADJ} = V_{\text{CC}}$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|----------------------|--|---|-----|--------------|-----|------------|
| AC Linearity | | | | | | |
| 10MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -89 -93 | | dBc dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -100 -110 | | dBc dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 56 | | dBm |
| P1dB | Output 1dB Compression Point | | | 16.1 | | dBm |
| 70MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -74 -77 | | dBc dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -86 -96 | | dBc dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 48 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.8 | | dBm |
| 140MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -69 -73 | | dBc dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -80 -91 | | dBc dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 46 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.8 | | dBm |
| 200MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -68 -71 | | dBc dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -78 -87 | | dBc dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 44 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.8 | | dBm |
| 240MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -67 -70 | | dBc dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -76 -85 | | dBc dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 43 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.7 | | dBm |
| 300MHz Signal | | | | | | |
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -66 -69 | | dBc dBc |

AC ELECTRICAL CHARACTERISTICS The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V^+ = 5\text{V}$ unless otherwise noted, $\text{GND} = 0\text{V}$, $R_{\text{LOAD}} = 500\Omega$, $C_{\text{LOAD}} = 6\text{pF}$. $V_{\text{CM}} = 1.25\text{V}$, $\text{CLHI} = V^+$, $\text{PWRADJ} = V_{\text{CC}}$, $\text{SHDN} = 0\text{V}$ unless otherwise noted. V_{INCM} is defined as $(\text{IN}^+ + \text{IN}^-)/2$. V_{OUTCM} is defined as $(\text{OUT}^+ + \text{OUT}^-)/2$. V_{INDIFF} is defined as $(\text{IN}^+ - \text{IN}^-)$. V_{OUTDIFF} is defined as $(\text{OUT}^+ - \text{OUT}^-)$. See DC test circuit schematic.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|--------|--|--|-----|------|-----|-------|
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -73 | | dBc |
| | | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -79 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 41 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.6 | | dBm |

380MHz Signal

| | | | | | | |
|------|--|--|----|------|--|-----|
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -66 | | dBc |
| | | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -68 | | dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -68 | | dBc |
| | | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -77 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | 36 | 39 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.3 | | dBm |

400MHz Signal

| | | | | | | |
|------|--|--|--|------|--|-----|
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -65 | | dBc |
| | | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -68 | | dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -68 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 39 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.3 | | dBm |

500MHz Signal

| | | | | | | |
|------|--|--|--|------|--|-----|
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -65 | | dBc |
| | | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$ | | -67 | | dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -64 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 37 | | dBm |
| P1dB | Output 1dB Compression Point | | | 15.0 | | dBm |

600MHz Signal

| | | | | | | |
|------|--|--|--|------|--|-----|
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -60 | | dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -58 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 34 | | dBm |
| P1dB | Output 1dB Compression Point | | | 14.7 | | dBm |

700MHz Signal

| | | | | | | |
|------|--|--|--|------|--|-----|
| HD3 | Third Harmonic Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -55 | | dBc |
| IM3 | Third Order Intermodulation Distortion | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | -52 | | dBc |
| OIP3 | Output Third Order Intercept | $V_{\text{OUTDIFF}} = 2.4\text{V}_{\text{P-P}}$, $R_L = 50\Omega$ | | 31 | | dBm |
| P1dB | Output 1dB Compression Point | | | 14.2 | | dBm |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

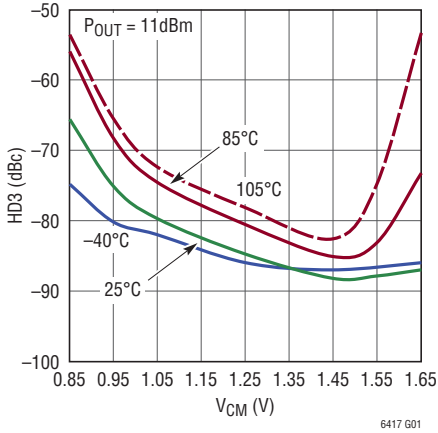
Note 2: The LTC6417C/LTC6417I is guaranteed functional over the case temperature operating range of -40°C to 105°C . $\theta_{\text{JC}} = 6.8^\circ\text{C/W}$.

Note 3: The LTC6417C is guaranteed to meet specified performance from 0°C to 70°C . It is designed, characterized and expected to meet specified performance from -40°C and 105°C case temperature range but is not tested or QA sampled at these temperatures. The LTC6417I is guaranteed to meet specified performance from -40°C to 105°C case temperature range.

Note 4: This parameter is pulse tested.

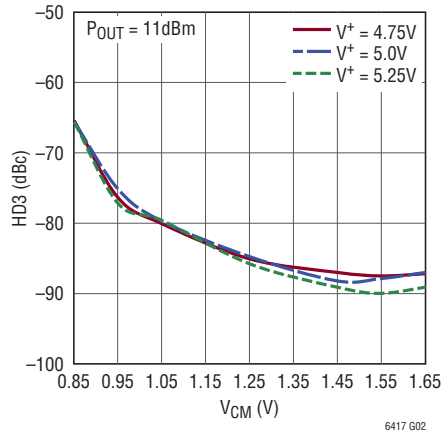
TYPICAL PERFORMANCE CHARACTERISTICS

HD3 at 30MHz vs V_{CM} Over Temperature



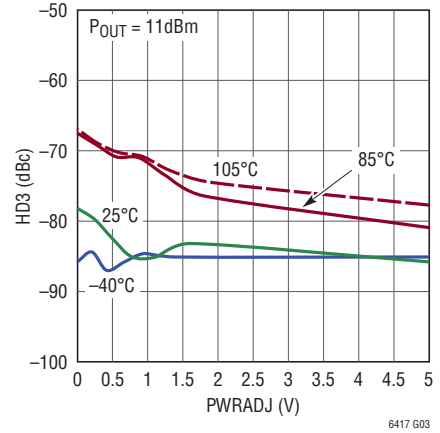
6417 G01

HD3 at 30MHz vs V_{CM} Over V^+



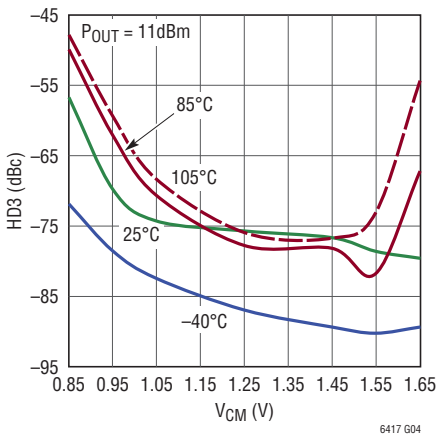
6417 G02

HD3 at 30MHz vs PWRADJ Over Temperature



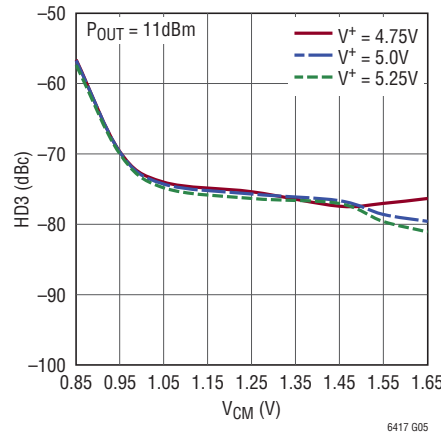
6417 G03

HD3 at 70MHz vs V_{CM} Over Temperature



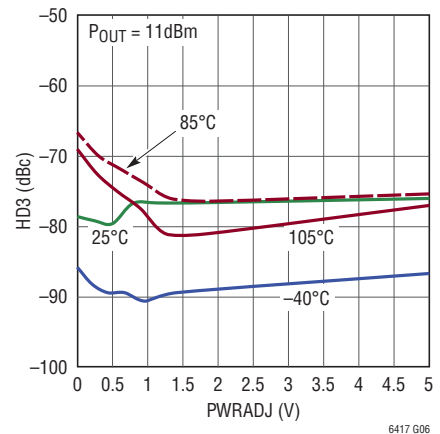
6417 G04

HD3 at 70MHz vs V_{CM} Over V^+



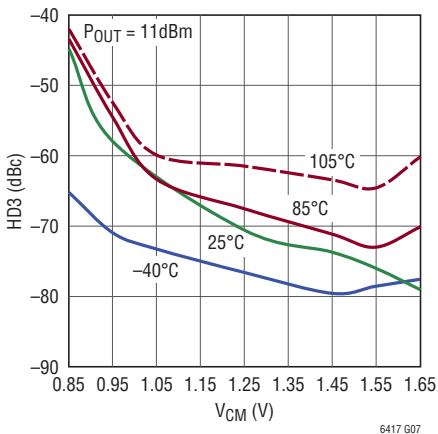
6417 G05

HD3 at 70MHz vs PWRADJ Over Temperature



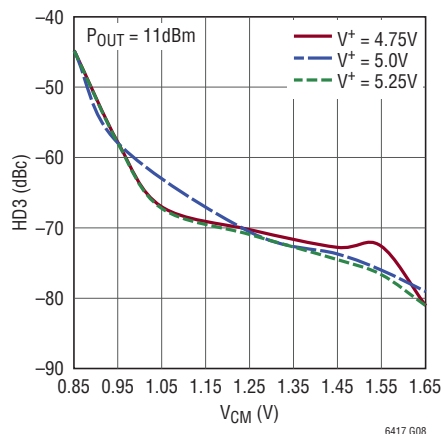
6417 G06

HD3 at 140MHz vs V_{CM} Over Temperature



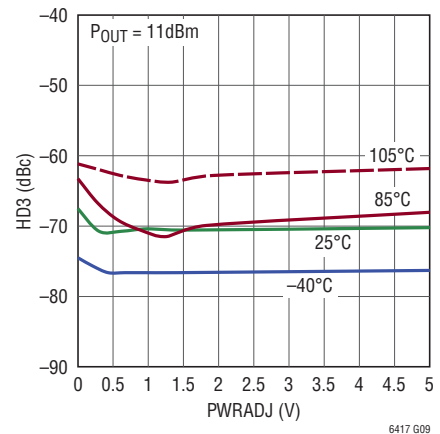
6417 G07

HD3 at 140MHz vs V_{CM} Over V^+



6417 G08

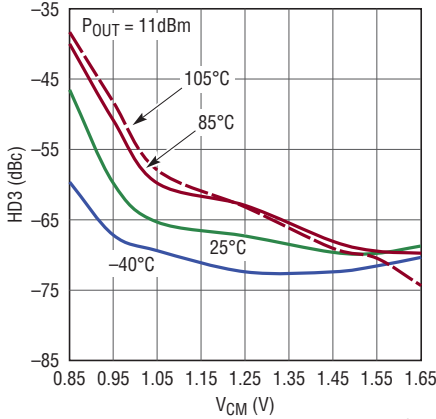
HD3 at 140MHz vs PWRADJ Over Temperature



6417 G09

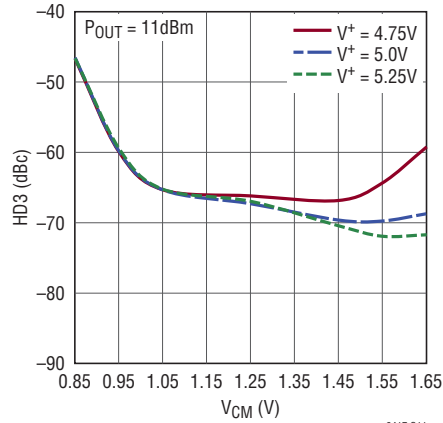
TYPICAL PERFORMANCE CHARACTERISTICS

HD3 at 240MHz vs V_{CM} Over Temperature



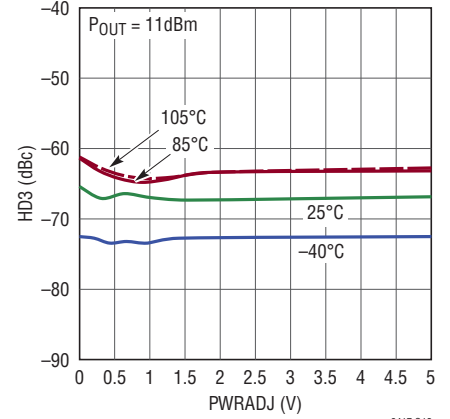
6417 G10

HD3 at 240MHz vs V_{CM} Over V^+



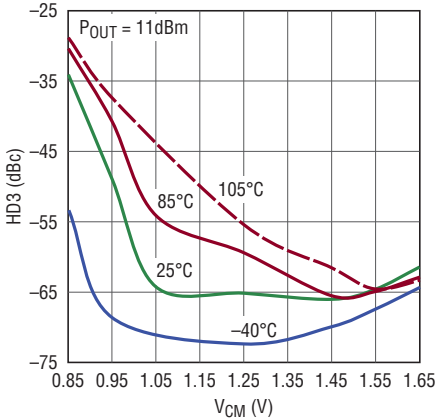
6417 G11

HD3 at 240MHz vs PWRADJ Over Temperature



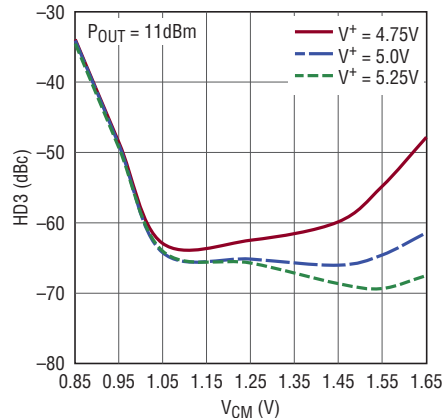
6417 G12

HD3 at 380MHz vs V_{CM} Over Temperature



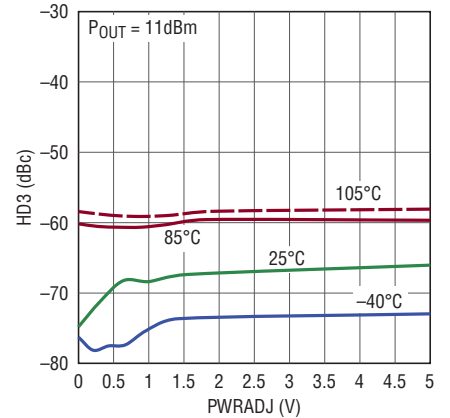
6417 G13

HD3 at 380MHz vs V_{CM} Over V^+



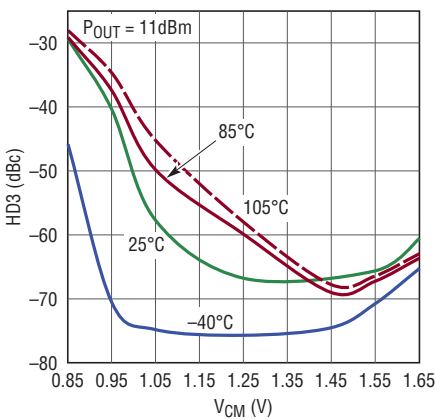
6417 G14

HD3 at 380MHz vs PWRADJ Over Temperature



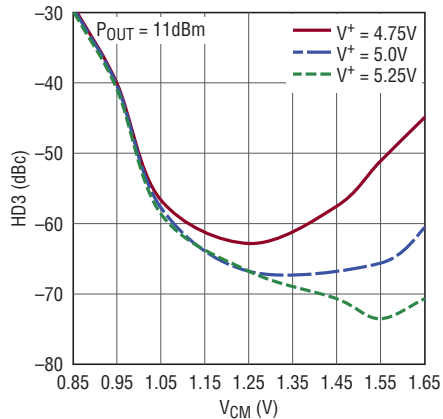
6417 G15

HD3 at 500MHz vs V_{CM} Over Temperature



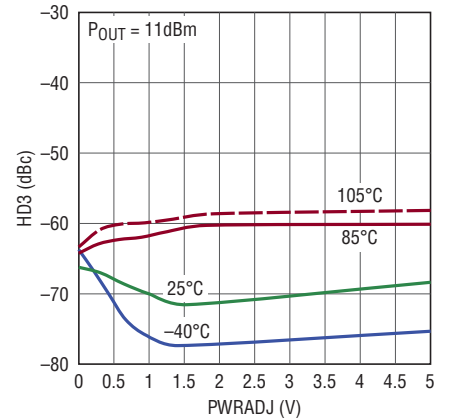
6417 G16

HD3 at 500MHz vs V_{CM} Over V^+



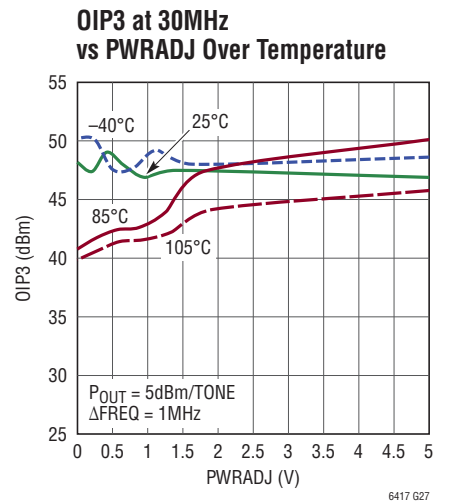
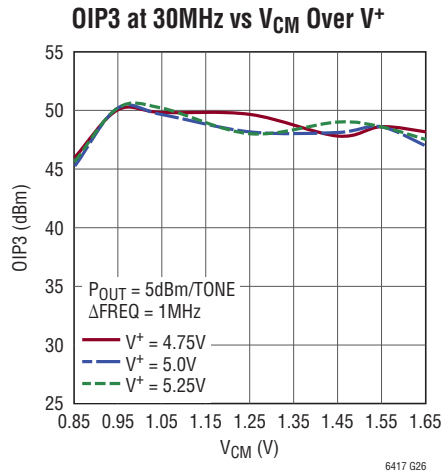
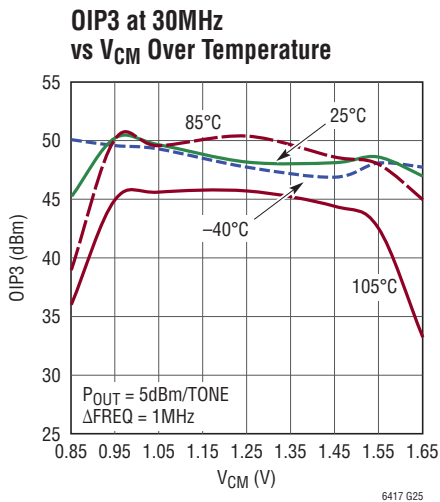
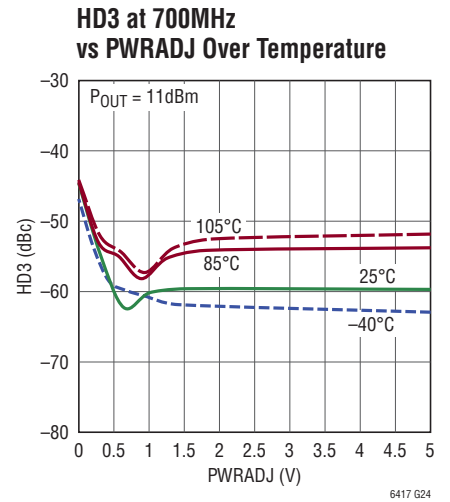
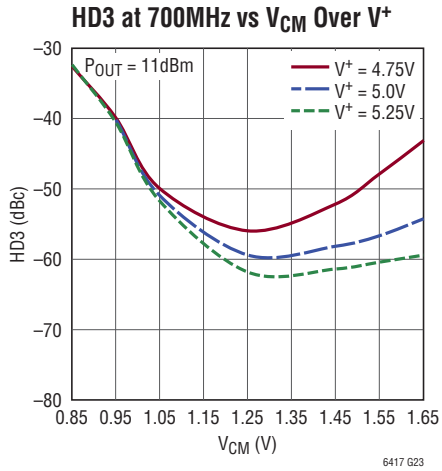
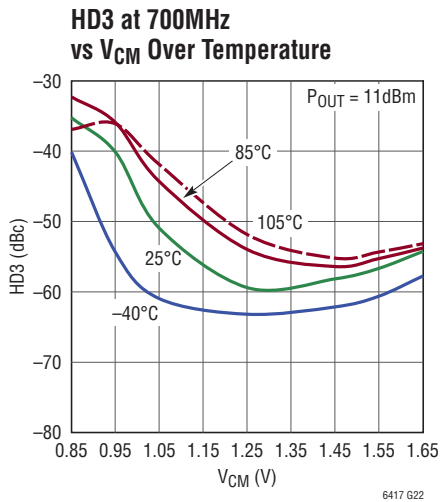
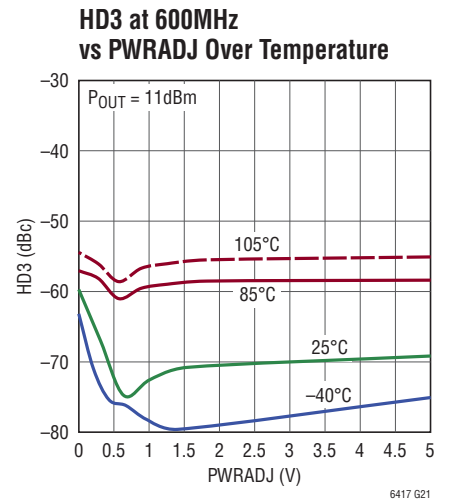
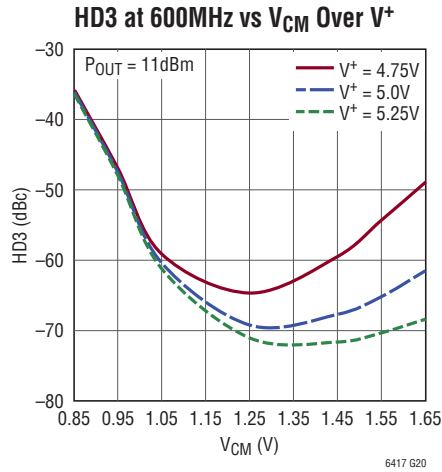
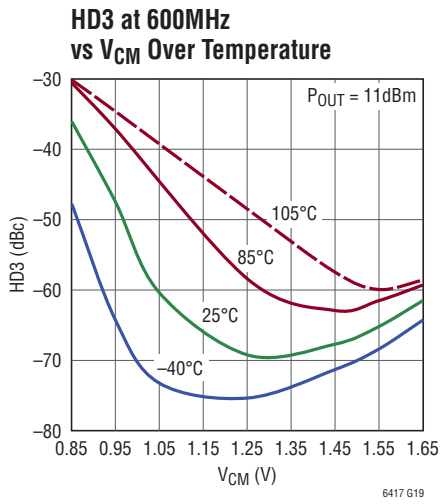
6417 G17

HD3 at 500MHz vs PWRADJ Over Temperature



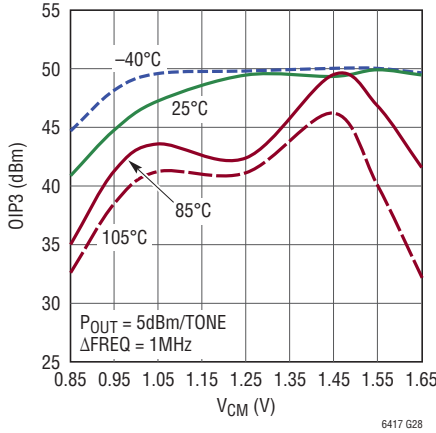
6417 G18

TYPICAL PERFORMANCE CHARACTERISTICS

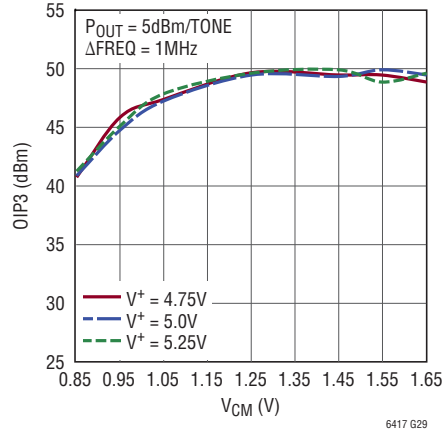


TYPICAL PERFORMANCE CHARACTERISTICS

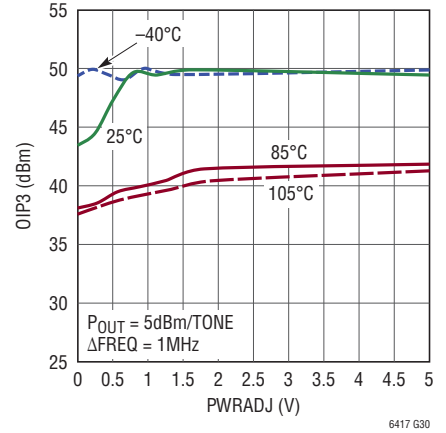
OIP3 at 70MHz vs V_{CM} Over Temperature



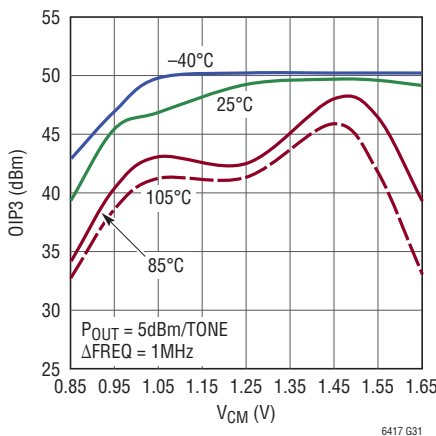
OIP3 at 70MHz vs V_{CM} Over V^+



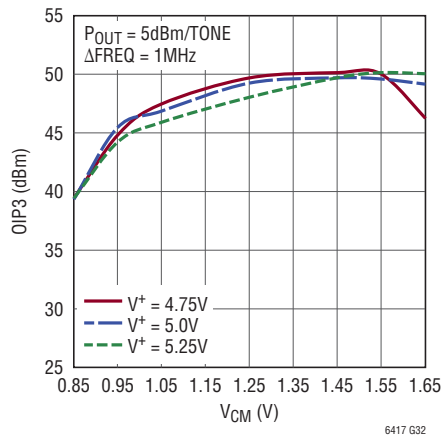
OIP3 at 70MHz vs PWRADJ Over Temperature



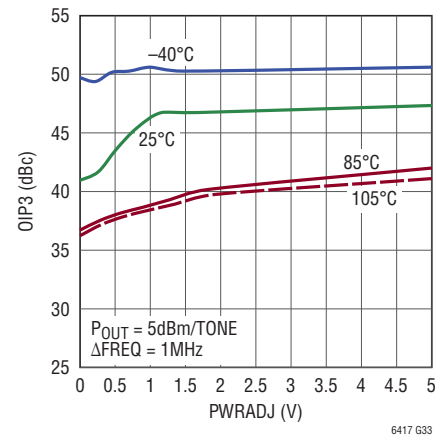
OIP3 at 100MHz vs V_{CM} Over Temperature



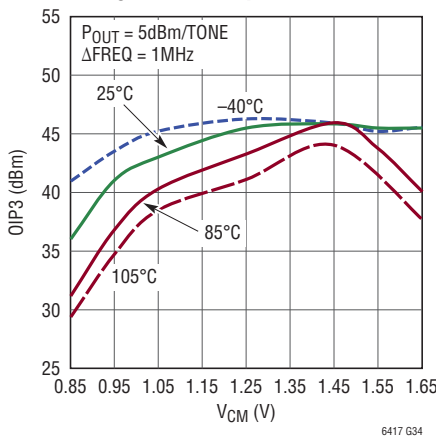
OIP3 at 100MHz vs V_{CM} Over V^+



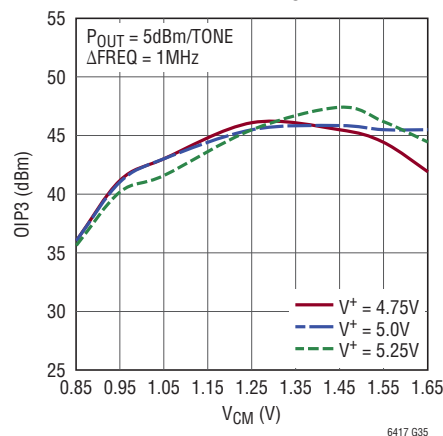
OIP3 at 100MHz vs PWRADJ Over Temperature



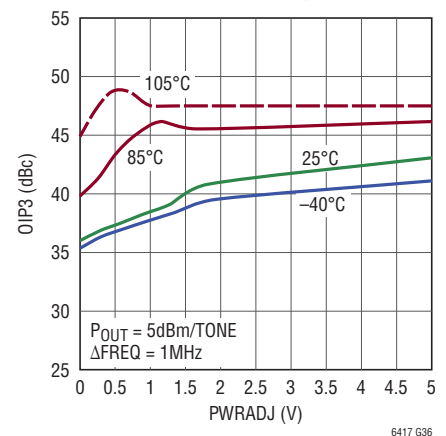
OIP3 at 140MHz vs V_{CM} Over Temperature



OIP3 at 140MHz vs V_{CM} Over V^+

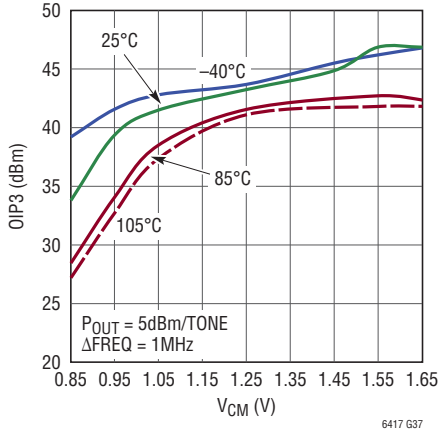


OIP3 at 140MHz vs PWRADJ Over Temperature

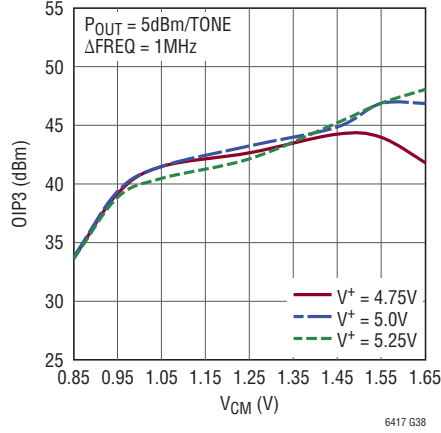


TYPICAL PERFORMANCE CHARACTERISTICS

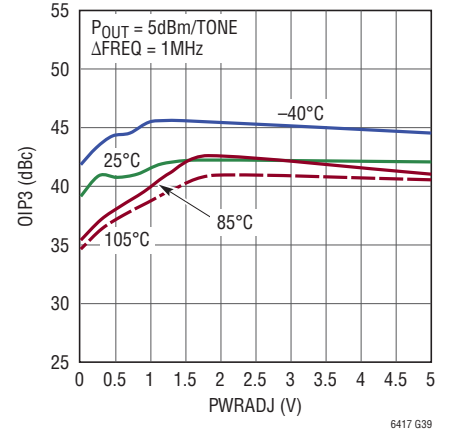
OIP3 at 240MHz vs V_{CM} Over Temperature



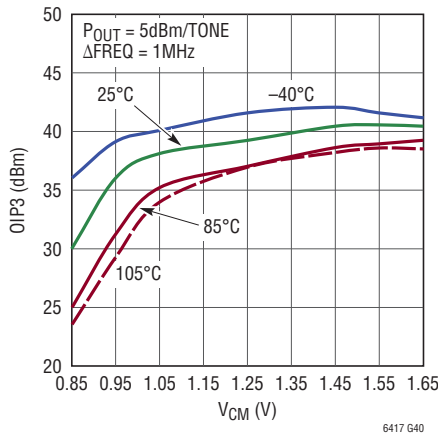
OIP3 at 240MHz vs V_{CM} Over V^+



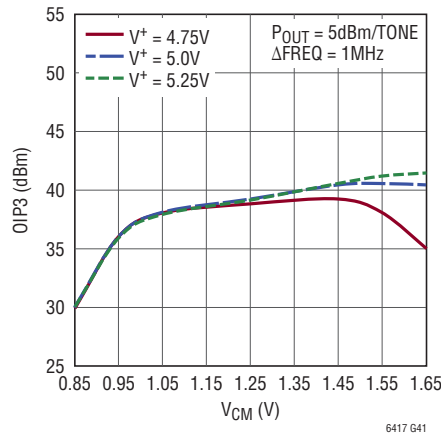
OIP3 at 240MHz vs PWRADJ Over Temperature



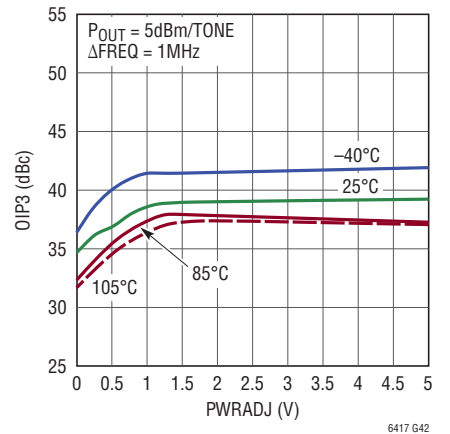
OIP3 at 380MHz vs V_{CM} Over Temperature



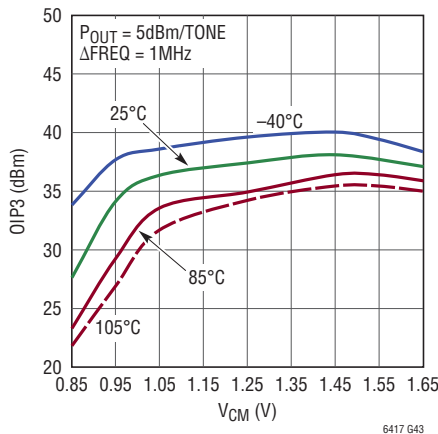
OIP3 at 380MHz vs V_{CM} Over V^+



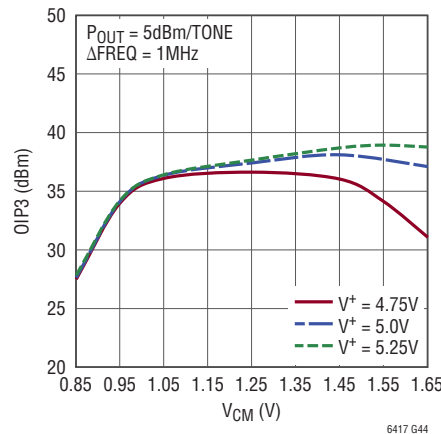
OIP3 at 380MHz vs PWRADJ Over Temperature



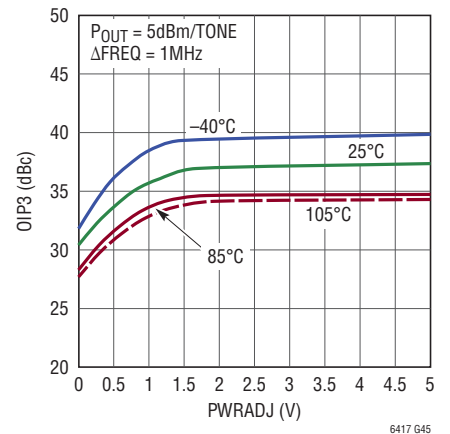
OIP3 at 500MHz vs V_{CM} Over Temperature



OIP3 at 500MHz vs V_{CM} Over V^+

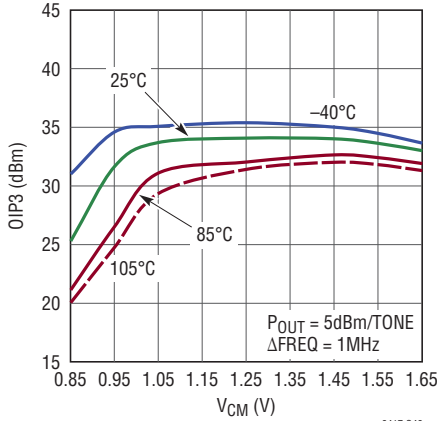


OIP3 at 500MHz vs PWRADJ Over Temperature

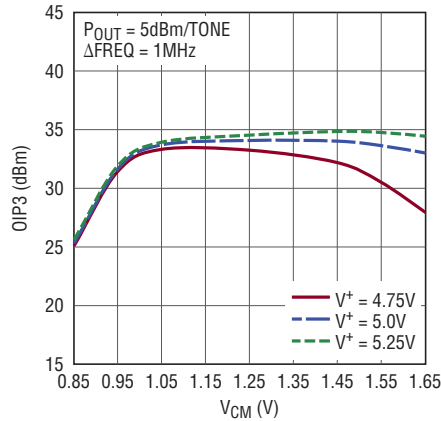


TYPICAL PERFORMANCE CHARACTERISTICS

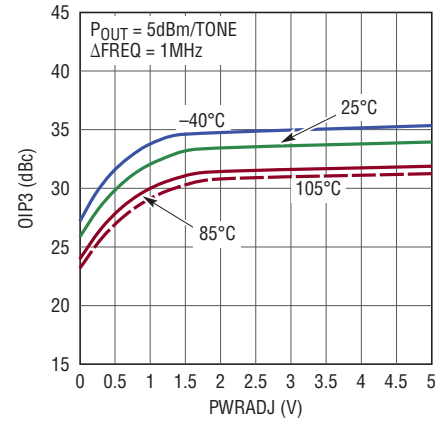
OIP3 at 600MHz vs V_{CM} Over Temperature



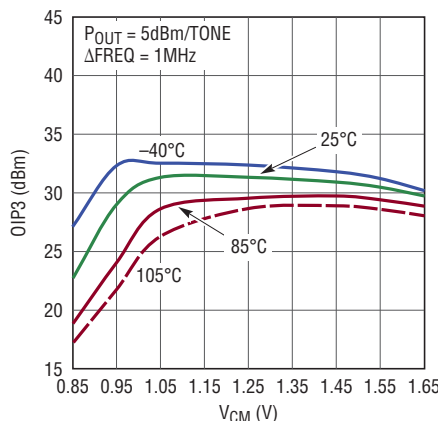
OIP3 at 600MHz vs V_{CM} Over V^+



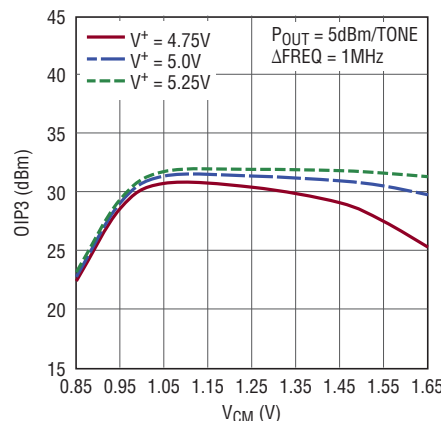
OIP3 at 600MHz vs PWRADJ Over Temperature



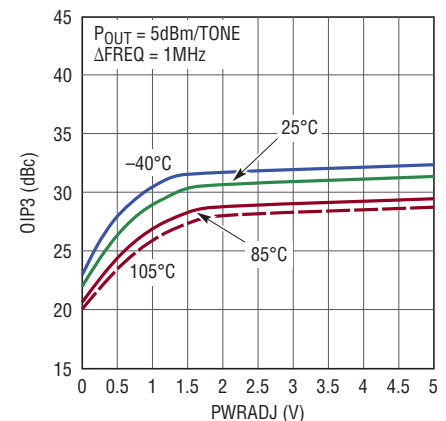
OIP3 at 700MHz vs V_{CM} Over Temperature



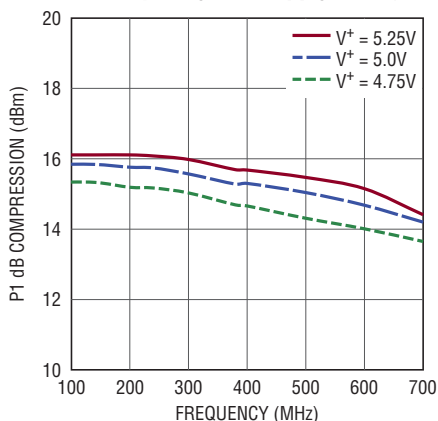
OIP3 at 700MHz vs V_{CM} Over V^+



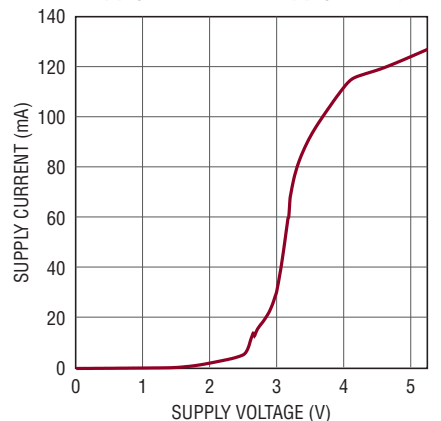
OIP3 at 700MHz vs PWRADJ Over Temperature



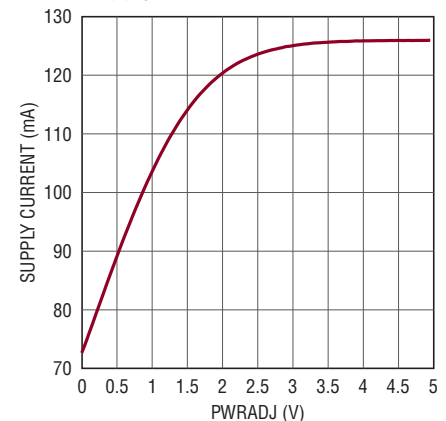
Output 1dB Compression vs Frequency and Supply Voltage



Supply Current vs Supply Voltage

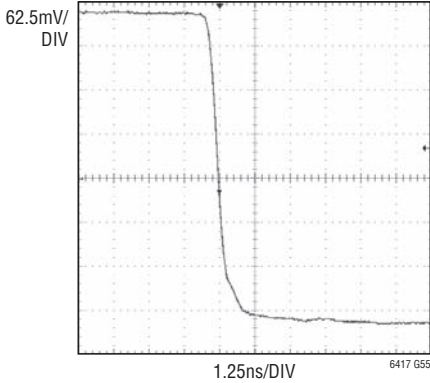


Supply Current vs PWRADJ

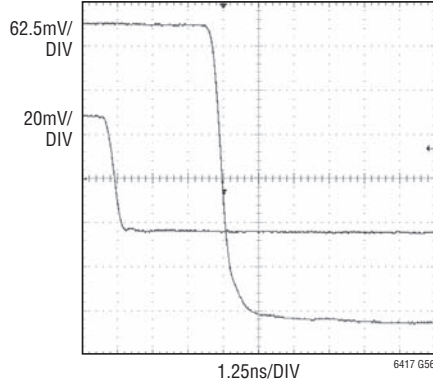


TYPICAL PERFORMANCE CHARACTERISTICS

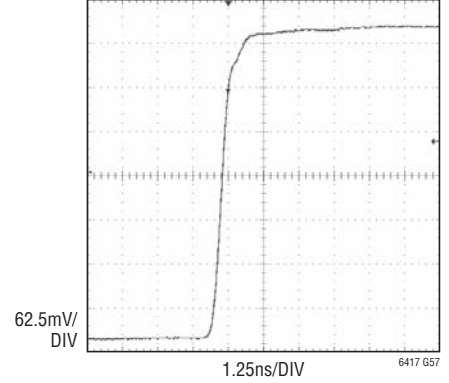
Small Signal Transient Response, Falling Edge



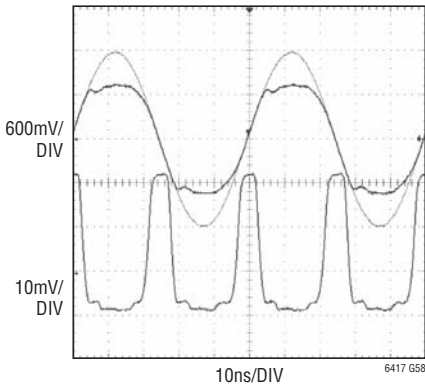
Small Signal Transient Response, Falling Edge with Input



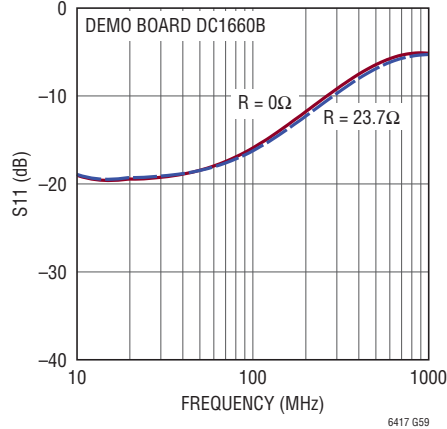
Small Signal Transient Response, Rising Edge



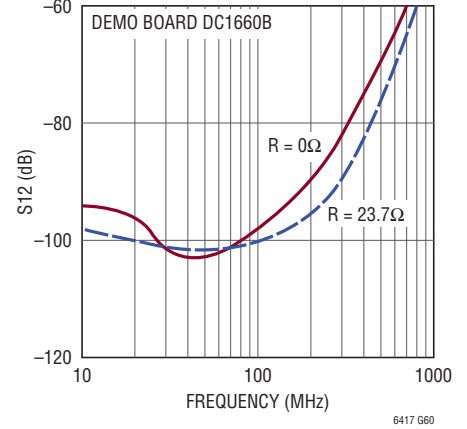
Overdrive Recovery and Overrange Response



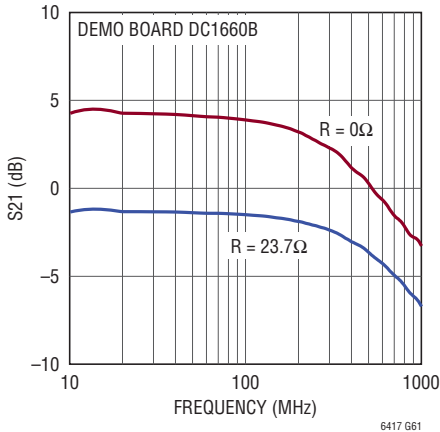
Differential Input Return Loss (S11) vs Frequency



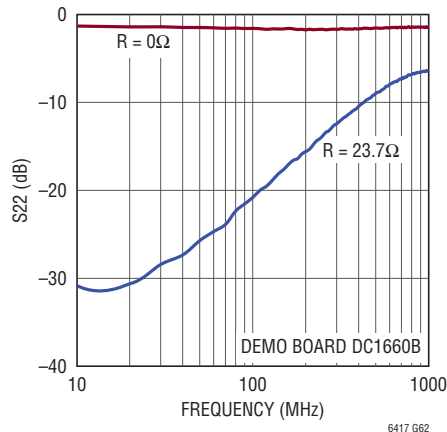
Differential Reverse Isolation (S12) vs Frequency



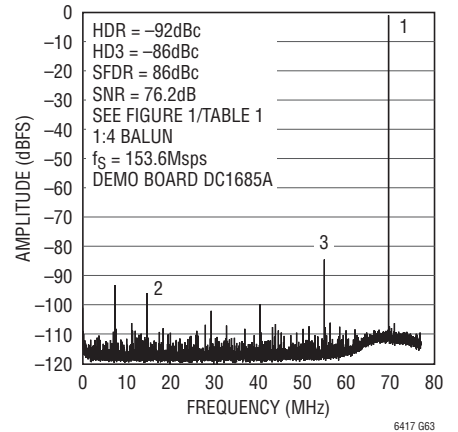
Differential Forward Gain (S21) vs Frequency



Differential Output Return Loss (S22) vs Frequency

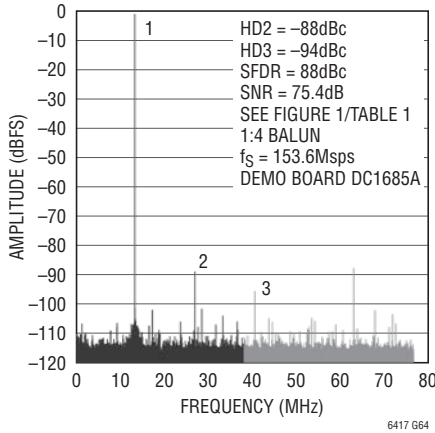


**LTC6417 Driving LTC2209
16-Bit ADC, 32K Point FFT,
f_{IN} = 69.5MHz, -1dBFS, PGA = 0**



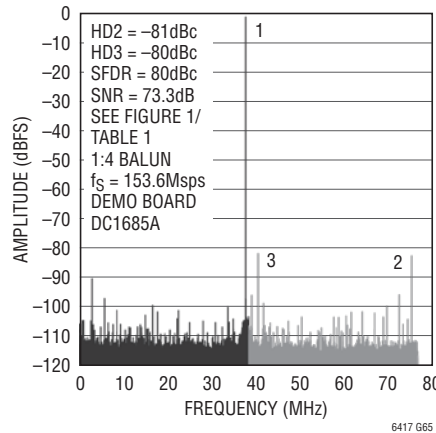
TYPICAL PERFORMANCE CHARACTERISTICS

**LTC6417 Driving LTC2209
16-Bit ADC, 64K Point FFT,
 $f_{IN} = 140\text{MHz}$, -1dBFS , $\text{PGA} = 0$**



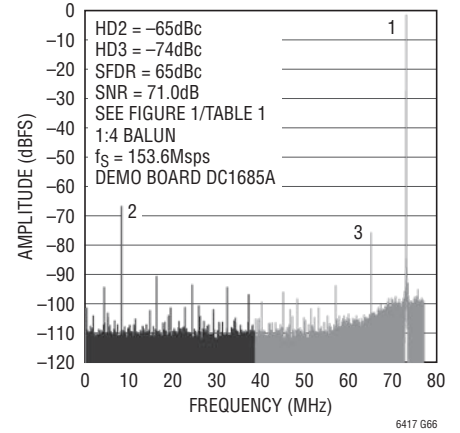
6417 G64

**LTC6417 Driving LTC2209
16-Bit ADC, 64K Point FFT,
 $f_{IN} = 270\text{MHz}$, -1dBFS , $\text{PGA} = 0$**



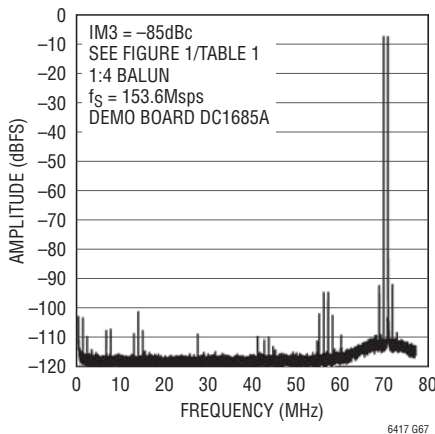
6417 G65

**LTC6417 Driving LTC2209
16-Bit ADC, 64K Point FFT,
 $f_{IN} = 380\text{MHz}$, -1dBFS , $\text{PGA} = 0$**



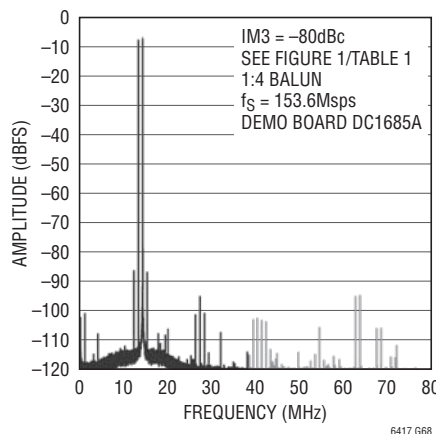
6417 G66

**LTC6417 Driving LTC2209 16-Bit ADC,
32K Point FFT, $f_{IN} = 69.5\text{MHz}$ and
 70.5MHz , -7dBFS/Tone , $\text{PGA} = 0$**



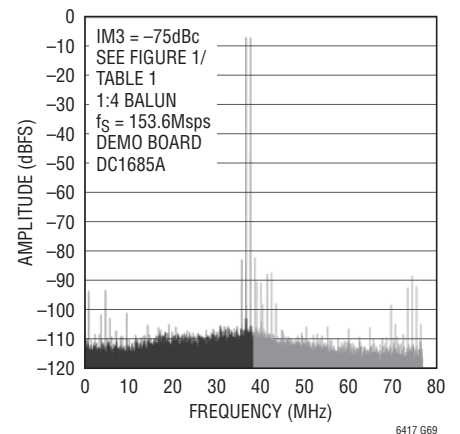
6417 G67

**LTC6417 Driving LTC2209 16-Bit ADC,
64K Point FFT, $f_{IN} = 139.5\text{MHz}$ and
 140MHz , -7dBFS/Tone , $\text{PGA} = 0$**



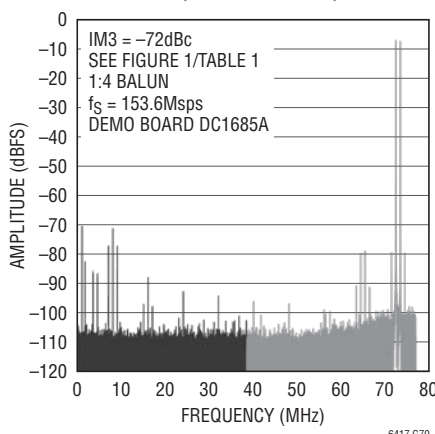
6417 G68

**LTC6417 Driving LTC2209 16-Bit ADC,
64K Point FFT, $f_{IN} = 269.5\text{MHz}$ and
 270.5MHz , -7dBFS/Tone , $\text{PGA} = 0$**



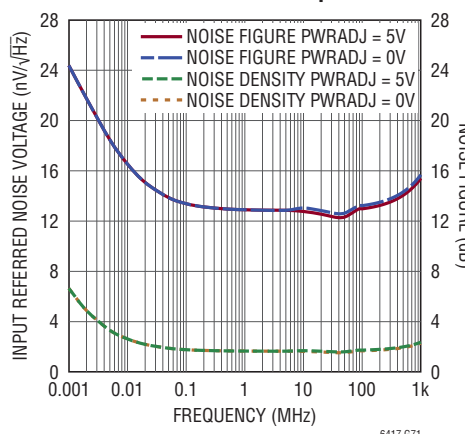
6417 G69

**LTC6417 Driving LTC2209 16-Bit ADC,
64K Point FFT, $f_{IN} = 379.5\text{MHz}$ and
 380.5MHz , -7dBFS/Tone , $\text{PGA} = 0$**



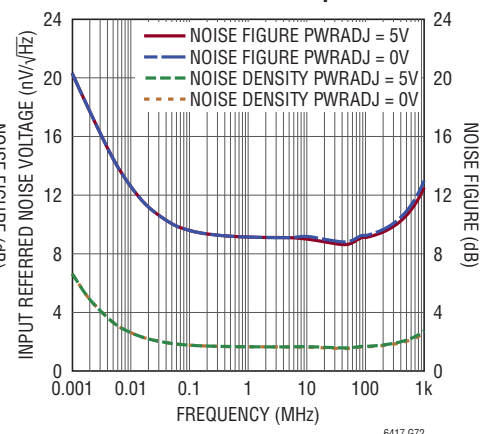
6417 G70

**Input Referred Noise Voltage
vs Frequency and Noise Figure for
the DC1660B with 1:1 Input Balun**



6417 G71

**Input Referred Noise Voltage
vs Frequency and Noise Figure for
the DC1660B with 1:4 Input Balun**



6417 G72

PIN FUNCTIONS

V⁺ (Pins 1, 6, 11, 16): Positive Power Supply. Typically 5V. Split supplies are possible as long as the voltage between V⁺ and GND is 4.75V to 5.25V. Bypass capacitors of 680pF and 0.1μF as close to the part as possible should be used between the supplies.

CLHI (Pin 2): High Side Clamp Voltage. The voltage applied to the CLHI pin defines the upper voltage limit of the OUT⁺ and OUT⁻ pins. This voltage should be set at least 300mV above the upper voltage range of the ADC. On a 5V supply, the CLHI pin will float to a 2.5V default voltage. CLHI has a Thevenin equivalent of approximately 4.8kΩ and can be overdriven by an external voltage. The CLHI pin should be bypassed with a high quality ceramic bypass capacitor of at least 0.01μF.

GND (Pins 3, 7, 10, 17, 20, Exposed Pad Pin 21): Negative Power Supply. Normally tied to ground. All pins and the exposed pad must be tied to the same voltage. GND may be tied to a voltage other than ground as long as the voltage between V⁺ and GND is 4.75V to 5.25V. If the GND pins are not tied to ground, bypass each with 680pF and 0.1μF capacitors as close to the package as possible. The exposed pad must be soldered to the printed circuit board ground plane for good heat transfer.

NC (Pins 4, 13): No Connection. These pins are not connected internally.

PWRADJ (Pin 5): Power Adjust Voltage. The voltage applied to this pin scales the bias current internal to the LTC6417. The PWRADJ pin will float to a 1.6V default voltage. PWRADJ has a Thevenin equivalent resistance of approximately 14.5k and can be overdriven by an external voltage. The PWRADJ pin should be bypassed with a high quality ceramic bypass capacitor of at least 0.01μF.

IN⁺, IN⁻ (Pin 8, Pin 9): Non-inverting and inverting input pins of the buffer, respectively. These pins are high impedance, approximately 9.5k. If AC-coupled, these pins will self bias to the voltage applied to the V_{CM} pin.

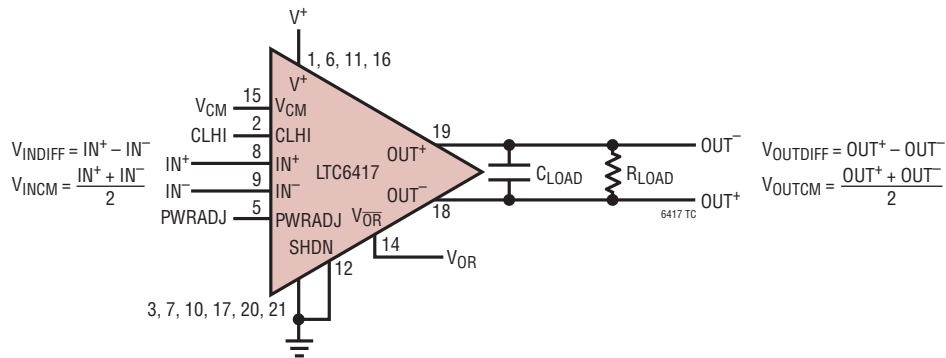
SHDN (Pin 12): This pin puts the LTC6417 in sleep mode when pulled high. If no voltage is applied to the SHDN pin, it floats down to the same potential as GND.

V_{OR} (Pin 14): Overrange Output. This pin, by default at 3.4V, will be pulled down to GND, when one or both input signals go beyond the minimum or maximum swing set by the CLHI and V_{CM} pins.

V_{CM} (Pin 15): This pin sets the output common mode voltage seen at OUT⁺ and OUT⁻ by driving IN⁺ and IN⁻ through a buffer with a high output resistance of 9.5k. The V_{CM} pin has a Thevenin equivalent resistance of approximately 2.7k and can be overdriven by an external voltage. If no voltage is applied to V_{CM}, it will float to a default voltage of approximately 1.25V on a 5V supply. The V_{CM} pin should be bypassed with a high quality ceramic bypass capacitor of at least 0.01μF.

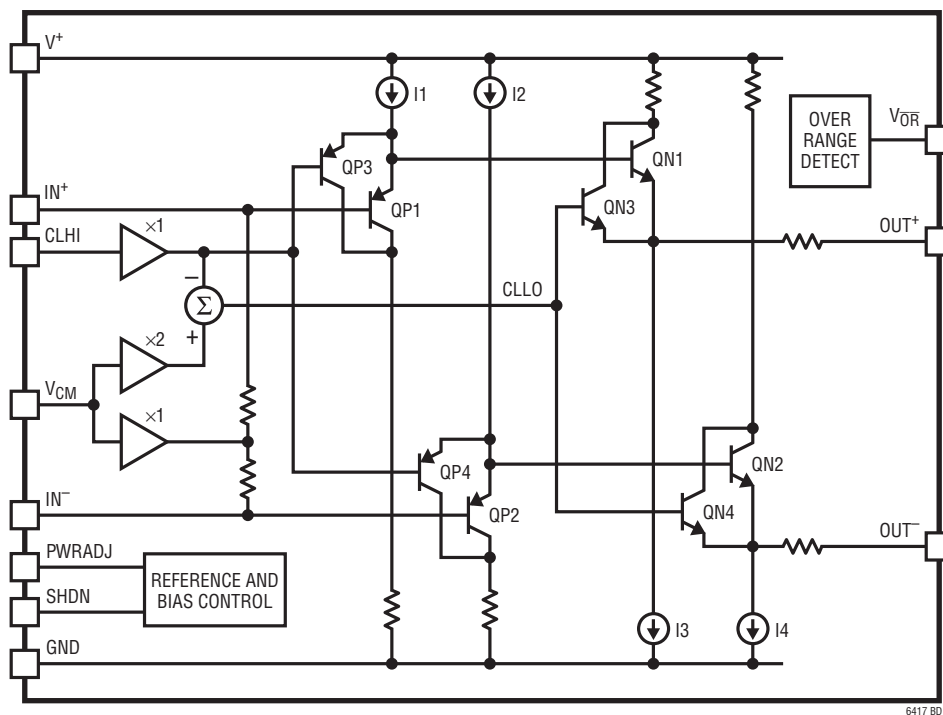
OUT⁻, OUT⁺ (Pin 18, Pin 19): Outputs.

DC TEST CIRCUIT SCHEMATIC



BLOCK DIAGRAM

LTC6417 Simplified Schematic



APPLICATIONS INFORMATION

Circuit Operation

The LTC6417 is a low noise and low distortion fully differential unity gain ADC driver with a -3dB bandwidth spanning DC to 1.6GHz, a differential input impedance of $18.5\text{k}\Omega$, and a differential output impedance of 3Ω . The LTC6417 is composed of a fully differential buffer with output common mode voltage control circuitry and high speed voltage-limiting clamps at the output. Lowpass or bandpass filters are easily implemented with just a few external components. The LTC6417 is very flexible in terms of I/O coupling. It can be AC- or DC-coupled at the inputs, the outputs or both. When using the LTC6417 with DC-coupled inputs, best performance is obtained with an input common mode voltage between 1V and 1.5V. For AC-coupled operation, the LTC6417 will take the voltage applied to the V_{CM} pin and use it to bias the inputs so that the output common mode voltage equals V_{CM} , thus no external circuitry is needed. The V_{CM} pin has been designed to directly interface with the V_{CM} pin found on Linear Technology's high speed ADC families.

Input Impedance and Matching

The LTC6417 has a high differential input impedance of $18.5\text{k}\Omega$. The differential inputs may need to be terminated to a lower value impedance, e.g. 50Ω , in order to provide an impedance match for the source. Figure 1 shows input matching and single-ended to differential conversion using a 1:1 balun, while Figure 2 shows a similar circuit using a 1:4 balun to achieve an additional 6dB of voltage gain. These circuits provide a wideband impedance match. The balun and matching resistors must be placed close to the input pins in order to minimize the rejection due to input mismatch. In Figures 1 and 2, the capacitor center-tapping the two input termination resistors improves high frequency common mode rejection. As an alternative to this wideband approach, a narrowband impedance match can be used at the inputs of the LTC6417 for frequency selection and/or noise reduction.

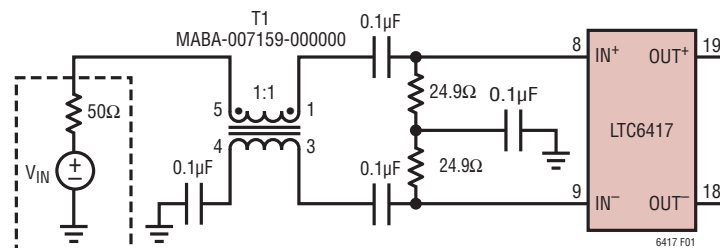


Figure 1. Input Termination for Differential 50Ω Input Impedance Using a 1:1 Balun

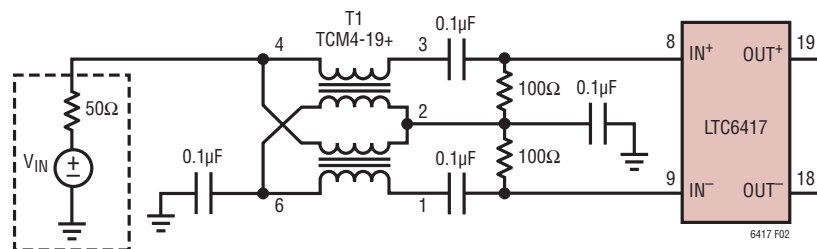


Figure 2. Input Termination for Differential 50Ω Input Impedance Using a 1:4 Balun

APPLICATIONS INFORMATION

The noise figure of the LTC6417 application circuit also depends upon the input termination. For example, the input 1:4 balun in Figure 2 improves noise figure by adding 6dB of voltage gain at the inputs. A trade-off between gain and noise is obvious when constant noise figure circle and constant gain circle are plotted within the same input Smith Chart. This technique can be used to determine the optimal source impedance for a given gain and noise requirement.

Output Match and Filter

The LTC6417 provides an output resistance of 1.5Ω at each output. In most cases, the LTC6417 can be used to drive an ADC without back termination but for testing purposes, Figure 3 shows the LTC6417 driving a differential 50Ω load impedance using a 1:1 balun. If output

matching for the 1:1 balun is desired, resistors of 23.7Ω should be inserted in series with each LTC6417 output. This is shown in Figure 4 where the LTC6417 is driving a differential 100Ω load impedance.

As mentioned above, the LTC6417 can drive an ADC without external output impedance matching, but improved performance can usually be obtained with the addition of a few components. Figure 5 shows a 6th order bandpass filter with a 148MHz center frequency, -3dB points of 85MHz and 210MHz used for driving the LTC2209 16-bit ADC. In the passband the filter has less than 1 dB ripple. This higher order filter has a sharp roll-off outside its passband, therefore it rejects noise and suppresses distortion components in its stopband. To double the filter center frequency, halve the capacitor and inductor values, and maintain resistor values; this also doubles the filter bandwidth.

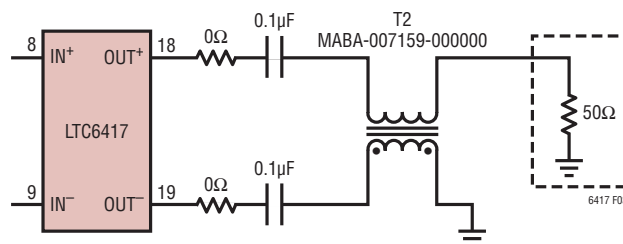


Figure 3. LTC6417 with No Back Termination Driving a 50Ω Load Using a 1:1 Balun

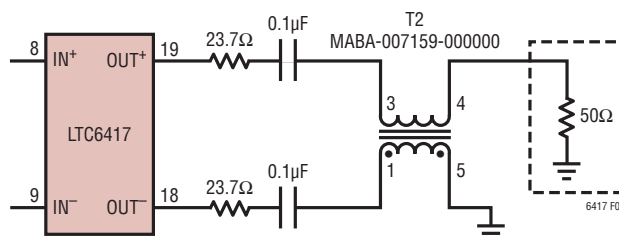


Figure 4. Output Termination for Differential 50Ω Load Using a 1:1 Balun

APPLICATIONS INFORMATION

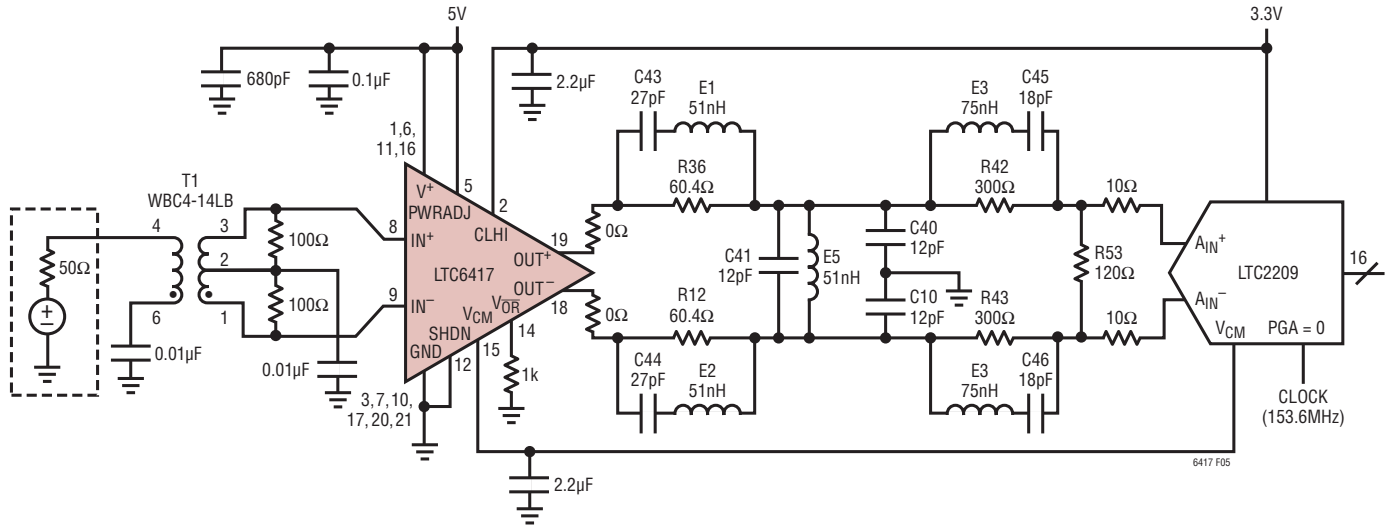


Figure 5. DC1685A Simplified Schematic with Suggested Bandpass Filter for Driving an LTC2209 16-Bit ADC at 140MHz

Table 1. Bandpass Filter Component Values for Different Input Frequencies

| COMPONENTS | INPUT FREQUENCIES | | | |
|------------|-------------------|--------|--------|--------|
| | 70MHz | 140MHz | 270MHz | 380MHz |
| R12 = R36 | 60.4Ω | 60.4Ω | 60.4Ω | 60.4Ω |
| C43 = C44 | 56pF | 27pF | 15pF | 12pF |
| E1 = E2 | 100nH | 51nH | 27nH | 18nH |
| C41 | 47pF | 12pF | 12pF | 10pF |
| C10 = C40 | 13pF | 12pF | 3.3pF | 2.7pF |
| E5 | 100nH | 51nH | 27nH | 18nH |
| R42 = R43 | 300Ω | 300Ω | 300Ω | 300Ω |
| R53 | 120Ω | 120Ω | 120Ω | 120Ω |
| C45 = C46 | 39pF | 18pF | 10pF | 8.2pF |
| E3 = E4 | 150nH | 75nH | 39nH | 27nH |

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Output Common Mode Adjustment

For AC-coupled applications, the output common mode voltage is set by the V_{CM} pin. An internal buffer, as shown in Figure 6, couples the voltage on the V_{CM} pin to the inputs via high impedance resistors. Because the input common mode voltage is approximately the same as the output common mode voltage, both are approximately equal to the voltage applied to the V_{CM} pin. For DC-coupled applications, the internal V_{CM} is overdriven by the input signal. The V_{CM} pin has a Thevenin equivalent resistance of 2.7k and can be overdriven by an external voltage. The V_{CM} pin floats to a default voltage of 1.25V on a 5V supply. The output common mode voltage is capable of tracking V_{CM} in a range from 0.29V to 2.25V on a 5.0V supply. The V_{CM} pin can be floated, but it should always be bypassed close to the LTC6417 with a 0.1 μ F bypass capacitor to GND. When interfacing with A/D converters such as the LTC22xx families, the V_{CM} pin can be connected to the V_{CM} output pin of the ADC, as shown in Figure 5.

Clamping, the CLHI Pin and the V_{CM} Pin

The CLHI pin is used to set the high side clamp voltage of the high speed internal circuitry.

This limits the single-ended maximum and minimum voltage excursion at each of the outputs. This feature is extremely important in applications with input signals having very large peak-to-average ratios such as cellular base station receivers.

Internal circuitry generates a symmetric low side clamp voltage with respect to the common mode voltage V_{CM} (Figures 7 and 8). The LTC6417 clamp control circuitry features two additional mechanisms. First, internally imposed maximum swing of 2.5V and minimum swing of 0.2V ensure that the transistors do not go into deep saturation. This ensures a quick recovery after the clamps are released. Second, if CLHI voltage is less than V_{CM} , internal CLLO starts to track CLHI. This limits output swing and protects output transistors. Since the clamp response is on the order of 5ns to clamp and 1ns to release, clamp circuit becomes less effective at frequencies beyond 160MHz.

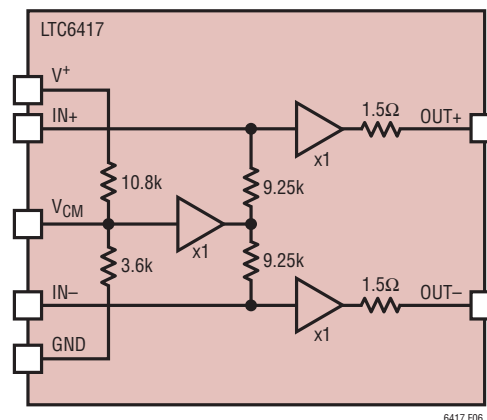


Figure 6. LTC6417 Internal Topology Showing the Common Mode Buffer Biasing the Inputs

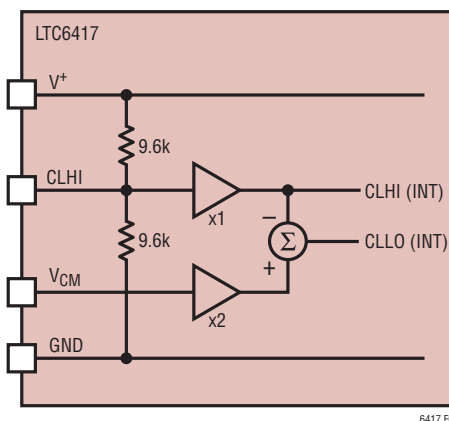


Figure 7. Internal Circuitry Generating Symmetric Clamp Voltages with Respect to V_{CM}

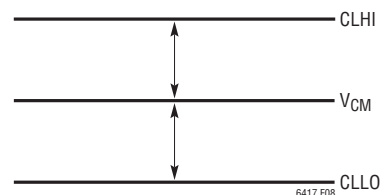


Figure 8. Symmetric High- and Low-Side Clamp Voltages with Respect to V_{CM}

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If a very large signal arrives at the LTC6417, the voltages applied to the CLHI and V_{CM} pins will determine the maximum and minimum output swing. Once the input signal returns to the normal operating range, the LTC6417 returns to linear operation within 2ns. For DC-coupled operation, the common mode of the input signals might be different than the voltage on the V_{CM} pin. The minimum swing will still be set by the voltages applied to the V_{CM} and CLHI pins.

CLHI is a high impedance input. It has an input impedance of 4.8k. On a 5V supply, CLHI self-biases to 2.5V. To limit the signal swing to a subsequent stage's power supply, e.g. an ADC such as the LTC2165, simply connect CLHI to the positive supply pin of the LTC2165. The CLHI pin should be bypassed with a 0.1 μ F capacitor as close to the LTC6417 as possible.

The V_{OR} Pin

The V_{OR} , overrange pin signals an overrange condition when one or both inputs exceed the minimum or maximum signal swing limits set by the CLHI and V_{CM} pins.

The LTC6417 V_{OR} pin can be used by a control system to limit the input power dynamically. This is very useful in applications where the overload response of the complete system would be too slow.

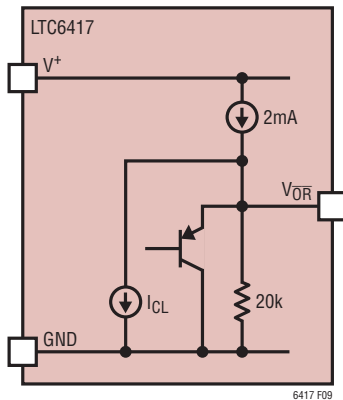


Figure 9. LTC6417 Internal Topology Showing V_{OR} Pin with Pull-Down Resistor and Clamp

The V_{OR} pin, as shown in Figure 9, is internally connected to a current source sourcing 2mA, plus an internal 20k resistor pull-down to GND. An internal clamp limits the maximum output to 3.4V. As soon as one of the inputs goes beyond the limits, and therefore engages one of the clamps, the output current, hence, the V_{OR} voltage goes to zero. The dynamic response of the V_{OR} pin can be adjusted with an external resistor and an optional external capacitor. For a high speed operation, add a 50 Ω resistor from V_{OR} to GND, resulting in a high speed signal with 100mV swing.

The PWRADJ Pin

The voltage applied to the PWRADJ pin scales the supply current and performance of the LTC6417. This is useful for reducing power consumption in applications where linearity of the LTC6417 exceeds the linearity of the other components in the system; hence LTC6417's linearity can be derated without effecting system performance. PWRADJ is a high impedance input. It has an input impedance of 14.5k. On a 5V supply, PWRADJ self-biases to 1.6V. For full power, simply connect PWRADJ to the positive supply V^+ . For minimum power, short the PWRADJ pin to GND. The PWRADJ pin should be bypassed with a 0.1 μ F capacitor as close to the LTC6417 as possible. LTC6417 performance vs PWRADJ can be found in the graphs.

The SHDN Pin

When pulled high, the SHDN pin puts the LTC6417 in sleep mode, significantly reducing supply current. SHDN is a high impedance input. It has an input impedance of 10.5k Ω . If the SHDN pin is not driven with an external voltage, it floats down to the same potential as GND, keeping the LTC6417 enabled. The SHDN pin should be bypassed with a 0.1 μ F capacitor as close to the LTC6417 as possible.

In sleep mode, the input and output stages are turned off, but the input and output clamps are kept alive to protect the part against overvoltage.

The supply current in sleep mode is only 24mA, instead of the typical 125mA. But should the clamps turn on, the current drawn from the supply can be as high as 180mA.

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This can be avoided by following a few precautions when putting the LTC6417 in sleep mode:

- Do not force the outputs below the inputs, this will turn the output stages on.
- Either float CLHI or tie it to V_{CC} . This will allow a wider signal range at the inputs before the clamps are activated.
- Maintain the inputs below CLHI or 2.5V whichever is lower, otherwise the input clamps will be activated.
- Do not short V_{CM} or the outputs to GND, in either case the output clamps will turn on. Current drawn from the supply can be as high as 180mA.
- Float the outputs if possible. The outputs will be pulled down by internal resistors to V_{CM} .

Heeding these precautions will protect the LTC6417 as well any part it is driving, while maintaining a low current consumption in sleep mode.

Noise and Noise Figure

The LTC6417's differential input referred voltage and current noise densities are $1.5nV/\sqrt{Hz}$ and $4.3pA/\sqrt{Hz}$, respectively.

Before presenting a noise model, the circuit with the transformer in Figure 10 will be simplified. In Figure 11, the circuit is redrawn with the source impedance reflected to the secondary side of the transformer. The source impedance is multiplied by the impedance ratio m of the transformer. In Figure 12, noise sources associated with the amplifier and resistors have been added. Based on this noise model of the LTC6417, the total output noise power excluding the noise contribution of the source is:

$$\begin{aligned} e_{no}^2 &= e_{ni}^2 + (i_{ni} \cdot R_{EQ})^2 + i_{RT}^2 \cdot R_{EQ}^2 \\ &= e_{ni}^2 + (i_{ni} \cdot R_{EQ})^2 + \frac{4kT}{R_T} \cdot R_{EQ}^2 \end{aligned}$$

where $R_{EQ} = mR_S || R_T$ is the equivalent impedance seen at the input of the LTC6417. The output noise power due to the noise of source resistance is given by:

$$\begin{aligned} e_{no(mR_S)}^2 &= i_{mR_S}^2 \cdot R_{EQ}^2 \\ &= \frac{4kT}{mR_S} \cdot R_{EQ}^2 \end{aligned}$$

Noise figure (NF) is calculated from the ratio of these noise powers:

$$NF = 10 \log \left(1 + \frac{e_{no}^2}{e_{no(mR_S)}^2} \right)$$

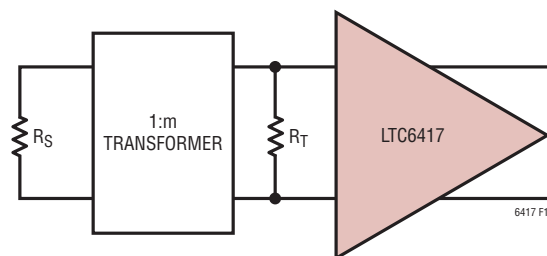


Figure 10. LTC6417 with a Transformer

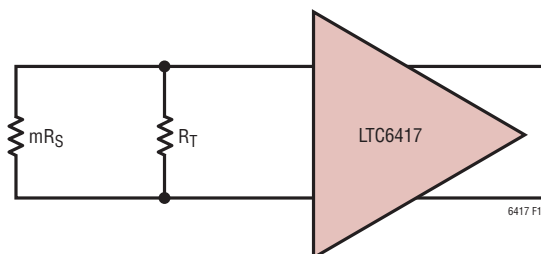


Figure 11. Source Resistance Referred to the Secondary

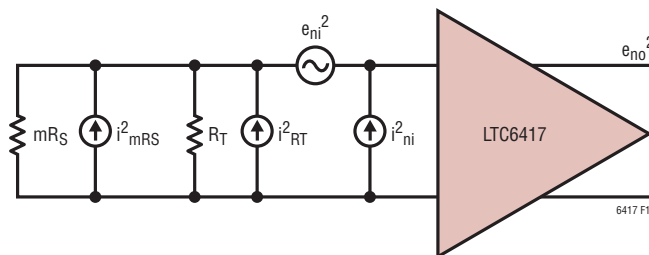


Figure 12. LTC6417 Simplified Noise Model

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In most cases the termination resistor will be matched to the source resistance, e.g. $R_T = mR_S$. For the LTC6417 with a wide-band terminated transformer, a plot of output and input noise density and NF versus termination resistor is shown in Figure 13. To get the best noise performance in the system, use the LTC6417 matched to a transformer with high impedance ratio. Although the output noise density will be higher, noise figure will improve because of the additional gain realized in the transformer. An impedance ratio greater than 8 is not recommended, as the increased termination resistance with the LTC6417 input capacitance will limit signal bandwidth. Consult Table 2 for a quick estimate of the LTC6417's output noise density and NF for different transformer impedance ratios. Measured NF numbers will be higher as the simple noise model does not take the insertion loss in the transformer into account.

Table 2. Output Noise Density and NF of the LTC6417 with a Wide-Band Terminated Transformer, $R_S = 50\Omega$

| TRANSFORMER IMPEDANCE RATIO m | TERMINATION RESISTOR R_T (Ω) | GAIN (V/V) | OUTPUT NOISE DENSITY e_{no} (nV/\sqrt{Hz}) | NF (dB) |
|---------------------------------|---|------------|--|---------|
| 1 | 50 | 1.0 | 1.57 | 11.2 |
| 2 | 100 | 1.4 | 1.64 | 8.9 |
| 4 | 200 | 2.0 | 1.80 | 7.0 |
| 8 | 400 | 2.8 | 2.14 | 5.9 |

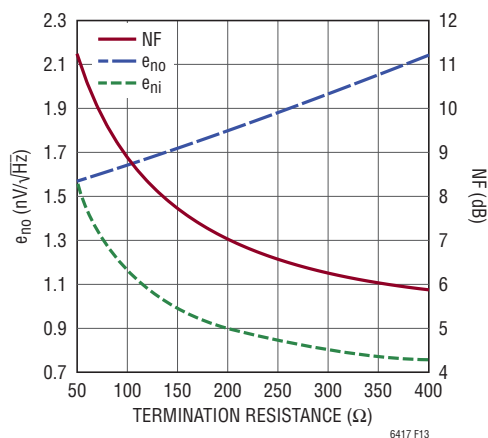


Figure 13. LTC6417 Output and Input Noise Density and NF vs Termination Resistance

Interfacing the LTC6417 to A/D Converters

The LTC6417 has been specially designed to interface directly with high speed A/D converters. It is possible to drive the ADC directly from the LTC6417. In practice, however, better performance may be obtained by adding a few external components at the output of the LTC6417. Figure 5 shows the LTC6417 driving an LTC2209 16-bit ADC. The differential outputs of the LTC6417 are bandpass filtered, then drive the differential inputs of the LTC2209. In many applications, a filter like this is desirable to limit the wideband noise of the amplifier. This is especially true in high performance 16-bit designs. The minimum recommended network between the LTC6417 and the ADC is simply two 10Ω series resistors, which are used to help eliminate resonances associated with the stray capacitance of PCB traces and the stray inductance of the internal bond wires at the ADC input pins and the driver output pins.

Single-Ended Signals

The LTC6417 has not been designed to convert single-ended signals to differential signals. A single-ended input signal can be converted to a differential signal via a balun connected to the inputs of the LTC6417. Figure 5 shows the LTC6417 driven by a 1:4 transformer which provides 6dB of voltage gain while also performing a single-ended to differential conversion.

Power Supply Considerations

For best linearity, the LTC6417 should have a positive supply of $V^+ = 5V$. For ESD protection, the LTC6417 has an internal edge-triggered supply voltage clamp. The timing mechanism of the clamp enables the LTC6417's protection circuit during ESD events. This internal clamp can also be activated by voltage overshoot and rapid slew rate on the positive supply V^+ pin. The LTC6417 should not be hot-plugged into a powered socket because there is a risk of activating this internal ESD clamp circuit. Bypass capacitors of 680pF and 0.1 μ F should be connected to the V^+ pin, as close as possible to the LTC6417.

Interfacing the LTC6417 with Active Mixers for Ultrawide IF Bandwidth

The LTC6417 is an excellent interface amplifier for use with active downconverting mixers like the LTC5567. By using

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the LTC6417 as a post-amplifier for the LTC5567, it is possible to achieve IF bandwidths in excess of 500MHz, while adding bandpass filtering. A key to achieving this extremely wide IF bandwidth is the use of pre-emphasis inductors in series with the LTC6417 inputs to compensate for the inherent rolloff caused by the LTC6417 input capacitance interacting with the interface impedance. In the example seen in Figure 14, a value of 33nH for each pre-emphasis inductor gives excellent wideband performance. Figure 15 shows performance for various values of L. For L = 33nH, overall conversion gain remains within 1dB from 90MHz to 590MHz, resulting in 500MHz of IF bandwidth.

Test Circuits

Due to the fully differential design of the LTC6417 and its usefulness in applications both with and without ADCs, two test circuits have been used to generate the information in this data sheet. Test circuit A is DC1660B, a two-port

demonstration circuit for the LTC6417. The board layout and the schematic are shown in Figures 16 and 17. These circuits include a 1:4 input balun and a 1:1 output balun for single-ended-to-differential conversion, allowing direct analysis using a 2-port network analyzer. Including the input and output baluns, the -3dB bandwidth is approximately 600MHz. A 1:4 input balun before the LTC6417 inputs provides 6dB of voltage gain, but results in better noise figure performance compared to a 1:1 input balun. Noise figure measurements for both input baluns can be found in the graphs.

Test circuit B is DC1685A. It consists of an LTC6417 driving an LTC2209 16-bit 153.6MSPS ADC. It is intended for use in conjunction with DC890B (computer interface board) and proprietary Linear Technology evaluation software to evaluate the performance of both parts together. Both the DC1685A board layout and the schematic can be seen Figures 18 and 19.

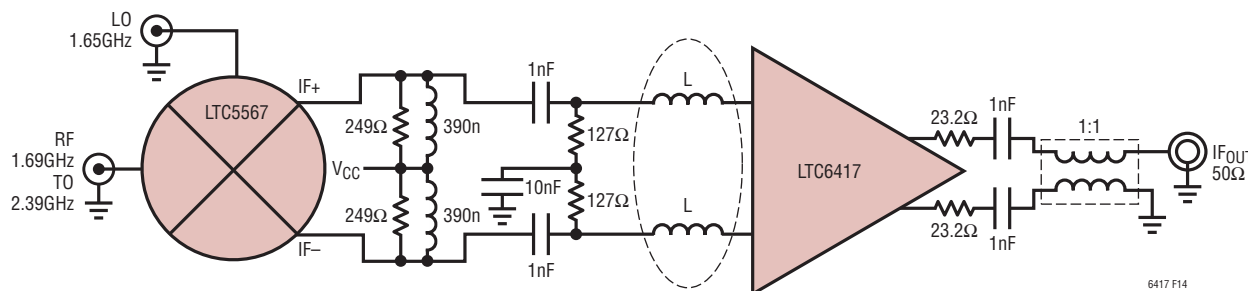


Figure 14

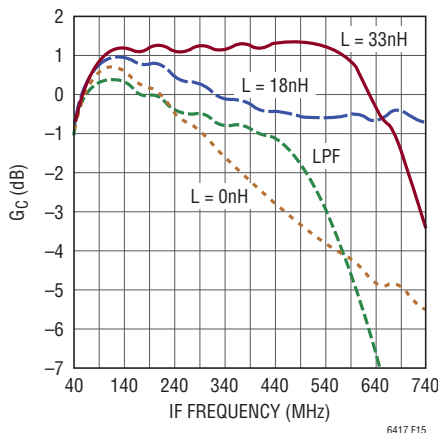


Figure 15

APPLICATIONS INFORMATION

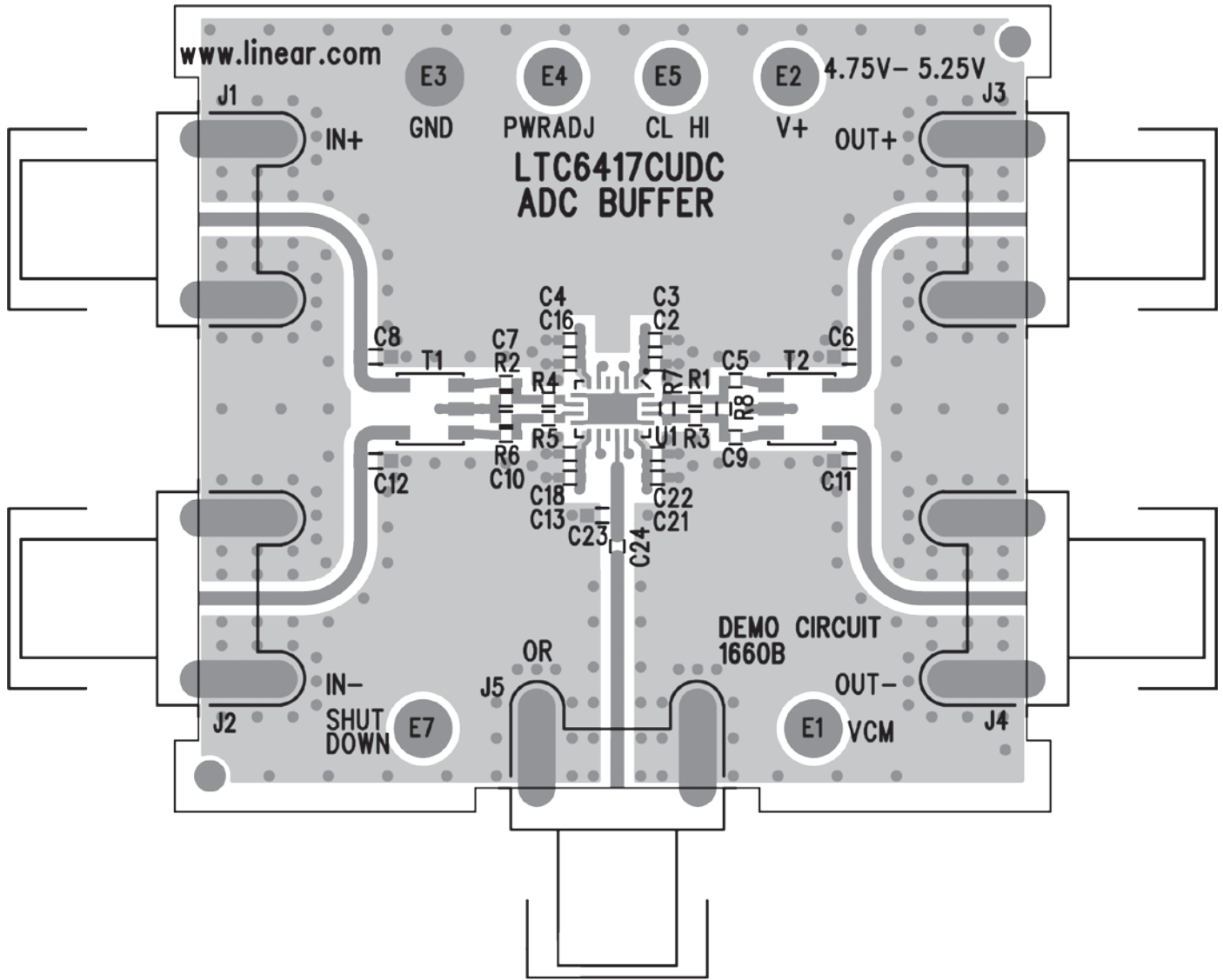


Figure 16. Demo Board DC1660B Layout

APPLICATIONS INFORMATION

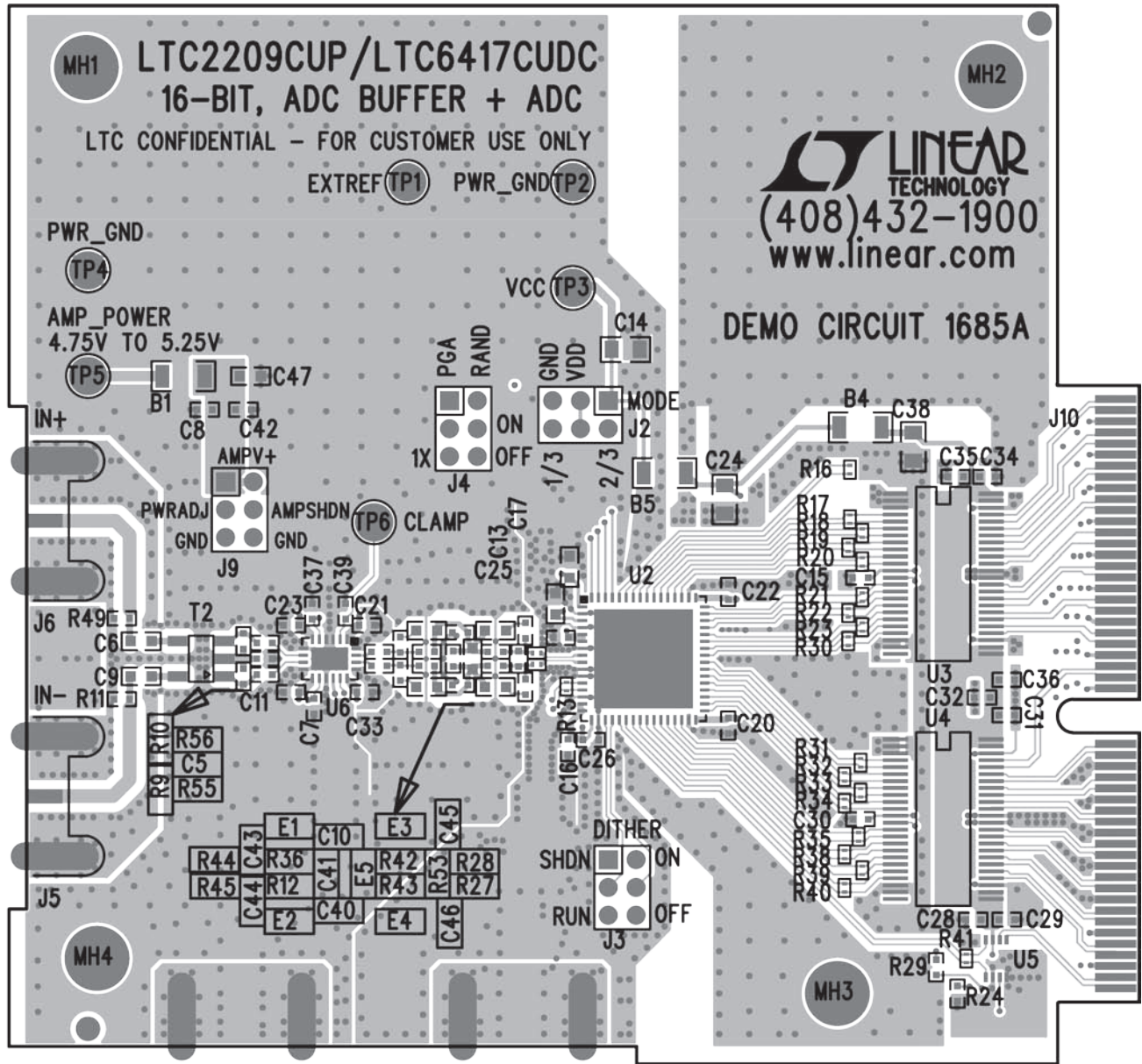
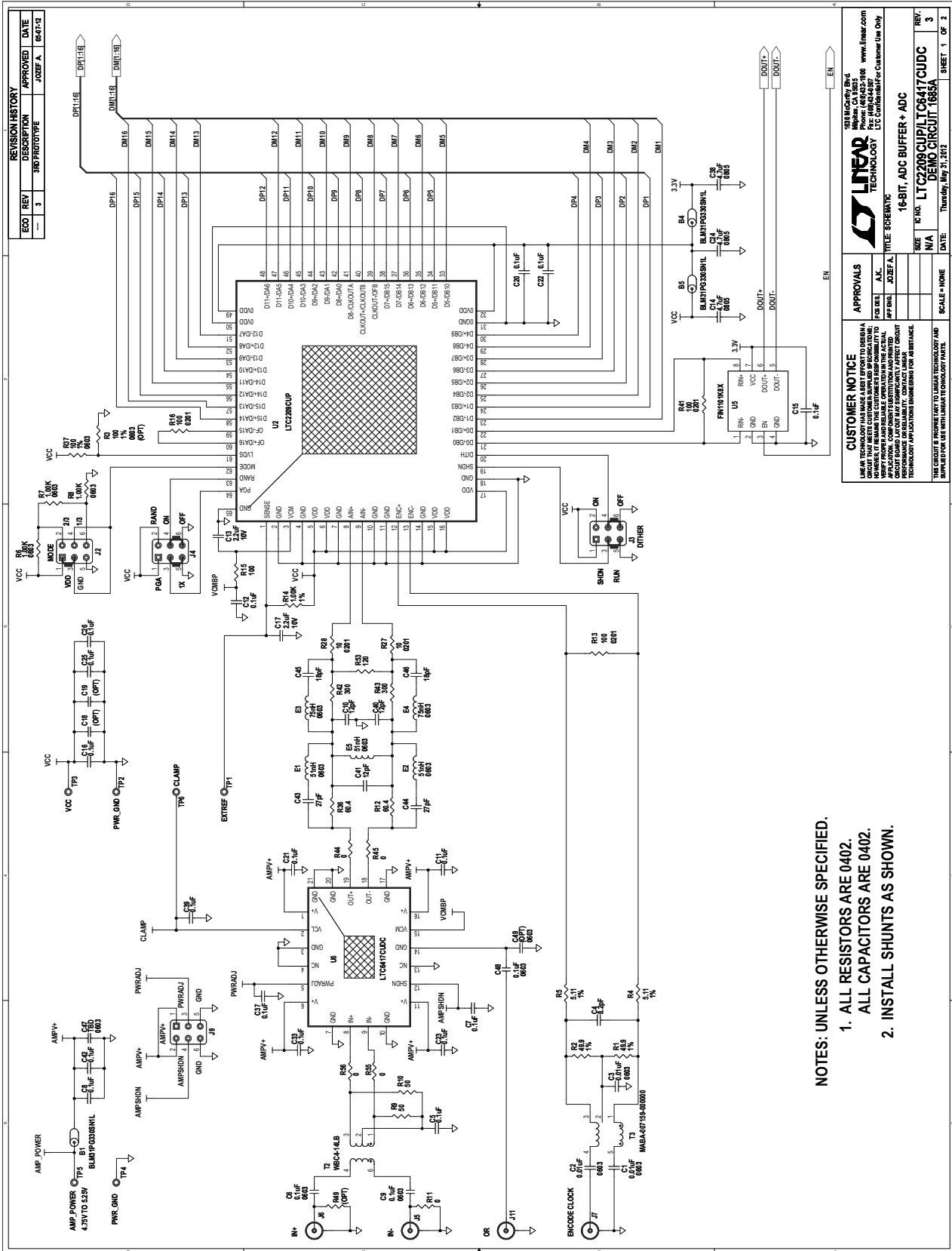


Figure 18. Demo Board DC1685A Layout

APPLICATIONS INFORMATION



| ECO | REV | DESCRIPTION | APPROVED | DATE |
|-----|-----|---------------|----------|----------|
| — | 3 | 3RD PROTOTYPE | JOSEF A. | 05-07-02 |

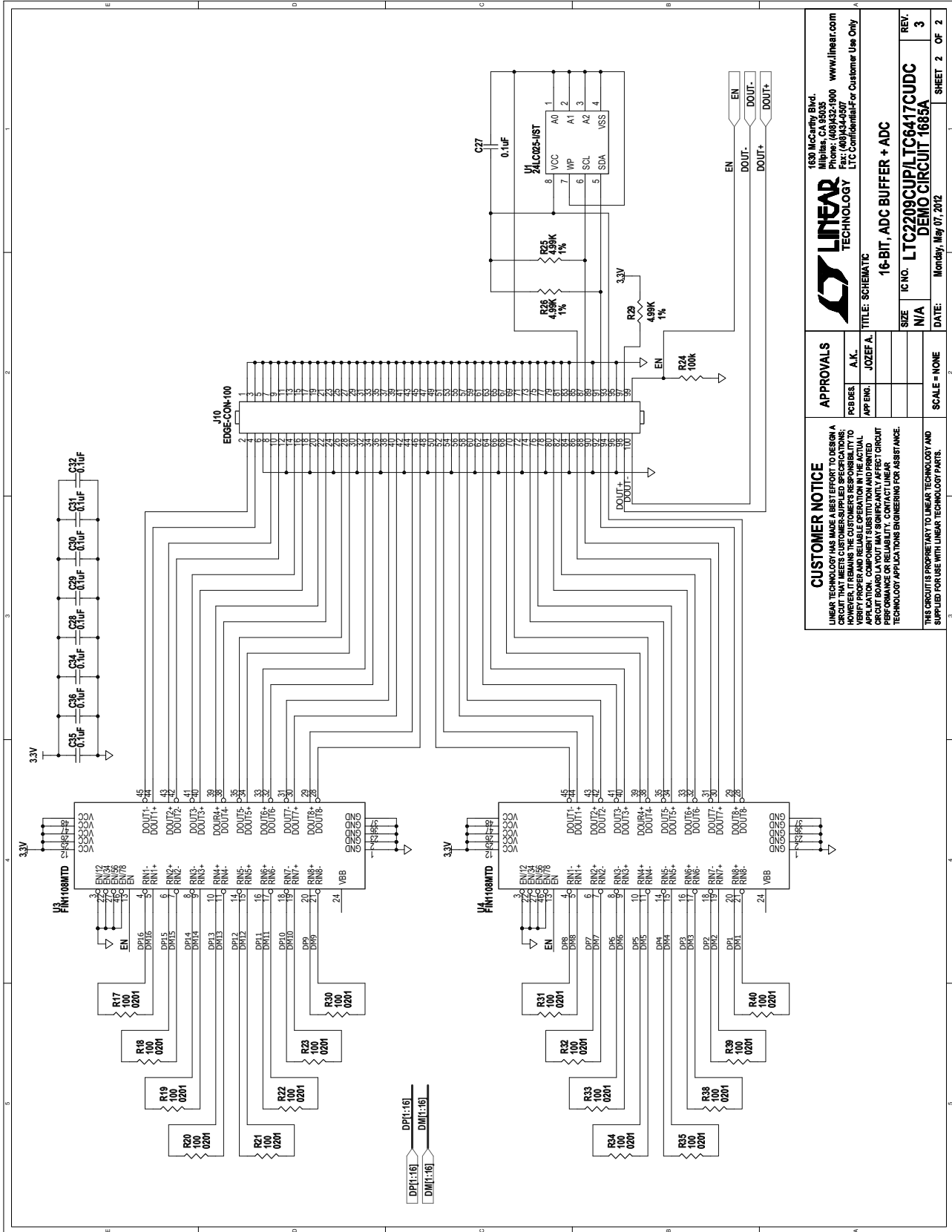
| REV. HISTORY | APPROVED | DATE |
|---------------|----------|----------|
| 3RD PROTOTYPE | JOSEF A. | 05-07-02 |

| CUSTOMER NOTICE | | APPROVALS | |
|---|--|-----------|------------------------|
| LINAER FROM THE LINAER LIAISON PROJECT TO DETERMINE THE BEST CUSTOMER APPROVAL OF OPERATIONS. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | DESIGN | A.J.C. |
| THE CIRCUIT IS PROVIDED AS A DEMO BOARD AND IS NOT INTENDED FOR PRODUCTION. CONTACT LINAER FOR INFORMATION ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | APP. ENG. | JOSEF A. |
| PERFORMANCE CHARACTERISTICS ARE BASED ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | SIZE | N/A |
| THE CIRCUIT IS PROVIDED AS A DEMO BOARD AND IS NOT INTENDED FOR PRODUCTION. CONTACT LINAER FOR INFORMATION ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | IC NO. | LTC2208CUP/LTC6417CUDC |
| THE CIRCUIT IS PROVIDED AS A DEMO BOARD AND IS NOT INTENDED FOR PRODUCTION. CONTACT LINAER FOR INFORMATION ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | DATE | Thursday, May 31, 2002 |
| THE CIRCUIT IS PROVIDED AS A DEMO BOARD AND IS NOT INTENDED FOR PRODUCTION. CONTACT LINAER FOR INFORMATION ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | SCALE | NONE |
| THE CIRCUIT IS PROVIDED AS A DEMO BOARD AND IS NOT INTENDED FOR PRODUCTION. CONTACT LINAER FOR INFORMATION ON THE LINAER LIAISON PROJECT. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. THE LINAER LIAISON PROJECT IS A JOINT EFFORT BETWEEN LINAER AND THE CUSTOMER. | | SHEET | 1 OF 2 |

NOTES: UNLESS OTHERWISE SPECIFIED.
 1. ALL RESISTORS ARE 0402.
 ALL CAPACITORS ARE 0402.
 2. INSTALL SHUNTS AS SHOWN.

Figure 19. Demo Board DC1685A Schematic (Test Circuit B)

APPLICATIONS INFORMATION



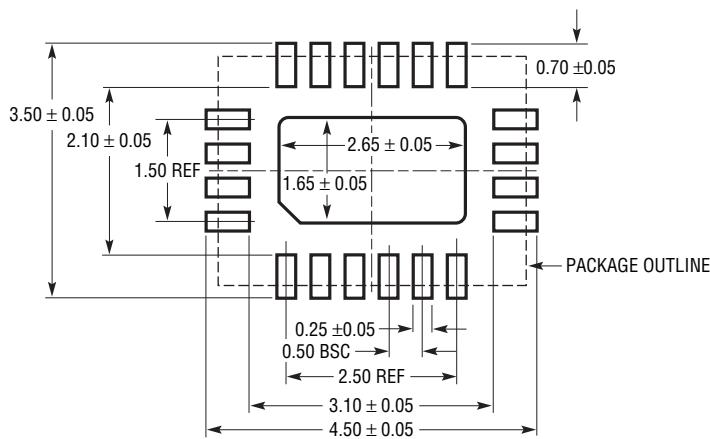
| | | | |
|--|--|---|---------------|
| <p>CUSTOMER NOTICE LINEAR TECHNOLOGY HAS MADE A BEST EFFORT TO DESIGN A SCHEMATIC FOR THIS CIRCUIT. HOWEVER, IT REMAINS THE CUSTOMER'S RESPONSIBILITY TO VERIFY PROPER AND RELIABLE OPERATION IN THE ACTUAL APPLICATION. COMPONENT SUBSTITUTION AND PRINTED BOARD MANUFACTURING VARIATIONS MAY AFFECT CIRCUIT PERFORMANCE OR RELIABILITY. CONTACT LINEAR TECHNOLOGY APPLICATIONS ENGINEERING FOR ASSISTANCE.</p> | | <p>APPROVALS</p> <p>DESIGNER: _____ A.I.C.: _____ APP'NG: JOZEFA</p> | |
| <p>THIS CIRCUIT IS PROPRIETARY TO LINEAR TECHNOLOGY AND SUPPLIED FOR USE WITH LINEAR TECHNOLOGY PARTS.</p> | | <p>SCALE = NONE</p> | |
| <p>LINEAR TECHNOLOGY 1630 McCarthy Blvd. Milpitas, CA 95035 Phone: (408)432-1900 www.linear.com Fax: (408)434-5050 LTC Confidential or Customer Use Only</p> | | <p>16-BIT, ADC BUFFER + ADC DEMO CIRCUIT 1685A</p> | |
| <p>DATE: Monday, May 07, 2012</p> | | <p>SIZE: N/A</p> | <p>REV: 3</p> |
| <p>SHEET 2 OF 2</p> | | <p>IC NO. LTC2209CUIPLTC6417CUDC</p> | |

Figure 19 (Continued). Demo Board DC1685A Schematic (Test Circuit B)

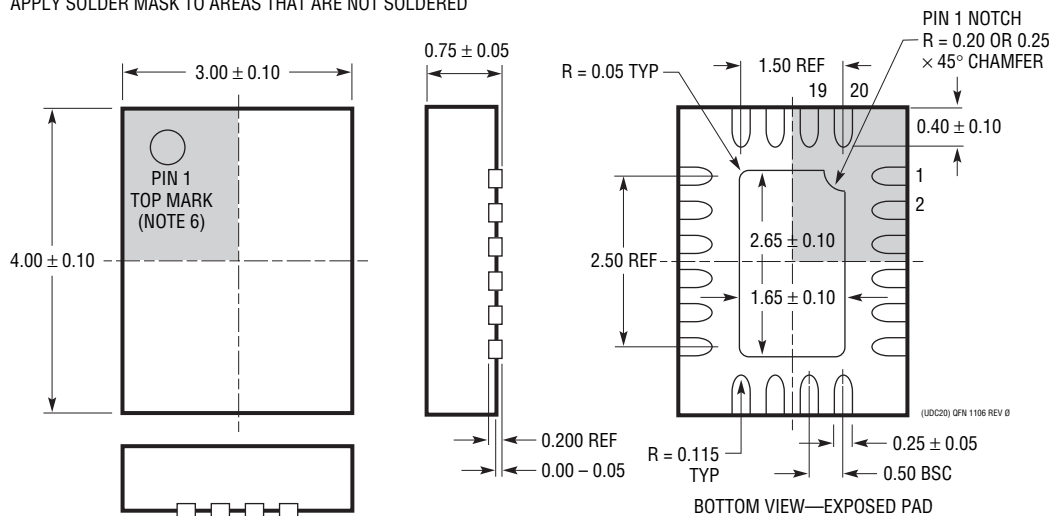
PACKAGE DESCRIPTION

Please refer to <http://www.linear.com/designtools/packaging/> for the most recent package drawings.

UDC Package
20-Lead Plastic QFN (3mm × 4mm)
 (Reference LTC DWG # 05-08-1742 Rev 0)



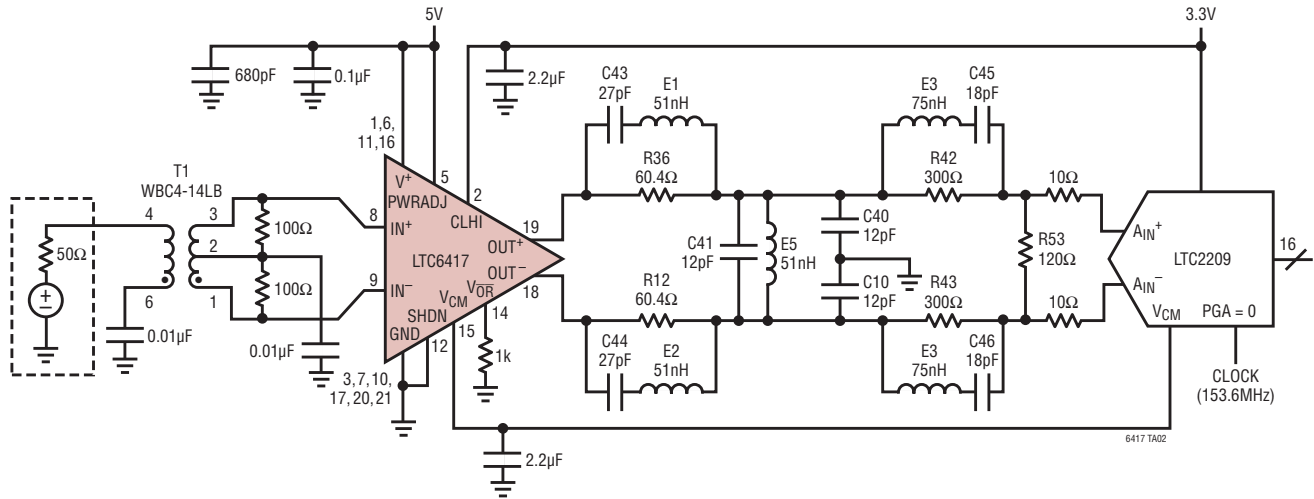
RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS
 APPLY SOLDER MASK TO AREAS THAT ARE NOT SOLDERED



- NOTE:
1. DRAWING IS NOT A JEDEC PACKAGE OUTLINE
 2. DRAWING NOT TO SCALE
 3. ALL DIMENSIONS ARE IN MILLIMETERS
 4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
 5. EXPOSED PAD SHALL BE SOLDER PLATED
 6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

TYPICAL APPLICATION

DC1685A Simplified Schematic with Suggested Output Termination for Driving an LTC2209 16-Bit ADC at 140MHz



RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
|---|---|---|
| Fixed Gain IF Amplifiers/ADC Drivers | | |
| LTC6400-8/LTC6400-14/ LTC6400-20/LTC6400-26 | 1.8GHz Low Noise, Low Distortion Differential ADC Drivers | -71dBc IM3 at 240MHz 2V _{p-p} Composite, I _S = 90mA, A _V = 8dB, 14dB, 20dB, 26dB |
| LTC6420-20 | Dual 1.8GHz Low Noise, Low Distortion Differential ADC Drivers | Dual Version of the LTC6400-20, A _V = 8dB, 14dB, 20dB, 26dB |
| LTC6401-8/LTC6401-14/ LTC6401-20/LTC6401-26 | 1.3GHz Low Noise, Low Distortion Differential ADC Drivers | -74dBc IM3 at 140MHz 2V _{p-p} Composite, I _S = 50mA, A _V = 8dB, 14dB, 20dB, 26dB |
| LTC6421-20 | Dual 1.3GHz Low Noise, Low Distortion Differential ADC Drivers | Dual Version of the LTC6401-20, A _V = 8dB, 14dB, 20dB, 26dB |
| IF Amplifiers/ADC Drivers with Variable Gain | | |
| LTC6412 | 800MHz, 31dB Range Analog-Controlled VGA | Continuously Adjustable Gain Control, -14dB to 17dB Linear-in-dB Gain Range |
| LT5554 | High Dynamic Range 7-Bit Digitally Controlled IF VGA/ADC Driver | OIP3 = 46dBm at 200MHz, Gain Range 1.725 to 17.6dB 0.125dB Steps |
| LT5514 | Ultra-Low Distortion IF Amplifier/ADC Driver with Digitally Controlled Gain | OIP3 = 47dBm at 100MHz, Gain Range 10.5dB to 33dB 1.5dB Steps |
| LT5524 | Low Distortion IF Amplifier/ADC Driver with Digitally Controlled Gain | OIP3 = 40dBm at 100MHz, Gain Range 4.5dB to 37dB 1.5dB Steps |
| Baseband Differential Amplifiers | | |
| LT6416 | 2GHz Low Noise Differential 16-Bit ADC Buffer | -84dBc IM3 at 160MHz 2V _{p-p} Composite, A _V = 1, e _n = 1.8nV/√Hz, 42mA |
| LTC6409 | 10GHz 1.1nV/√Hz ADC Driver | AC- or DC-Coupled 0MHz to 100MHz |
| LTC6406 | 3GHz Rail-to-Rail Input Differential Amplifier/ADC Driver | -65dBc IM3 at 50MHz 2V _{p-p} Composite, Rail-to-Rail Inputs, e _n = 1.6nV/√Hz, 18mA |
| LTC6404-1/LTC6404-2/ LTC6404-4 | Low Noise Rail-to-Rail Output Differential Amplifier/ADC Driver | 16-Bit SNR and SFDR at 10MHz, Rail-to-Rail Outputs, e _n = 1.5nV/√Hz, LTC6404-1 is Unity-Gain Stable, LTC6404-2 is Gain-of-2 Stable |
| LTC6403-1 | Low Noise Rail-to-Rail Output Differential Amplifier/ADC Driver | 16-Bit SNR and SFDR at 3MHz, Rail-to-Rail Outputs, e _n = 2.8nV/√Hz |
| ADCs | | |
| LTC2209 | 16-Bit 160Msps ADC | 77.3dBFS Noise Floor, 100dB SFDR |
| LTC2208 | 16-Bit 130Msps ADC | 78dBFS Noise Floor, 100dB SFDR |

6417f

Компания «Океан Электроники» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Поставка оригинальных импортных электронных компонентов напрямую с производств Америки, Европы и Азии, а так же с крупнейших складов мира;
- Широкая линейка поставок активных и пассивных импортных электронных компонентов (более 30 млн. наименований);
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Помощь Конструкторского Отдела и консультации квалифицированных инженеров;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Поставка электронных компонентов под контролем ВП;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- При необходимости вся продукция военного и аэрокосмического назначения проходит испытания и сертификацию в лаборатории (по согласованию с заказчиком);
- Поставка специализированных компонентов военного и аэрокосмического уровня качества (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Actel, Aeroflex, Peregrine, VPT, Syfer, Eurofarad, Texas Instruments, MS Kennedy, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Компания «Океан Электроники» является официальным дистрибьютором и эксклюзивным представителем в России одного из крупнейших производителей разъемов военного и аэрокосмического назначения «JONHON», а так же официальным дистрибьютором и эксклюзивным представителем в России производителя высокотехнологичных и надежных решений для передачи СВЧ сигналов «FORSTAR».



JONHON

«JONHON» (основан в 1970 г.)

Разъемы специального, военного и аэрокосмического назначения:

(Применяются в военной, авиационной, аэрокосмической, морской, железнодорожной, горно- и нефтедобывающей отраслях промышленности)

«FORSTAR» (основан в 1998 г.)

ВЧ соединители, коаксиальные кабели, кабельные сборки и микроволновые компоненты:

(Применяются в телекоммуникациях гражданского и специального назначения, в средствах связи, РЛС, а так же военной, авиационной и аэрокосмической отраслях промышленности).



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